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(54) **ENGINE CARBURETION**

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See application file for complete search history.

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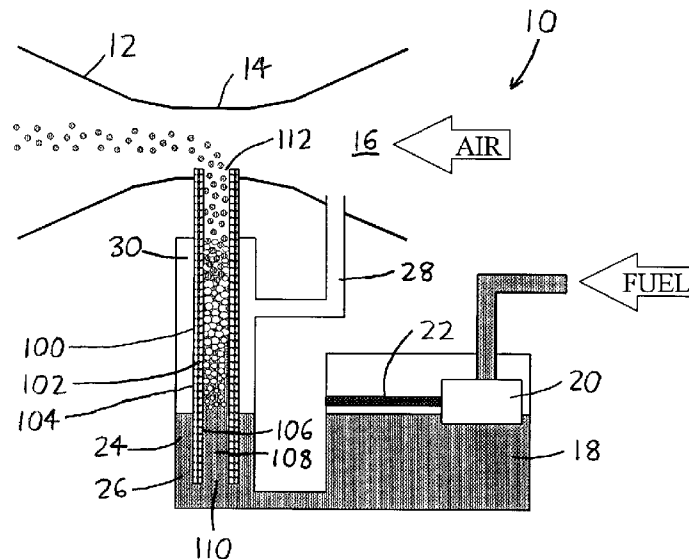
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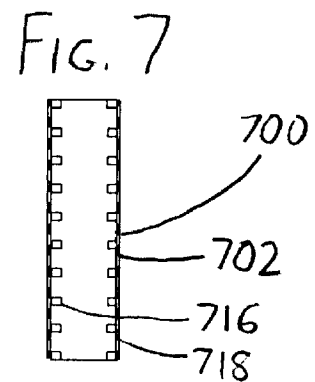
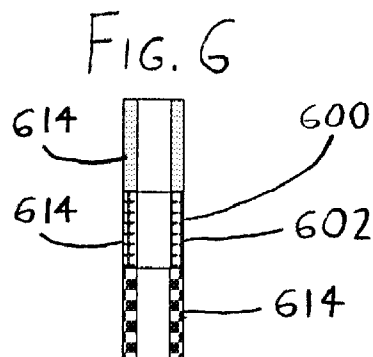
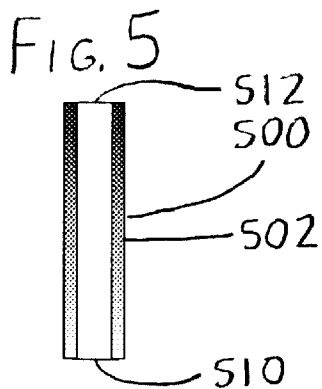
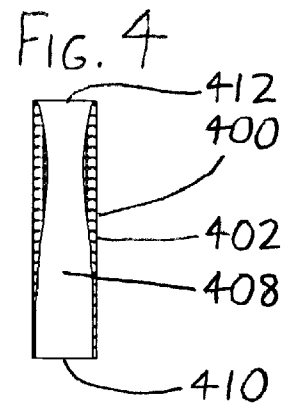
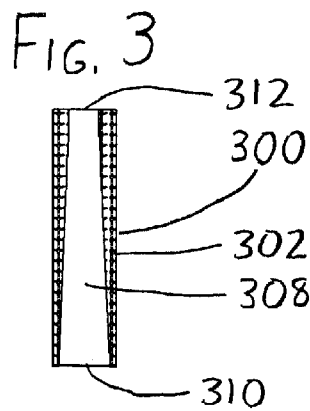
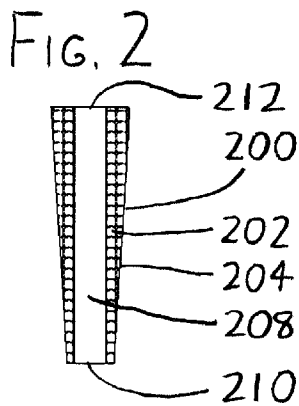
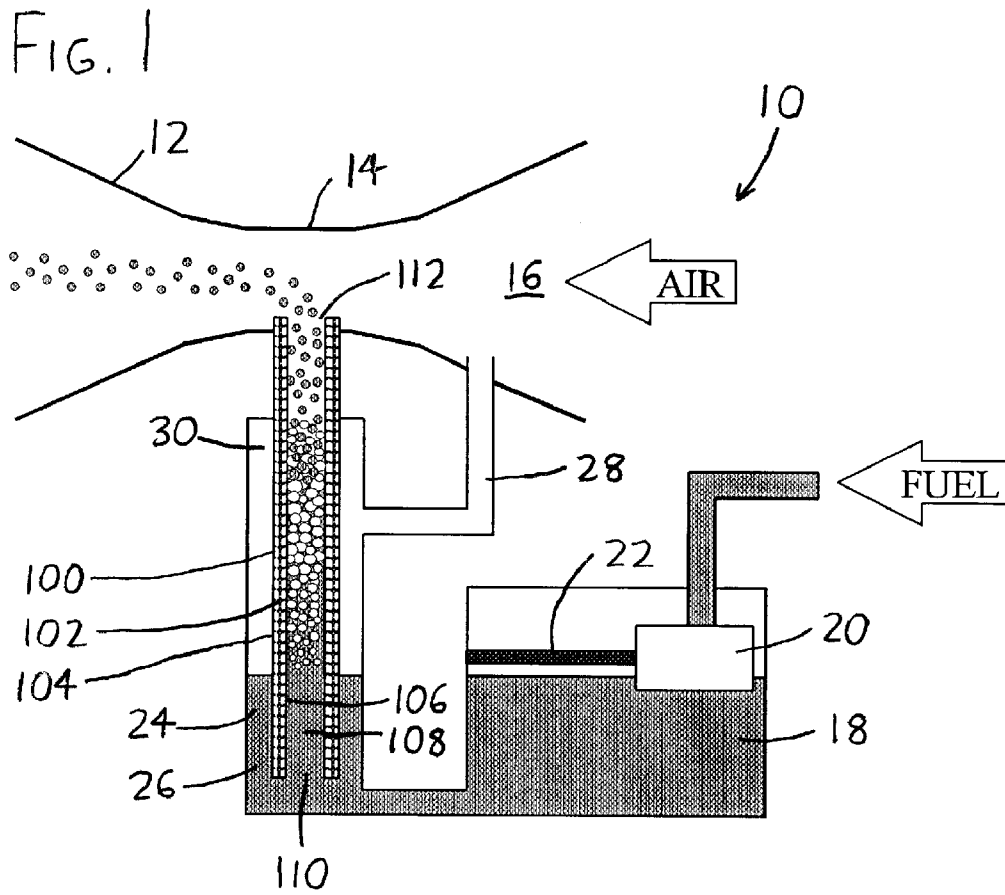
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(57) **ABSTRACT**

An emulsion tube for a carburetor is formed with a porous wall surrounding an inner passage, wherein air travels about one side of the wall and fuel travels about the opposite side, with air being supplied through the pores to aerate the fuel (with the aerated fuel then being expelled into a venturi wherein engine intake air is traveling to further mix the fuel with the intake air therein). The emulsion tube can beneficially provide a high degree of fuel/air mixing across the entire range of intake airstream flow rates at which an engine may operate. The porosity of the emulsion tube can also be tailored to provide the desired fuel/air ratio(s) across the engine's operational range of intake airstream flow rates.

22 Claims, 1 Drawing Sheet





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ENGINE CARBURETION**STATEMENT REGARDING FEDERALLY
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This invention was made with United States government support awarded by the following agencies:

NSF Grant No(s): 0134510

The United States has certain rights in this invention.

FIELD OF THE INVENTION

This document concerns an invention relating generally to carburetors, and more specifically to emulsion tubes for carburetors.

BACKGROUND OF THE INVENTION

Spark ignition (SI) engines, wherein fuel and air are provided to a cylinder and ignited by a spark, have conventionally been provided with fuel and air by either carburetion or by fuel injection. In fuel injection, one or more injectors squirt fuel into the cylinder(s) of the engine, and/or into the cylinder air intake port(s), with the object of atomizing the fuel and mixing it with the air to better enable ignition of the fuel. In carburetion, fuel is supplied into the intake airstream entering the engine and its cylinders, generally at a venturi (a necked passage) which generates suction to pull fuel into the intake airstream in accordance with the flow rate of the intake airstream. Since the air/fuel mixture has a major impact on engine performance and pollutant emissions, the goal of both carburetion and fuel injection is to attain the desired fuel-air mixture at the desired time within the engine cylinder(s). Carburetion systems have the advantage of being rather easily and inexpensively manufactured, but they have the disadvantage that they offer only crude control over the degree of air/fuel mixing, the air/fuel ratio, and the timing of the air/fuel charge entering the cylinder(s). As a result, carburetors tend to offer lesser fuel economy and greater pollutant emissions than fuel injection systems, which is why many modern SI engines (e.g., automotive SI engines) use fuel injection. However, in some applications—in particular for small engines (which are typically regarded as engines having an output of less than 25 horsepower)—carburetion is still commonly used simply because the cost of implementing fuel injection in small engine applications (e.g., lawnmowers, snowthrowers, chainsaws, and other small tools and vehicles) would increase their costs to levels unaffordable to many consumers. Thus, small engines have a reputation (often deserved) for being “dirty” and inefficient. It would therefore be useful to have means available for efficiently and economically enhancing carburetion quality so as to reduce these disadvantages.

SUMMARY OF THE INVENTION

The invention, which is defined by the claims set forth at the end of this document, is directed to emulsion tubes for carburetors (and to carburetors incorporating such emulsion tubes) which at least partially alleviate the aforementioned problems. To give the reader a basic understanding of the invention, following is a brief summary of an exemplary version of the invention, with the summary referring to the accompanying drawings. Since this is merely a summary, it should be understood that more details regarding the preferred versions may be found in the Detailed Description set forth elsewhere in this document. The claims set forth at the

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end of this document then define the various versions of the invention in which exclusive rights are secured.

Looking to FIG. 1, which presents a schematic view of a section of an exemplary carburetor **10** for an internal combustion engine, a venturi **12** has a narrowed throat **14** through which intake air flows from an air supply **16** to enter the intake valves of the engine (with neither the engine nor the valves being depicted). The carburetor **10** also includes a fuel supply **18** which may receive fuel from a source such as a fuel tank, with fuel here being metered into the fuel supply **18** via a float **20** mounted on a spring **22**. An emulsion tube **100** then extends within a well **24** from the fuel supply **18** to the venturi **12**, and it includes an elongated tubular body **102** having an outer surface **104**, an opposing inner surface **106** surrounding an inner passage **108**, and opposing first and second openings **110** and **112** between which the inner passage **108** extends. The inner passage **108** of the emulsion tube **100** communicates fuel from the lower portion **26** of the well **24** (and from the fuel supply **18**) to the venturi **12**, with the low pressure within the venturi **12** pulling fuel from the fuel supply **18** so that the fuel may be carried by the intake air into the engine. A high-pressure air passage **28** can be provided which leads from a high-pressure area in the intake airstream path, e.g., an area situated upstream from the narrowed throat **14** of the venturi **12**, to the upper portion **30** of the well **24** and to an area of the tubular body **102** between its first and second openings **110** and **112**. As a result, the high-pressure air at the upper portion **30** of the well **24** assists in pushing fuel through the emulsion tube **100** to the venturi **12**.

Thus far, such an arrangement is relatively conventional. An objective of this arrangement is to provide a fuel flow rate which is roughly proportional to the intake airstream flow rate, so as to provide a relatively constant air-fuel ratio regardless of the engine speed and the resulting intake airstream flow rate. However, owing to the compressibility of air and other factors, a desired air-fuel ratio can be difficult to obtain across the engine's operational range of intake airflow rates. To compensate for these factors, the emulsion tube **100** may have one or more holes drilled from its outer surface **104** to its inner passage **108** along the upper portion of the well **24**, with the holes accepting air from the high-pressure air passage **28** into the fuel stream traveling in the inner passage **108**. When such holes are properly sized and spaced, they can assist in tailoring the fuel-air ratio as desired across the range of intended engine intake airstream flow rates. Emulsion tubes of this nature still tend to suffer from the disadvantage that they fail to attain the desired degree of mixing across at least a portion of the engine's operational range of intake airstream flow rates, with the fuel leaving the emulsion tube as a trailing stream or as large droplets rather than as a finely-atomized spray. This often occurs at least in part because the two-phase gas/liquid flow in the emulsion tube tends to transition between distinctly different types of flow as the flow rate changes from low to high (e.g., between known two-phase flow regimes such as dispersed bubble flow, churn flow, annular flow, bridging flow, slug flow, etc.), and certain flow regimes result in good atomization whereas others do not. Poorly-dispersed fuel can then lead to further ill effects; for example, the exiting fuel droplets/streams may impinge on the walls of the venturi and pool downstream from the emulsion tube, with fuel dripping off of the venturi and entering the engine cylinder(s) at irregular times. Thus, even though a desired amount of fuel may be exiting the emulsion tube, it may not result in the desired air/fuel mixture actually entering the engine cylinder(s). Further, the nonuniform mixing of the air/fuel mixture accepted into the cylinder(s), arriving as a collection of large amorphous droplets or other agglomera-

tions of fuel rather than as a more homogeneous atomized spray, can lead to less efficient combustion and greater pollutant emissions.

The invention at least partially overcomes these drawbacks by forming at least a portion of the tubular body **102** of the emulsion tube **100** of porous material such as sintered metal, with multiple pores extending through the tubular body **102** from the outer surface **104** to the inner surface **106** to open upon the inner passage **108**. The pores preferably have an average diameter of less than about 0.5 mm, and more preferably less than about 100 micrometers (0.1 mm). So long as such pores are adjacent the upper portion of the well **24** (the portion supplied by the high-pressure air passage **28**), air will enter the fuel stream traveling along inner passage **108** of the tubular body **102** and aerate it. This has been found to result in extremely good atomization of the fuel stream, with the fuel stream exiting the tubular body **102** as a foamy and far more homogeneous mixture.

It may then be necessary to configure the tubular body **102** of the emulsion tube **100**, and/or to tailor its porosity, so that the air-fuel ratio has the desired relationship with respect to the intake airstream flow rate in the venturi **12** (e.g., to obtain a relatively constant air-fuel ratio across the operational range of intake airstream flow rates). This can be done, for example, in the manner of the emulsion tube **200** of FIG. 2, wherein the porous tubular body **202** is configured with a thickness which varies along its length, and thereby has a varying pressure drop between its outer surface **204** and its inner passage **208**. Here, assuming the porous tubular body **202** has uniform porosity, circumferential admittance of air and/or fuel is greater nearer the first opening **210** owing to lesser thickness of the tube (and thus a lower pressure drop across the tube wall). FIG. 3 illustrates a similar arrangement, but here the inner passage **308** has varying diameter, unlike the arrangement of FIG. 2 where the outer surface **204** varies in diameter while the inner passage **208** remains constant. The arrangement of FIG. 3 can have the further effect of accelerating the air-fuel mixture as it travels from the first opening **310** to the second opening **312** (or decelerating the air-fuel mixture, if the tubular body **302** is installed with the second opening **312** in the venturi **12**), and at the same time the emulsion tube **300** is more amenable to retrofitting within preexisting carburetors which might not accept an externally tapered emulsion tube (as with the emulsion tube **200** of FIG. 2). Other more complex configurations are also possible, as exemplified by FIG. 4, wherein the tubular body **402** of the emulsion tube **400** starts with a relatively uniform tube thickness near its first opening **410**, with the inner passage **408** then necking inwardly before expanding outwardly at the second opening **412**.

Alternatively and/or additionally, the pore sizes and/or densities may vary at different locations along the length of the tubular body. For example, FIG. 5 illustrates an emulsion tube **500** having tube wall pressure drops similar to those of the emulsion tubes **200** and **300**, with greater pore density and/or greater average pore diameter nearer the first opening **510**, and decreasing density and/or pore diameter approaching the opposing second opening **512**. Such variable-porosity tubes can be manufactured, for example, by sintering together particles whose diameters vary in accordance with their location along the length of the tube (e.g., larger diameter particles, and thus larger pores, near the first opening **510**, and smaller diameter particles, and thus smaller pores, near the second opening **512**). Since variable-porosity tubes can be difficult and expensive to construct, an alternative arrangement is illustrated in FIG. 6, wherein the emulsion tube **600** is formed of a tubular body **602** in three joined axially-aligned

sections **614** which are substantially identical save for their porosity (i.e., they each have different average pore sizes and/or densities, for example, the sections **614** might have pore sizes which increase by 3 micrometers or more with each successive section **614**). In this case, porosity varies discretely rather than continuously over the length of the tubular body **602**.

The porous emulsion tube **100** has been found in experiments to result in generation of a foamy "bubbly flow" across the entire operating range of air intake flow rates of common carburetors, with a very well-mixed emulsion at the exit of the emulsion tube **100**, one which is far superior to that produced with conventional prior emulsion tubes. Further, with appropriate tailoring of the porosity of the emulsion tube **100** (as dictated by flow modeling, computerized simulation, and/or by trial and error), the emulsion tube **100** can be made to provide a linear (or other) relationship between fuel flow and air intake flow, as in conventional emulsion tubes. Further features and advantages of the invention will be apparent from the remainder of this document in conjunction with the associated drawings.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a schematic view of a cross-section of a carburetor **10** incorporating a porous emulsion tube **100** which exemplifies the invention, wherein the emulsion tube **100** extends from a fuel supply **18** to a venturi **12**, with a section of the emulsion tube **100** between its first opening **110** and second opening **112** being exposed to an air supply **16**.

FIG. 2 is a schematic view of a cross-section of another porous emulsion tube **200** exemplifying the invention, wherein the outer diameter of the emulsion tube **200** varies between its first opening **210** and second opening **212** to provide variable resistance to air and/or fuel admittance along its length.

FIG. 3 is a schematic view of a cross-section of another porous emulsion tube **300** exemplifying the invention, wherein the diameter of the inner passage **308** of the emulsion tube **300** varies linearly between its first opening **310** and second opening **312** to provide variable resistance to air and/or fuel admittance along its length.

FIG. 4 is a schematic view of a cross-section of another porous emulsion tube **400** exemplifying the invention, wherein the diameter of the inner passage **408** of the emulsion tube **400** varies nonlinearly between its first opening **410** and second opening **412** to provide variable resistance to air and/or fuel admittance along its length.

FIG. 5 is a schematic view of a cross-section of another porous emulsion tube **500** exemplifying the invention, wherein the porosity of its tubular body **502** varies in pore size and/or density between its first opening **510** and second opening **512** to provide variable resistance to air and/or fuel admittance along its length.

FIG. 6 is a schematic view of a cross-section of another porous emulsion tube **600** exemplifying the invention, wherein the tubular body **602** of the emulsion tube **600** is formed in discrete sections **614**, each having a different average pore size and/or density, to provide variable resistance to air and/or fuel admittance along the length of the tubular body **602**.

FIG. 7 is a schematic view of a cross-section of another porous emulsion tube **700** exemplifying the invention, wherein the tubular body **702** is formed of a mesh lattice/framework **716** with a porous skin **718** wrapped about the framework **716**.

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DETAILED DESCRIPTION OF PREFERRED
VERSIONS OF THE INVENTION

Expanding on the foregoing discussion, it should be understood that the various versions of the invention discussed above are merely exemplary, and the invention includes other variations as well. As an example, the tubular body of the emulsion tube need not necessarily be formed of metal, and could instead be formed of (for example) ceramic, or potentially even plastic (provided such plastic can withstand engine temperatures and prolonged exposure to fuel). Emulsion tubes made of more than one material, and/or composite structures, are also a possibility, e.g., an emulsion tube having a sintered metal entryway and a plastic section extending into the venturi, or having a ceramic entryway and a metal section extending into the venturi. FIG. 7 illustrates an emulsion tube **700** of this nature wherein a tubular lattice/framework **716** (e.g., one made of metal or plastic) is wrapped with a porous textile skin **718** (e.g., one made of carbon or glass fiber), with the skin **718** being bonded to the framework. Moreover, porosity may be made to vary about the outer skin **718** by varying its weave, and/or by stretching/elongating parts of the textile, so that the pores/spaces between adjoining fibers vary as desired. It should also be understood that the pores need not be present upon initial manufacture of the tubular body of the emulsion tube; for example, they might be formed via laser machining after the tubular body is initially molded, cast, or otherwise formed.

The various foregoing emulsion tubes can incorporate other features as well, e.g., protruding threading or teeth, and/or sockets or other indentations, which allow the emulsion tubes to be firmly installed within (and readily removed from) the carburetor. As an example, some carburetors utilize emulsion tubes having threaded ends which screw into sockets for easy installation of the emulsion tubes. An appropriately designed emulsion tube in accordance with the present invention might be formed to be threaded into such sockets as a replacement for conventional emulsion tubes.

As noted previously, the pores preferably have an average diameter of less than 100 micrometers. By this it should be understood that some pores may have diameters of greater than 100 micrometers and some may have diameters of less than 100 micrometers, but when all diameters are averaged together, they are preferably less than 100 micrometers. Experiments with a sintered bronze tubular body have found that good results arise with pore sizes on the order of about 20 micrometers (on average), but since only limited experimentation has been conducted as of the date that this document was first prepared, this should not be construed as suggesting that other sizes might not work as well. It is believed that pore diameters of less than 50 micrometers (and more specifically at ranges of around 10-40 micrometers) may be particularly useful.

The carburetor **10** in FIG. 1 is merely a simplified exemplary carburetor, and it should be understood that emulsion tubes in accordance with the invention may be used in a wide variety of carburetors having vastly different configurations, including those of the type wherein air is supplied through the inner passage of the emulsion tube to aerate a surrounding body of fluid. The configuration of the emulsion tube may also vary; for example, it need not necessarily extend along a linear path, nor need it have a circular cross-section, though such configurations are preferred since conventional emulsion tubes generally have these features.

In addition, while the invention was previously described as being preferred for use in small SI engines, the invention is not limited to such uses. As an evident example, the invention

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is readily usable in large SI engines, though the current trend is away from the use of carburetion (and toward fuel injection) in such engines. The invention may also be used for carburetion in non-SI engines and other engines/motors. For example, many gas turbine engines have carburetion systems wherein emulsion tubes—which, in the gas turbine context, are more often referred to as atomizers, injectors, or injection nozzles—provide fuel to a supply of air leading to the combustion chamber/passage, and the invention is suitable for use in these types of carburetors as well.

The invention is not intended to be limited to the preferred versions of the invention described above, but rather is intended to be limited only by the claims set out below. Thus, the invention encompasses all different versions that fall literally or equivalently within the scope of these claims.

What is claimed is:

1. A carburetor for an engine including an emulsion tube with an elongated tubular body, the tubular body having an outer surface, an opposing inner surface surrounding an inner passage, and opposing first and second openings between which the inner passage extends, wherein at least a portion of the tubular body is porous, with

- a. multiple pores extending between the inner surface and outer surface, and
- b. the pores having an average diameter of less than about 100 micrometers.

2. The carburetor of claim **1** wherein the thickness of the tubular body, as measured between its inner and outer surfaces, is greater at the second opening than at the first opening.

3. The carburetor of claim **2** wherein the outer surface decreases in diameter between the first opening and the second opening.

4. The carburetor of claim **1** wherein the average diameters of the pores decrease over the tubular body as it extends from its first opening to its second opening.

5. The carburetor of claim **1** wherein the tubular body is formed of two or more axially aligned tubes situated in abutment.

6. The carburetor of claim **5** wherein at least two of the tubes have pores of different average diameter, with one of the tubes having an average pore diameter at least 3 micrometers greater than the average pore diameter of an adjacent tube.

7. The carburetor of claim **1** wherein the pores have an average diameter of less than 50 micrometers.

8. The carburetor of claim **1** wherein the pores have diameters between 10-40 micrometers.

9. The carburetor of claim **1** wherein the tubular body is at least partially formed of sintered metal.

10. The carburetor of claim **1** further including:

- a. a fuel supply situated at one of the first and second openings, and
- b. an air supply about at least a portion of the outer surface, wherein the air supply is at an air pressure such that air is urged from the outer surface into the inner passage.

11. The carburetor of claim **1** further including a fuel supply and a venturi having a narrowed throat, wherein the inner passage of the tubular body extends between the venturi and the fuel supply with the first opening receiving fuel from the fuel supply and the second opening supplying fuel to the venturi.

12. The carburetor of claim **11** wherein:

- a. the second opening of the tubular body opens onto the narrowed throat of the venturi, and
- b. the carburetor further includes a high-pressure air passage leading between:

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- (1) an area of the tubular body between its first and second openings, and
- (2) a high-pressure area situated upstream or downstream from the narrowed throat of the venturi.

13. The carburetor of claim 12 wherein the outer surface of the tubular body has lesser diameter at the first opening than at the second opening.

14. The carburetor of claim 12 wherein the average diameters of the pores vary in relation to their distance from the first opening.

15. The carburetor of claim 12 wherein the tubular body is formed in two or more tubular sections, wherein at least one of the tubular sections has an average pore diameter which is at least 3 micrometers greater than the average pore diameter of an adjacent tubular section.

16. The carburetor of claim 12 wherein the pores have an average diameter of less than 100 micrometers.

17. The carburetor of claim 12 further comprising:

- a. a fuel supply supplying fuel to the emulsion tube, and
- b. an air supply supplying air between the inner surface and the outer surface of the tubular body of the emulsion tube.

18. The carburetor of claim 12 further including a fuel supply and a venturi having a narrowed throat, wherein the first opening of the tubular body is in fluid communication with the fuel supply and the second opening of the tubular body is in fluid communication with the venturi.

19. The carburetor of claim 17 wherein the pores in the tubular body have an average diameter of less than 0.5 mm.

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20. The carburetor of claim 17 wherein the pores in the tubular body have an average diameter of less than about 100 micrometers.

21. A carburetor for an engine including an emulsion tube with an elongated tubular body, the tubular body having an outer surface, an opposing inner surface surrounding an inner passage, and opposing first and second openings between which the inner passage extends, wherein at least a portion of the tubular body is formed of sintered material having pores extending between the inner surface and outer surface, with the pores having an average diameter of less than 0.5 mm.

22. A carburetor for an engine including:

- a. a venturi having a narrowed throat,
- b. a fuel supply,
- c. an air supply,
- d. a sintered metal emulsion tube with an elongated tubular body, the tubular body having an outer surface and an opposing inner surface surrounding an inner passage, wherein:
 - (1) the inner passage extends between a first opening in fluid communication with the fuel supply and a second opening in fluid communication with the venturi,
 - (2) pores extend through the tubular body from the outer surface to the inner surface to open upon the inner passage, and
 - (3) the air supply is situated about at least a portion of the outer surface, and is at a pressure sufficient to urge air through the outer surface and into the inner passage.

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