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(54) **(20R,25S)-2-METHYLENE-19,26-DINOR-1 α ,25-DIHYDROXYVITAMIN D₃ IN CRYSTALLINE FORM**

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(58) **Field of Classification Search** 514/167;
552/653

See application file for complete search history.

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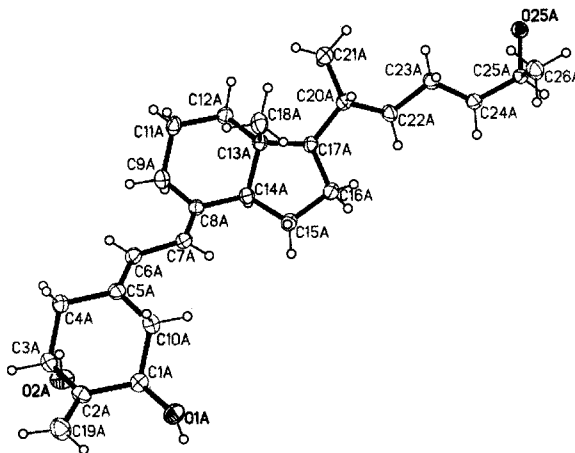
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(57) **ABSTRACT**

A method of purifying (20R,25S)-2-methylene-19,26-dinor-1 α ,25-dihydroxyvitamin D₃ to obtain (20R,25S)-2-methylene-19,26-dinor-1 α ,25-dihydroxyvitamin D₃ in crystalline form. The method includes the steps of preparing a solvent of methanol and water, dissolving a product containing (20R,25S)-2-methylene-19,26-dinor-1 α ,25-dihydroxyvitamin D₃ to be purified in the solvent, cooling the solvent and dissolved product below ambient temperature for a sufficient amount of time to form a precipitate of (20R,25S)-2-methylene-19,26-dinor-1 α ,25-dihydroxyvitamin D₃ crystals, and recovering the (20R,25S)-2-methylene-19,26-dinor-1 α ,25-dihydroxyvitamin D₃ crystals.

16 Claims, 5 Drawing Sheets



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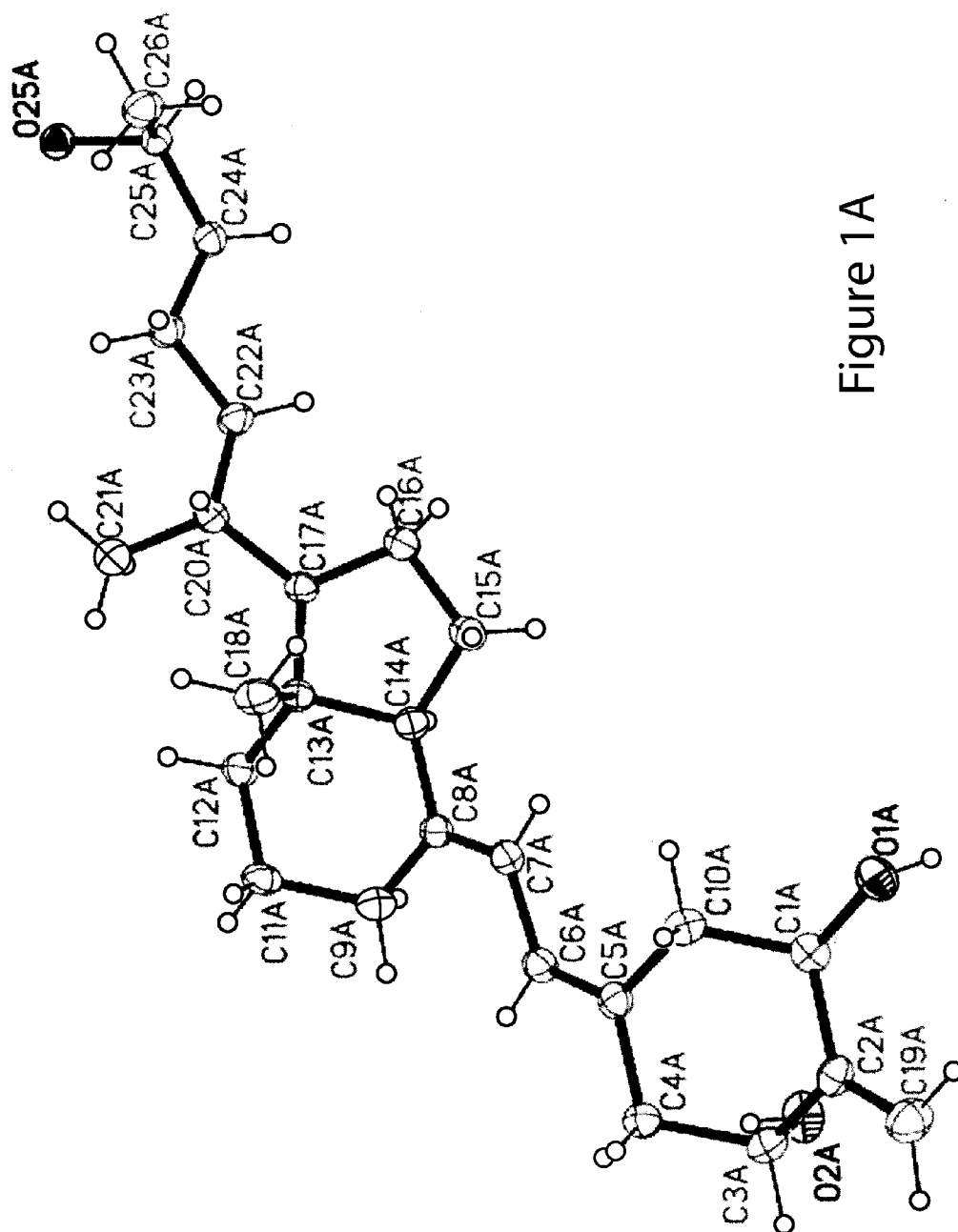


Figure 1A

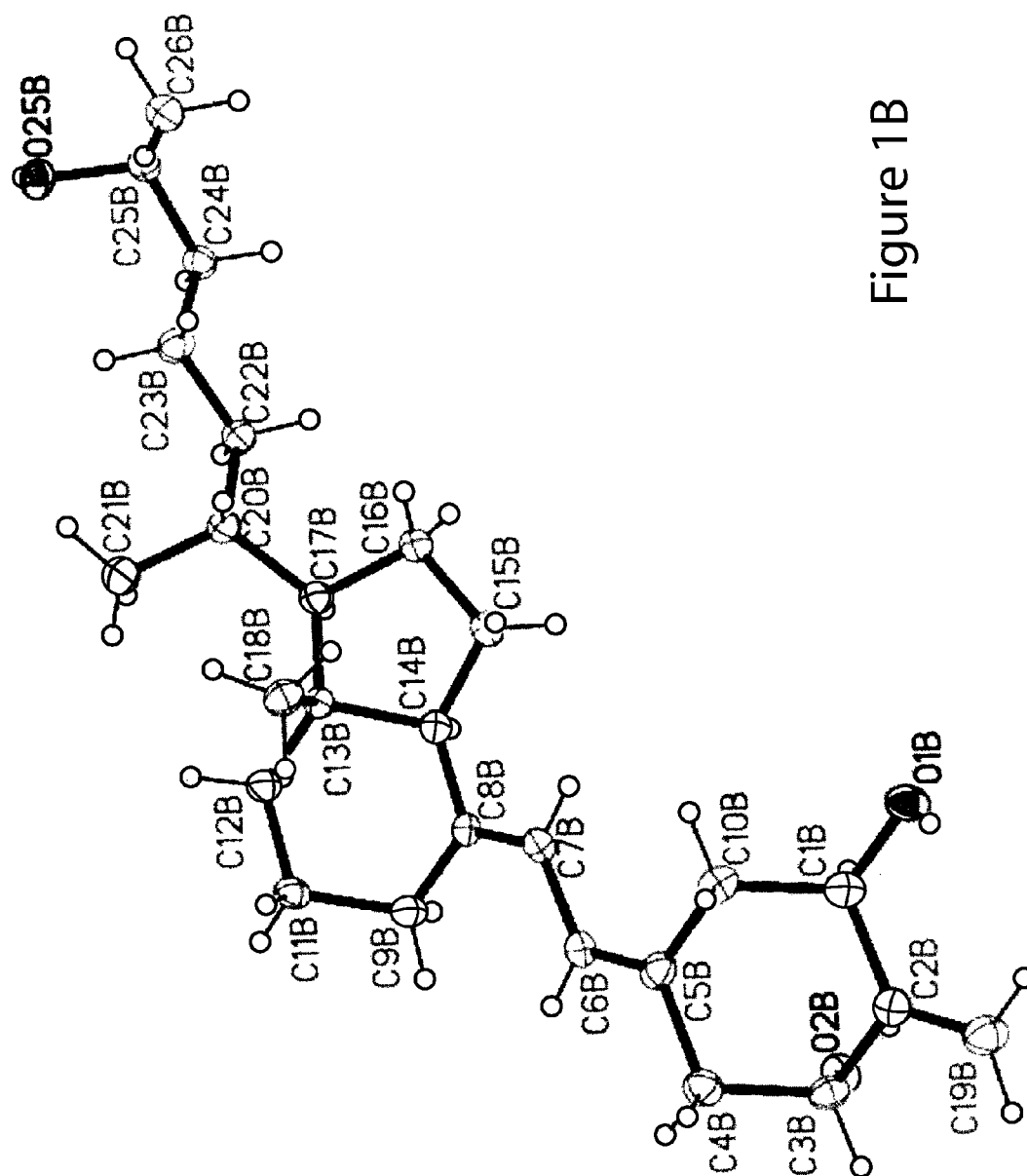


Figure 1B

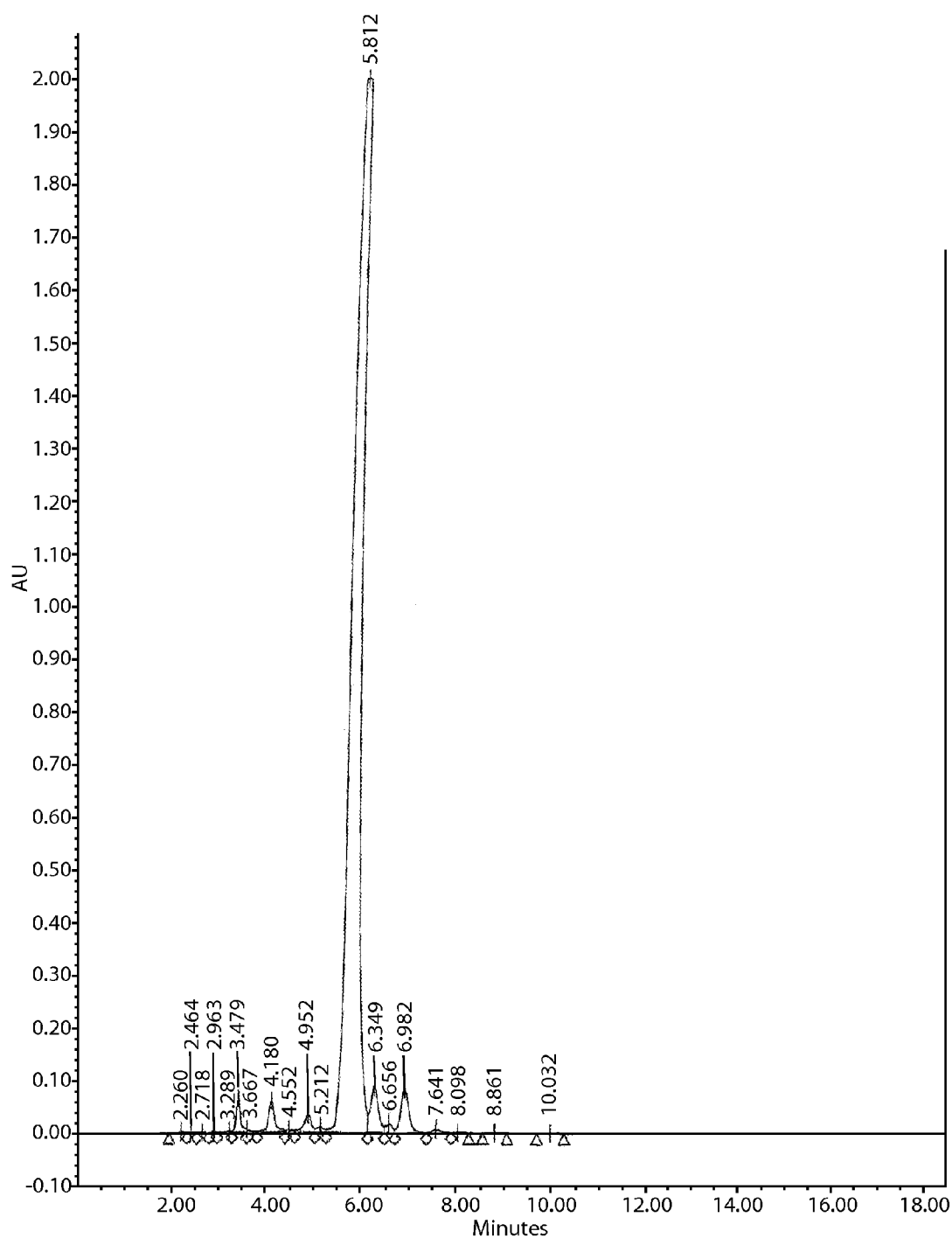


Figure 2

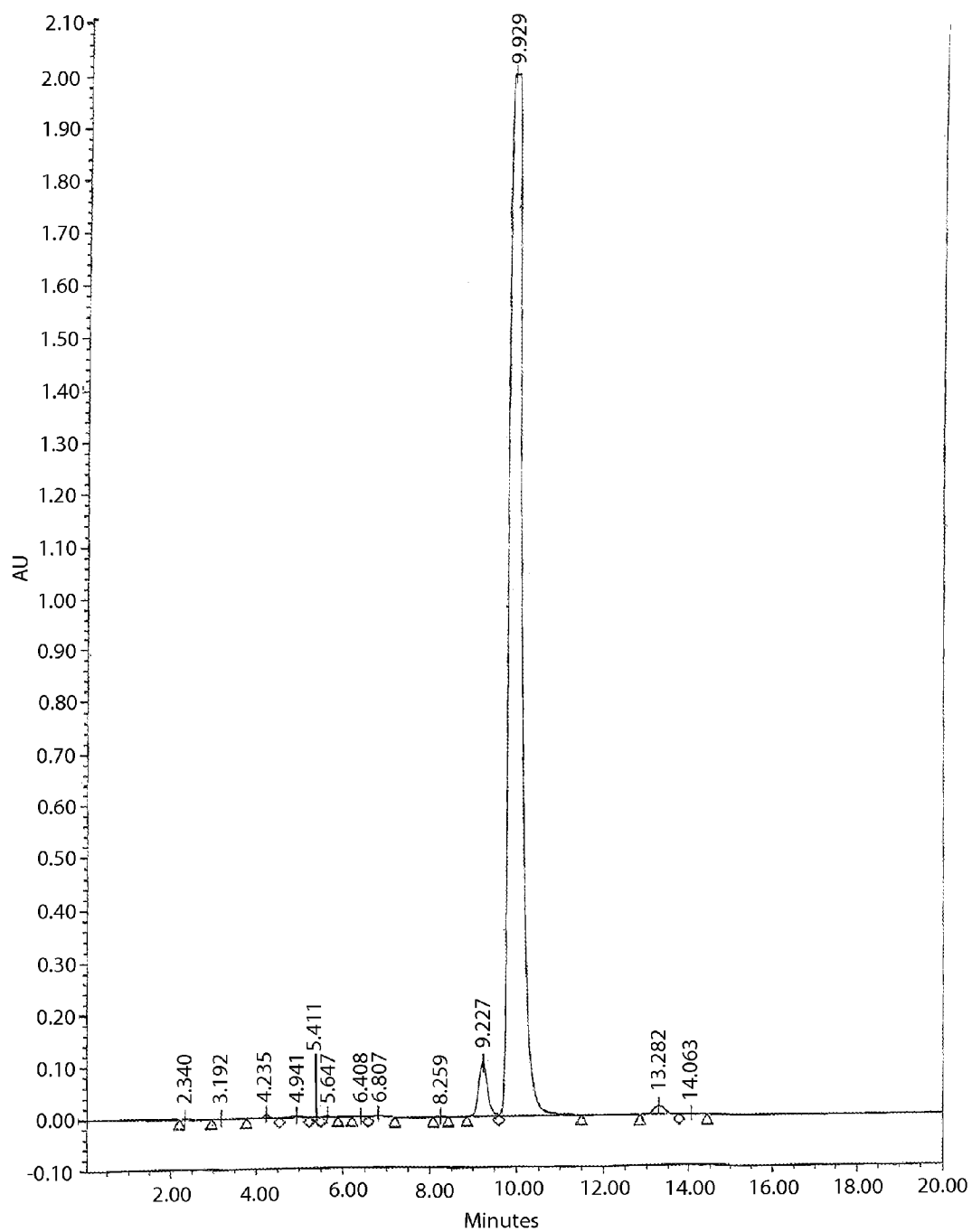


Figure 3

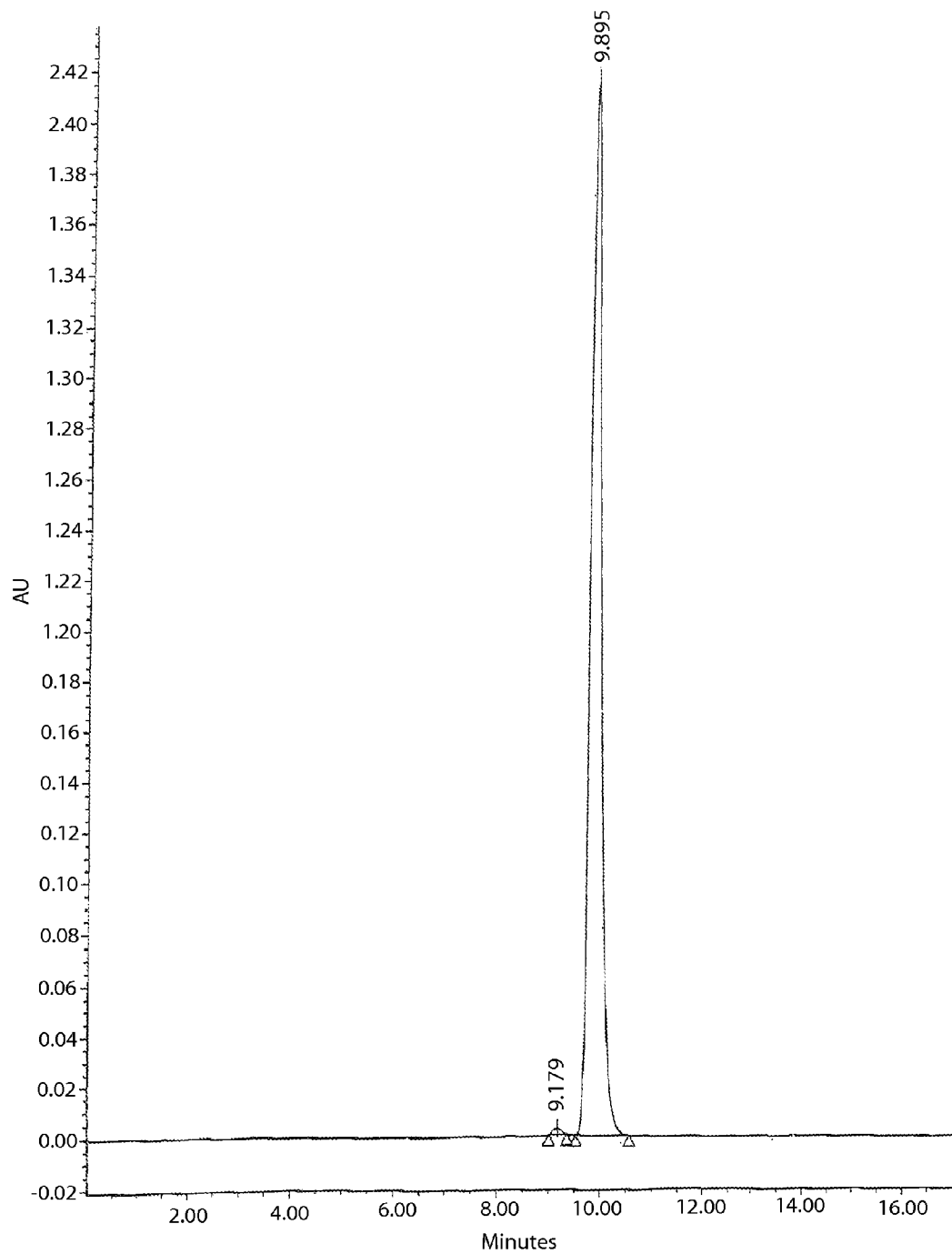


Figure 4

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(20R,25S)-2-METHYLENE-19,26-DINOR-1 α ,25-DIHYDROXYVITAMIN D₃ IN CRYSTALLINE FORM

STATEMENT REGARDING FEDERALLY
SPONSORED RESEARCH OR DEVELOPMENT

This invention was made with government support under DK047814 awarded by the National Institutes of Health. The government has certain rights in the invention.

BACKGROUND OF THE INVENTION

The present invention relates to purification of organic compounds, and more particularly to the purification of (20R, 25S)-2-Methylene-19,26-Dinor-1 α ,25-Dihydroxyvitamin D₃ (referred to herein as "NEL") by preparing it in crystalline form.

Purification of organic compounds, especially those designated for pharmaceutical use, is of considerable importance for chemists synthesizing such compounds. Preparation of the compound usually requires many synthetic steps and, therefore, the final product can be contaminated not only with side-products derived from the last synthetic step of the procedure but also with compounds that were formed in previous steps. Even chromatographic purification, which is a very efficient but relatively time-consuming process, does not usually provide compounds which are sufficiently pure to be used as drugs.

Depending on the method used to synthesize 1 α -hydroxyvitamin D compounds, different minor undesirable compounds can accompany the final product. Thus, for example, if direct C-1 hydroxylation of 5,6-trans geometric isomer of vitamin D is performed, followed by SeO₂/NMO oxidation and photochemical irradiation [see Andrews et al., *J. Org. Chem.* 51, 1635 (1986); Calverley et al., *Tetrahedron* 43, 4609 (1987); Choudry et al., *J. Org. Chem.* 58, 1496 (1993)], the final 1 α -hydroxyvitamin D product can be contaminated with 1 β -hydroxy- as well as 5,6-trans isomers. If the method consists of C-1 allylic oxidation of the 4-phenyl-1,2,4-triazoline-3,5-dione adduct of the previtamin D compound, followed by cycloreversion of the modified adduct under basic conditions [Nevinckx et al., *Tetrahedron* 47, 9419 (1991); Vanmaele et al., *Tetrahedron* 41, 141 (1985) and 40, 1179 (1994); Vanmaele et al., *Tetrahedron Lett.* 23, 995 (1982)], one can expect that the desired 1 α -hydroxyvitamin can be contaminated with the previtamin 5(10), 6,8-triene and 1 β -hydroxy isomer. One of the most useful C-1 hydroxylation methods, of very broad scope and numerous applications, is the experimentally simple procedure elaborated by Paaren et al. [see *J. Org. Chem.* 45, 3253 (1980) and *Proc. Natl. Acad. Sci. U.S.A.* 75, 2080 (1978)]. This method consists of allylic oxidation of 3,5-cyclovitamin D derivatives, readily obtained from the buffered solvolysis of vitamin D tosylates, with SeO₂/t-BuOOH and subsequent acid-catalyzed cycloreversion to the desired 1 α hydroxy compounds. Taking into account this synthetic path it is reasonable to assume that the final product can be contaminated with 1 α -hydroxy epimer, 5,6-trans isomer and the previtamin D form. 1 α -hydroxyvitamin D₄ is another undesirable contaminant found in 1 α -hydroxyvitamin D compounds synthesized from vitamin D₂ or from ergosterol. 1 α -hydroxyvitamin D₄ results from C-1 oxidation of vitamin D₄, which in turn is derived from contamination of the commercial ergosterol material. Typically, the final product may contain up to about 1.5% by weight 1 α -hydroxyvitamin D₄. Thus, a purification technique that would eliminate or substantially reduce the

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amount of 1 α -hydroxyvitamin D₄ in the final product to less than about 0.1-0.2% would be highly desirable.

The vitamin D conjugated triene system is not only heat- and light-sensitive but it is also prone to oxidation, leading to the complex mixture of very polar compounds. Oxidation usually happens when a vitamin D compound has been stored for a prolonged time. Other types of processes that can lead to a partial decomposition of vitamin D compounds consist of some water-elimination reactions; their driving force is allylic (1 α -) and homoallylic (3 β -) position of the hydroxy groups. The presence of such above-mentioned oxidation and elimination products can be easily detected by thin-layer chromatography.

Usually, all 1 α -hydroxylation procedures require at least one chromatographic purification. However, even chromatographically purified 1 α hydroxyvitamin D compounds, although showing consistent spectroscopic data, suggesting homogeneity, do not meet the purity criteria required for therapeutic agents that can be orally, parenterally or transdermally administered. Therefore, it was evident that a suitable method of purification of the 1 α hydroxylated vitamin D compound NEL is required.

SUMMARY OF THE INVENTION

The present invention relates to a method of purifying NEL by means of crystallization to obtain NEL in crystalline form. The solvent plays a crucial role in the crystallization process, and is typically an individual liquid substance or a suitable mixture of different liquids. For crystallizing NEL, the most appropriate solvent and/or solvent system is characterized by the following factors:

- (1) low toxicity;
- (2) low boiling point;
- (3) significant dependence of solubility properties with regard to temperature (condition necessary for providing satisfactory crystallization yield); and
- (4) relatively low cost.

Interestingly, hexane, so frequently used for crystallization purposes, was found less suitable for crystallization of NEL. However, it was found that a mixture of two liquids, namely water and methanol, in amounts of from about 10% water with about 90% methanol to about 30% water with about 70% methanol, was most useful for the crystallization of NEL. In particular, it, was determined that a mixture of 20% water with 80% methanol (by volume) performed well. The water/methanol solvent mixture was also easy to remove by evaporation or other well known methods. In all cases the crystallization process occurred easily and efficiently; and the precipitated crystals were sufficiently large to assure their recovery by filtration or other means.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1A is an illustration of the three dimensional structure of a first asymmetric molecular structure for NEL as defined by the atomic positional parameters discovered and set forth herein;

FIG. 1B is, an illustration of the three dimensional structure of a second asymmetric molecular structure for NEL as defined by the atomic positional parameters discovered and set forth herein;

FIG. 2 is an HPLC (9.4 mm $\times$ 25 cm Zorbax-Sil column, 15% 2-propanol in hexane; 6 mL/min; R_t=5.8 min.) profile of the solid material of NEL compound obtained after chemical

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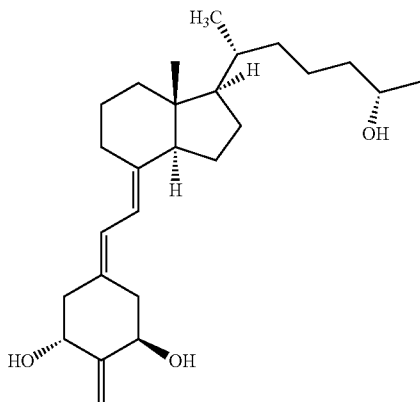
synthesis; purity of the NEL compound before further HPLC purification was found to be 88.9%, checked by straight-phase HPLC;

FIG. 3 is an HPLC (9.4 mm×25 cm Zorbax RX-C18 column, 15% water in methanol; 3 mL/min; R_t =9.9 min.) profile of the NEL compound obtained after a first, straight-phase HPLC purification of the solid NEL material; purity of the NEL compound after this first HPLC purification was found to be 95.3%, checked by reversed-phase HPLC; and

FIG. 4 is an HPLC (9.4 mm×25 cm Zorbax RX-C18 column, 15% water in methanol; 3 mL/min; R_t =9.9 min.) profile of the NEL compound obtained after a second reversed-phase HPLC purification of the NEL compound obtained from the first HPLC purification; purity of the NEL compound after this second HPLC purification was found to be 99.5%, checked by reversed-phase HPLC. Crystals of the NEL compound were obtained after reversed-phase HPLC purification by single crystallization using a 20% water/80% methanol solvent system.

DETAILED DESCRIPTION OF THE INVENTION

The present invention provides (20R,25S)-2-methylene-19,26-dinor-1 α ,25-dihydroxyvitamin D₃ (NEL) in crystalline form, a pharmacologically important compound, characterized by the formula I shown below:



The present invention also provides a valuable method of purification of NEL. The purification technique involves obtaining the NEL product in crystalline form by utilizing a crystallization procedure wherein the NEL material to be purified is dissolved using as the solvent a mixture comprised of methanol and water in amounts of from about 10% water with about 90% methanol to about 30% water with about 70% methanol, by volume. Preferably the mixture comprises 80% methanol and 20% water (by volume). The solvent and dissolved product containing (20R,25S)-2-methylene-19,26-dinor-1 α ,25-dihydroxyvitamin D₃ (NEL) to be purified may then be cooled to about -20° C., or may in a first step be maintained at ambient temperature for a period of time (1 hour to 1 week) and then cooled in a second step to about -20° C. In either case, the solution is then maintained at about -20° C. for up to 7 weeks. Thereafter, the solvent can be removed by evaporation, with or without vacuum, or other means as is well known, or the resultant crystals may be filtered from the mother liquor. The technique can be used to purify a wide range of final products containing NEL obtained from any known synthesis thereof, and in varying concentrations, i.e.

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from microgram amounts to kilogram amounts. As is well known to those skilled in this art, the amount of solvent utilized should be minimized and/or adjusted according to the amount of NEL to be purified.

The usefulness and advantages of the present crystallization procedure is shown in the following specific Examples 1 and 2. After crystallization, the precipitated material was observed under a microscope to confirm its crystalline form. Additionally, the crystals were then analyzed to determine their initial purity (88.9%; FIG. 2), and their significantly improved purity was confirmed after a first, straight-phase HPLC (95.3%, FIG. 3), as well as a second, reversed-phase HPLC (99.5%; FIG. 4). Yields of crystals were high and the obtained crystals showed a relatively sharp melting point of 154-155° C.

The described crystallization process of the synthetic NEL product represents a valuable purification method, which can remove most side products derived from the synthetic path. Such impurity is the result of the contamination of starting raw materials. The crystallization process occurred easily and efficiently; and the precipitated crystals were sufficiently large to assure their recovery by filtration, or other means.

EXAMPLE 1

Crystallization of (20R,25S)-2-methylene-19,26-dinor-1 α ,25-dihydroxyvitamin D₃ (NEL)

Crystals of the NEL analog were obtained from a solution of the compound in 20% water and 80% methanol (20% H₂O/80% MeOH) as follows:

14 mg of pure NEL compound was dissolved in 8 mL of water/methanol solvent mixture (water/methanol=2/8). The solution was kept at -20 degrees Celsius for 7 weeks. The precipitated crystals (M.p. 154-155° C.) were analyzed by straight phase HPLC (crystals: FIG. 2) and found to be 99.5% pure.

EXAMPLE 2

Experimental

A colorless prism-shaped crystal of dimensions 0.47×0.12×0.18 mm was selected for structural analysis. Intensity data were collected using a Bruker AXS Platinum 135 CCD detector controlled with the PROTEUM software suite (Bruker AXS Inc., Madison, Wis.). The x-ray source was CuK α radiation (1.54178 Å) from a Rigaku RU200 x-ray generator equipped with Montel optics, operated at 50 kV and 80 mA. The x-ray data were processed with SAINT version 7.06A (Bruker AXS Inc) and, internally scaled with SADABS version 2005/1 (Bruker AXS Inc.). The sample was mounted on a glass fiber using vacuum grease and cooled to 100° K. The intensity data were measured as a series of phi and omega oscillation frames each of 1° for 10-15 sec/frame. The detector was operated in 1024/1024 mode and was positioned 4.5 cm from the sample. Cell parameters were determined from a non-linear least squares fit of 9999 peaks in the range of 3.0<theta<64.8°. The data were merged to form a set of 6791 independent data with R(int)=0.0326.

The triclinic space group P1 was determined by systematic absences and statistical tests and verified by subsequent refinement. The structure was solved by direct methods, and refined by full matrix least-squares methods on F², (a) G. M. Sheldrick (1994), SHELXTL Version 5 Reference Manual, Bruker AXS Inc.; (b) *International Tables for Crystallography, Vol. C*, Kluwer: Boston (1995). The asymmetric unit was

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comprised of two molecules of NEL, designated with A and B. Hydrogen atom positions were determined from difference peaks and ultimately refined by a riding model with idealized geometry. Non-hydrogen atoms were refined with anisotropic displacement parameters. A total of 523 parameters were refined against 3 restraints and 6781 data to give $wR^2=0.0943$ and $S=1.066$ for weights of $w=1/[s^2(F^2)+(0.0613P)^2]$, where $P=[F^2+2F_c^2]/3$. The final $R(F)$ was 0.0342 for the 6781 observed data. The largest shift/s.u. was 0.001 in the final refinement cycle and the final difference map had maxima and minima of 0.217 and $-0.177\text{ e}/\text{\AA}^3$, respectively. The absolute structure was determined by refinement of the Flack parameter, H. D. Flack, *Acta Cryst. A*, vol. 39, 876-881 (1983).

The three dimensional structure of NEL as defined by the following physical data and atomic positional parameters described and calculated herein is illustrated in FIG. 1A and FIG. 1B.

TABLE 1

Crystal data and structure refinement for NEL.	
Identification code	NEL
Empirical formula	C ₂₆ H ₄₂ O ₃
Formula weight	402.60
Temperature	100(1) K
Wavelength	1.54178 Å
Crystal system, space group	P1,
Unit cell dimensions	a = 6.3820(11) Å $\alpha = 110.920(5)^\circ$ b = 12.594(2) Å $\beta = 95.256(5)^\circ$ c = 15.996(3) Å $\gamma = 90.609(5)^\circ$
Volume	1194.6(4) Å ³
Z, Calculated density	2, 1.119 Mg/m ³
Absorption coefficient	0.549 mm ⁻¹
F(000)	444
Crystal size	0.47 × 0.12 × 0.18 mm
Theta range for data collection	2.97 to 64.82°
Limiting indices	-7 ≤ h ≤ 7, -14 ≤ k ≤ 14, -18 ≤ l ≤ 18
Reflections collected/unique	18206/6781 [R(int) = 0.0326]
Completeness to theta = 64.82	96.0%
Refinement method	Full-matrix least-squares on F ²
Data/restraints/parameters	6781/3/523
Goodness-of-fit on F ²	1.066
Final R indices [I > 2σ(I)]	R1 = 0.0336, wR2 = 0.0943
R indices (all data)	R1 = 0.0342, wR2 = 0.0948
Absolute structure parameter	-0.04(13)
Largest diff. peak and hole	0.217 and $-0.177\text{ e}/\text{\AA}^3$

TABLE 2

Atomic coordinates ($\times 10^4$) and equivalent isotropic displacement parameters ($\text{\AA}^2 \times 10^3$) for NEL. U(eq) is defined as one third of the trace of the orthogonalized Uij tensor.				
	x	y	z	U(eq)
O(1B)	20004(2)	17550(1)	1623(1)	24(1)
O(25A)	17814(2)	15531(1)	1308(1)	22(1)
O(1A)	17343(2)	13368(1)	9956(1)	25(1)
O(2B)	26264(2)	18348(1)	1150(1)	24(1)
O(25B)	24669(2)	16177(1)	10298(1)	25(1)
O(2A)	23666(2)	12775(1)	10464(1)	30(1)
C(12B)	29763(3)	18997(2)	6571(1)	21(1)
C(3B)	24736(3)	19211(2)	1351(1)	21(1)
C(14A)	22676(3)	13599(2)	6215(1)	20(1)
C(1A)	19399(3)	12961(2)	9789(1)	22(1)
C(1B)	22059(3)	18070(2)	1796(1)	20(1)
C(7B)	26024(3)	18595(2)	4148(1)	23(1)
C(9B)	29674(3)	19090(2)	4995(1)	21(1)
C(7A)	22104(3)	12709(2)	7363(1)	22(1)
C(8A)	23258(3)	12850(2)	6750(1)	20(1)
C(18B)	25854(3)	19292(2)	6615(1)	23(1)

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TABLE 2-continued

Atomic coordinates ($\times 10^4$) and equivalent isotropic displacement parameters ($\text{\AA}^2 \times 10^3$) for NEL. U(eq) is defined as one third of the trace of the orthogonalized Uij tensor.				
	x	y	z	U(eq)
C(8B)	27529(3)	18497(2)	4760(1)	20(1)
C(4A)	22392(3)	11177(2)	9084(1)	22(1)
C(10B)	22526(3)	18874(2)	2783(1)	24(1)
C(13A)	22519(3)	12966(2)	5181(1)	21(1)
C(5A)	21554(3)	11878(2)	8545(1)	21(1)
C(13B)	27557(3)	18418(1)	6337(1)	18(1)
C(12A)	24663(3)	12455(2)	4951(1)	24(1)
C(4B)	25235(3)	19984(2)	2339(1)	23(1)
C(6B)	26236(3)	19238(2)	3562(1)	21(1)
C(5B)	24742(3)	19367(2)	2960(1)	22(1)
C(14B)	27268(3)	17751(2)	5300(1)	21(1)
C(10A)	19424(3)	12345(2)	8773(1)	24(1)
C(2B)	22531(3)	18696(2)	1180(1)	20(1)
C(11B)	30116(3)	19743(2)	6014(1)	22(1)
C(25A)	16921(3)	15954(2)	2170(1)	21(1)
C(11A)	25307(3)	11695(2)	5489(1)	26(1)
C(9A)	25341(3)	12322(2)	6512(1)	23(1)
C(2A)	20095(3)	12173(2)	10275(1)	22(1)
C(15B)	25289(4)	17009(2)	5155(1)	29(1)
C(19B)	21153(3)	18805(2)	546(1)	26(1)
C(22B)	26528(3)	16572(2)	7829(1)	24(1)
C(16A)	20397(3)	14647(2)	5542(1)	24(1)
C(19A)	18923(3)	11833(2)	10779(1)	29(1)
C(3A)	22290(3)	11784(2)	10098(1)	23(1)
C(6A)	22665(3)	12056(2)	7932(1)	22(1)
C(24A)	18538(3)	15914(2)	2914(1)	24(1)
C(15A)	20687(3)	14277(2)	6365(1)	28(1)
C(18A)	20768(3)	12036(2)	4871(1)	27(1)
C(20B)	26644(3)	17688(2)	7646(1)	22(1)
C(26B)	21533(3)	15634(2)	9292(1)	27(1)
C(25B)	23829(3)	15374(2)	9433(1)	21(1)
C(23B)	25282(3)	16605(2)	8603(1)	26(1)
C(16B)	25461(3)	16641(2)	5984(1)	26(1)
C(24B)	25149(3)	15444(2)	8706(1)	23(1)
C(23A)	19136(3)	14732(2)	2894(1)	26(1)
C(20A)	21004(3)	13700(2)	3878(1)	24(1)
C(17B)	27207(3)	17428(2)	6678(1)	20(1)
C(17A)	21928(3)	13962(1)	4855(1)	20(1)
C(22A)	20565(3)	14826(2)	3734(1)	24(1)
C(26A)	14899(3)	15287(2)	2077(1)	28(1)
C(21B)	28182(4)	18550(2)	8366(1)	33(1)
C(21A)	22416(4)	12988(2)	3186(1)	40(1)

TABLE 3

Bond lengths [Å] for NEL.	
O(1B)—C(1B)	1.419(2)
O(1B)—H(1BA)	0.8200
O(25A)—C(25A)	1.461(2)
O(25A)—H(25A)	0.8200
O(1A)—C(1A)	1.427(2)
O(1A)—H(1AA)	0.8200
O(2B)—C(3B)	1.438(2)
O(2B)—H(2BA)	0.8200
O(25B)—C(25B)	1.441(2)
O(25B)—H(25B)	0.8200
O(2A)—C(3A)	1.426(2)
O(2A)—H(2AA)	0.8200
C(12B)—C(13B)	1.529(3)
C(12B)—C(11B)	1.536(3)
C(12B)—H(12A)	0.9700
C(12B)—H(12B)	0.9700
C(3B)—C(2B)	1.503(3)
C(3B)—C(4B)	1.533(2)
C(3B)—H(3BA)	0.9800
C(14A)—C(8A)	1.511(3)
C(14A)—C(15A)	1.527(3)
C(14A)—C(13A)	1.552(2)
C(14A)—H(14A)	0.9800

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TABLE 3-continued

Bond lengths [Å] for NEL.	
C(1A)—C(2A)	1.511(3)
C(1A)—C(10A)	1.532(3)
C(1A)—H(1AB)	0.9800
C(1B)—C(2B)	1.513(3)
C(1B)—C(10B)	1.540(3)
C(1B)—H(1BB)	0.9800
C(7B)—C(8B)	1.346(3)
C(7B)—C(6B)	1.454(3)
C(7B)—H(7BA)	0.9300
C(9B)—C(8B)	1.502(3)
C(9B)—C(11B)	1.538(3)
C(9B)—H(9BA)	0.9700
C(9B)—H(9BB)	0.9700
C(7A)—C(8A)	1.338(3)
C(7A)—C(6A)	1.453(3)
C(7A)—H(7AA)	0.9300
C(8A)—C(9A)	1.512(3)
C(18B)—C(13B)	1.535(2)
C(18B)—H(18A)	0.9600
C(18B)—H(18B)	0.9600
C(18B)—H(18C)	0.9600
C(8B)—C(14B)	1.504(2)
C(4A)—C(5A)	1.508(3)
C(4A)—C(3A)	1.535(3)
C(4A)—H(4AA)	0.9700
C(4A)—H(4AB)	0.9700
C(10B)—C(5B)	1.499(3)
C(10B)—H(10A)	0.9700
C(10B)—H(10B)	0.9700
C(13A)—C(18A)	1.524(3)
C(13A)—C(12A)	1.538(2)
C(13A)—C(17A)	1.558(2)
C(5A)—C(6A)	1.342(3)
C(5A)—C(10A)	1.510(3)
C(13B)—C(17B)	1.551(2)
C(13B)—C(14B)	1.560(2)
C(12A)—C(11A)	1.536(3)
C(12A)—H(12C)	0.9700
C(12A)—H(12D)	0.9700
C(4B)—C(5B)	1.515(3)
C(4B)—H(4BA)	0.9700
C(4B)—H(4BB)	0.9700
C(6B)—C(5B)	1.345(3)
C(6B)—H(6BA)	0.9300
C(14B)—C(15B)	1.513(3)
C(14B)—H(14B)	0.9800
C(10A)—H(10C)	0.9700
C(10A)—H(10D)	0.9700
C(2B)—C(19B)	1.326(3)
C(11B)—H(11A)	0.9700
C(11B)—H(11B)	0.9700
C(25A)—C(26A)	1.499(3)
C(25A)—C(24A)	1.518(3)
C(25A)—H(25C)	0.9800
C(11A)—C(9A)	1.539(3)
C(11A)—H(11C)	0.9700
C(11A)—H(11D)	0.9700
C(9A)—H(9AA)	0.9700
C(9A)—H(9AB)	0.9700
C(2A)—C(19A)	1.320(3)
C(2A)—C(3A)	1.507(3)
C(15B)—C(16B)	1.548(3)
C(15B)—H(15A)	0.9700
C(15B)—H(15B)	0.9700
C(19B)—H(19A)	0.9300
C(19B)—H(19B)	0.9300
C(22B)—C(23B)	1.520(3)
C(22B)—C(20B)	1.537(2)
C(22B)—H(22A)	0.9700
C(22B)—H(22B)	0.9700
C(16A)—C(15A)	1.542(3)
C(16A)—C(17A)	1.563(2)
C(16A)—H(16A)	0.9700
C(16A)—H(16B)	0.9700
C(19A)—H(19C)	0.9300
C(19A)—H(19D)	0.9300
C(3A)—H(3AA)	0.9800
C(6A)—H(6AA)	0.9300

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TABLE 3-continued

Bond lengths [Å] for NEL.	
C(24A)—C(23A)	1.531(3)
C(24A)—H(24A)	0.9700
C(24A)—H(24B)	0.9700
C(15A)—H(15C)	0.9700
C(15A)—H(15D)	0.9700
C(18A)—H(18D)	0.9600
C(18A)—H(18E)	0.9600
C(18A)—H(18F)	0.9600
C(20B)—C(21B)	1.532(3)
C(20B)—C(17B)	1.541(2)
C(20B)—H(20A)	0.9800
C(26B)—C(25B)	1.519(3)
C(26B)—H(26A)	0.9600
C(26B)—H(26B)	0.9600
C(26B)—H(26C)	0.9600
C(25B)—C(24B)	1.523(3)
C(25B)—H(25D)	0.9800
C(23B)—C(24B)	1.531(2)
C(23B)—H(23A)	0.9700
C(23B)—H(23B)	0.9700
C(16B)—C(17B)	1.556(3)
C(16B)—H(16C)	0.9700
C(16B)—H(16D)	0.9700
C(24B)—H(24B)	0.9700
C(24B)—H(24C)	0.9700
C(23A)—C(22A)	1.519(3)
C(23A)—H(23C)	0.9700
C(23A)—H(23D)	0.9700
C(20A)—C(21A)	1.527(3)
C(20A)—C(17A)	1.536(3)
C(20A)—C(22A)	1.541(2)
C(20A)—H(20B)	0.9800
C(17B)—H(17A)	0.9800
C(17A)—H(17B)	0.9800
C(22A)—H(22C)	0.9700
C(22A)—H(22D)	0.9700
C(26A)—H(26D)	0.9600
C(26A)—H(26E)	0.9600
C(26A)—H(26F)	0.9600
C(21B)—H(21A)	0.9600
C(21B)—H(21B)	0.9600
C(21B)—H(21C)	0.9600
C(21A)—H(21D)	0.9600
C(21A)—H(21E)	0.9600
C(21A)—H(21F)	0.9600

TABLE 4

Bond angles [°] for NEL.	
C(1B)—O(1B)—H(1BA)	109.5
C(25A)—O(25A)—H(25A)	109.5
C(1A)—O(1A)—H(1AA)	109.5
C(3B)—O(2B)—H(2BA)	109.5
C(25B)—O(25B)—H(25B)	109.5
C(3A)—O(2A)—H(2AA)	109.5
C(13B)—C(12B)—C(11B)	111.64(14)
C(13B)—C(12B)—H(12A)	109.3
C(11B)—C(12B)—H(12A)	109.3
C(13B)—C(12B)—H(12B)	109.3
C(11B)—C(12B)—H(12B)	109.3
H(12A)—C(12B)—H(12B)	108.0
O(2B)—C(3B)—C(2B)	111.37(14)
O(2B)—C(3B)—C(4B)	107.64(14)
C(2B)—C(3B)—C(4B)	110.89(15)
O(2B)—C(3B)—H(3BA)	109.0
C(2B)—C(3B)—H(3BA)	109.0
C(4B)—C(3B)—H(3BA)	109.0
C(8A)—C(14A)—C(15A)	120.67(16)
C(8A)—C(14A)—C(13A)	113.85(14)
C(15A)—C(14A)—C(13A)	104.06(14)
C(8A)—C(14A)—H(14A)	105.7
C(15A)—C(14A)—H(14A)	105.7
C(13A)—C(14A)—H(14A)	105.7
O(1A)—C(1A)—C(2A)	113.69(15)

TABLE 4-continued

Bond angles [°] for NEL.	
O(1A)—C(1A)—C(10A)	108.29(14)
C(2A)—C(1A)—C(10A)	109.59(14)
O(1A)—C(1A)—H(1AB)	108.4
C(2A)—C(1A)—H(1AB)	108.4
C(10A)—C(1A)—H(1AB)	108.4
O(1B)—C(1B)—C(2B)	114.49(15)
O(1B)—C(1B)—C(10B)	111.74(15)
C(2B)—C(1B)—C(10B)	109.51(15)
O(1B)—C(1B)—H(1BB)	106.9
C(2B)—C(1B)—H(1BB)	106.9
C(10B)—C(1B)—H(1BB)	106.9
C(8B)—C(7B)—C(6B)	125.92(18)
C(8B)—C(7B)—H(7BA)	117.0
C(6B)—C(7B)—H(7BA)	117.0
C(8B)—C(9B)—C(11B)	111.32(15)
C(8B)—C(9B)—H(9BA)	109.4
C(11B)—C(9B)—H(9BA)	109.4
C(8B)—C(9B)—H(9BB)	109.4
C(11B)—C(9B)—H(9BB)	109.4
H(9BA)—C(9B)—H(9BB)	108.0
C(8A)—C(7A)—C(6A)	126.04(17)
C(8A)—C(7A)—H(7AA)	117.0
C(6A)—C(7A)—H(7AA)	117.0
C(7A)—C(8A)—C(14A)	124.19(17)
C(7A)—C(8A)—C(9A)	125.42(16)
C(14A)—C(8A)—C(9A)	110.37(15)
C(13B)—C(18B)—H(18A)	109.5
C(13B)—C(18B)—H(18B)	109.5
H(18A)—C(18B)—H(18B)	109.5
C(13B)—C(18B)—H(18C)	109.5
H(18A)—C(18B)—H(18C)	109.5
H(18B)—C(18B)—H(18C)	109.5
C(7B)—C(8B)—C(9B)	125.88(17)
C(7B)—C(8B)—C(14B)	123.46(18)
C(9B)—C(8B)—C(14B)	110.66(15)
C(5A)—C(4A)—C(3A)	112.48(14)
C(5A)—C(4A)—H(4AA)	109.1
C(3A)—C(4A)—H(4AA)	109.1
C(5A)—C(4A)—H(4AB)	109.1
C(3A)—C(4A)—H(4AB)	109.1
H(4AA)—C(4A)—H(4AB)	107.8
C(5B)—C(10B)—C(1B)	110.68(15)
C(5B)—C(10B)—H(10A)	109.5
C(1B)—C(10B)—H(10A)	109.5
C(5B)—C(10B)—H(10B)	109.5
C(1B)—C(10B)—H(10B)	109.5
H(10A)—C(10B)—H(10B)	108.1
C(18A)—C(13A)—C(12A)	110.65(15)
C(18A)—C(13A)—C(14A)	111.01(15)
C(12A)—C(13A)—C(14A)	107.41(15)
C(18A)—C(13A)—C(17A)	110.89(15)
C(12A)—C(13A)—C(17A)	116.13(15)
C(14A)—C(13A)—C(17A)	100.21(13)
C(6A)—C(5A)—C(4A)	121.11(17)
C(6A)—C(5A)—C(10A)	124.93(17)
C(4A)—C(5A)—C(10A)	113.96(16)
C(12B)—C(13B)—C(18B)	111.30(15)
C(12B)—C(13B)—C(17B)	115.91(14)
C(18B)—C(13B)—C(17B)	110.94(15)
C(12B)—C(13B)—C(14B)	107.44(15)
C(18B)—C(13B)—C(14B)	110.58(14)
C(17B)—C(13B)—C(14B)	100.00(13)
C(11A)—C(12A)—C(13A)	111.24(15)
C(11A)—C(12A)—H(12C)	109.4
C(13A)—C(12A)—H(12C)	109.4
C(11A)—C(12A)—H(12D)	109.4
C(13A)—C(12A)—H(12D)	109.4
H(12C)—C(12A)—H(12D)	108.0
C(5B)—C(4B)—C(3B)	110.96(15)
C(5B)—C(4B)—H(4BA)	109.4
C(3B)—C(4B)—H(4BA)	109.4
C(5B)—C(4B)—H(4BB)	109.4
C(3B)—C(4B)—H(4BB)	109.4
H(4BA)—C(4B)—H(4BB)	108.0
C(5B)—C(6B)—C(7B)	126.94(18)
C(5B)—C(6B)—H(6BA)	116.5
C(7B)—C(6B)—H(6BA)	116.5
C(6B)—C(5B)—C(10B)	125.49(17)

TABLE 4-continued

Bond angles [°] for NEL.	
C(6B)—C(5B)—C(4B)	121.22(18)
C(10B)—C(5B)—C(4B)	113.17(15)
C(8B)—C(14B)—C(15B)	121.27(16)
C(8B)—C(14B)—C(13B)	113.18(14)
C(15B)—C(14B)—C(13B)	104.01(15)
C(8B)—C(14B)—H(14B)	105.7
C(15B)—C(14B)—H(14B)	105.7
C(13B)—C(14B)—H(14B)	105.7
C(5A)—C(10A)—C(1A)	111.36(15)
C(5A)—C(10A)—H(10C)	109.4
C(1A)—C(10A)—H(10C)	109.4
C(5A)—C(10A)—H(10D)	109.4
C(1A)—C(10A)—H(10D)	109.4
H(10C)—C(10A)—H(10D)	108.0
C(19B)—C(2B)—C(3B)	121.69(17)
C(19B)—C(2B)—C(1B)	124.35(18)
C(3B)—C(2B)—C(1B)	113.96(15)
C(12B)—C(11B)—C(9B)	112.84(15)
C(12B)—C(11B)—H(11A)	109.0
C(9B)—C(11B)—H(11A)	109.0
C(12B)—C(11B)—H(11B)	109.0
C(9B)—C(11B)—H(11B)	109.0
H(11A)—C(11B)—H(11B)	107.8
O(25A)—C(25A)—C(26A)	108.17(15)
O(25A)—C(25A)—C(24A)	109.76(15)
C(26A)—C(25A)—C(24A)	114.61(16)
O(25A)—C(25A)—H(25C)	108.0
C(26A)—C(25A)—H(25C)	108.0
C(24A)—C(25A)—H(25C)	108.0
C(12A)—C(11A)—C(9A)	112.71(15)
C(12A)—C(11A)—H(11C)	109.0
C(9A)—C(11A)—H(11C)	109.0
C(12A)—C(11A)—H(11D)	109.0
C(9A)—C(11A)—H(11D)	109.0
H(11C)—C(11A)—H(11D)	107.8
C(8A)—C(9A)—C(11A)	110.93(15)
C(8A)—C(9A)—H(9AA)	109.5
C(11A)—C(9A)—H(9AA)	109.5
C(8A)—C(9A)—H(9AB)	109.5
C(11A)—C(9A)—H(9AB)	109.5
H(9AA)—C(9A)—H(9AB)	108.0
C(19A)—C(2A)—C(3A)	123.23(17)
C(19A)—C(2A)—C(1A)	124.78(18)
C(3A)—C(2A)—C(1A)	111.96(16)
C(14B)—C(15B)—C(16B)	103.37(15)
C(14B)—C(15B)—H(15A)	111.1
C(16B)—C(15B)—H(15A)	111.1
C(14B)—C(15B)—H(15B)	111.1
C(16B)—C(15B)—H(15B)	111.1
H(15A)—C(15B)—H(15B)	109.1
C(2B)—C(19B)—H(19A)	120.0
C(2B)—C(19B)—H(19B)	120.0
H(19A)—C(19B)—H(19B)	120.0
C(23B)—C(22B)—C(20B)	115.28(16)
C(23B)—C(22B)—H(22A)	108.5
C(20B)—C(22B)—H(22A)	108.5
C(23B)—C(22B)—H(22B)	108.5
C(20B)—C(22B)—H(22B)	108.5
H(22A)—C(22B)—H(22B)	107.5
C(15A)—C(16A)—C(17A)	107.70(14)
C(15A)—C(16A)—H(16A)	110.2
C(17A)—C(16A)—H(16A)	110.2
C(15A)—C(16A)—H(16B)	110.2
C(17A)—C(16A)—H(16B)	110.2
H(16A)—C(16A)—H(16B)	108.5
C(2A)—C(19A)—H(19C)	120.0
C(2A)—C(19A)—H(19D)	120.0
H(19C)—C(19A)—H(19D)	120.0
O(2A)—C(3A)—C(2A)	106.68(15)
O(2A)—C(3A)—C(4A)	112.30(15)
C(2A)—C(3A)—C(4A)	109.87(15)
O(2A)—C(3A)—H(3AA)	109.3
C(2A)—C(3A)—H(3AA)	109.3
C(4A)—C(3A)—H(3AA)	109.3
C(5A)—C(6A)—C(7A)	128.24(17)
C(5A)—C(6A)—H(6AA)	115.9
C(7A)—C(6A)—H(6AA)	115.9
C(25A)—C(24A)—C(23A)	116.64(15)

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TABLE 4-continued

Bond angles [°] for NEL.	
C(25A)—C(24A)—H(24A)	108.1
C(23A)—C(24A)—H(24A)	108.1
C(25A)—C(24A)—H(24B)	108.1
C(23A)—C(24A)—H(24B)	108.1
H(24A)—C(24A)—H(24B)	107.3
C(14A)—C(15A)—C(16A)	103.22(15)
C(14A)—C(15A)—H(15C)	111.1
C(16A)—C(15A)—H(15C)	111.1
C(14A)—C(15A)—H(15D)	111.1
C(16A)—C(15A)—H(15D)	111.1
H(15C)—C(15A)—H(15D)	109.1
C(13A)—C(18A)—H(18D)	109.5
C(13A)—C(18A)—H(18E)	109.5
H(18D)—C(18A)—H(18E)	109.5
C(13A)—C(18A)—H(18F)	109.5
H(18D)—C(18A)—H(18F)	109.5
H(18E)—C(18A)—H(18F)	109.5
C(21B)—C(20B)—C(22B)	109.89(15)
C(21B)—C(20B)—C(17B)	113.74(16)
C(22B)—C(20B)—C(17B)	109.14(14)
C(21B)—C(20B)—H(20A)	108.0
C(22B)—C(20B)—H(20A)	108.0
C(17B)—C(20B)—H(20A)	108.0
C(25B)—C(26B)—H(26A)	109.5
C(25B)—C(26B)—H(26B)	109.5
H(26A)—C(26B)—H(26B)	109.5
C(25B)—C(26B)—H(26C)	109.5
H(26A)—C(26B)—H(26C)	109.5
H(26B)—C(26B)—H(26C)	109.5
O(25B)—C(25B)—C(26B)	106.88(15)
O(25B)—C(25B)—C(24B)	109.97(15)
C(26B)—C(25B)—C(24B)	113.97(15)
O(25B)—C(25B)—H(25D)	108.6
C(26B)—C(25B)—H(25D)	108.6
C(24B)—C(25B)—H(25D)	108.6
C(22B)—C(23B)—C(24B)	111.82(15)
C(22B)—C(23B)—H(23A)	109.3
C(24B)—C(23B)—H(23A)	109.3
C(22B)—C(23B)—H(23B)	109.3
C(24B)—C(23B)—H(23B)	109.3
H(23A)—C(23B)—H(23B)	107.9
C(15B)—C(16B)—C(17B)	107.10(15)
C(15B)—C(16B)—H(16C)	110.3
C(17B)—C(16B)—H(16C)	110.3
C(15B)—C(16B)—H(16D)	110.3
C(17B)—C(16B)—H(16D)	110.3
H(16C)—C(16B)—H(16D)	108.6
C(25B)—C(24B)—C(23B)	115.78(15)
C(25B)—C(24B)—H(24B)	108.3
C(23B)—C(24B)—H(24B)	108.3
C(25B)—C(24B)—H(24C)	108.3
C(23B)—C(24B)—H(24C)	108.3
H(24B)—C(24B)—H(24C)	107.4
C(22A)—C(23A)—C(24A)	110.47(15)
C(22A)—C(23A)—H(23C)	109.6
C(24A)—C(23A)—H(23C)	109.6
C(22A)—C(23A)—H(23D)	109.6
C(24A)—C(23A)—H(23D)	109.6
H(23C)—C(23A)—H(23D)	108.1
C(21A)—C(20A)—C(17A)	113.40(17)
C(21A)—C(20A)—C(22A)	110.07(17)
C(17A)—C(20A)—C(22A)	109.15(14)
C(21A)—C(20A)—H(20B)	108.0
C(17A)—C(20A)—H(20B)	108.0
C(22A)—C(20A)—H(20B)	108.0
C(20B)—C(17B)—C(13B)	119.83(14)
C(20B)—C(17B)—C(16B)	110.64(15)
C(13B)—C(17B)—C(16B)	104.20(14)
C(20B)—C(17B)—H(17A)	107.2
C(13B)—C(17B)—H(17A)	107.2
C(16B)—C(17B)—H(17A)	107.2
C(20A)—C(17A)—C(13A)	119.67(14)
C(20A)—C(17A)—C(16A)	111.84(15)
C(13A)—C(17A)—C(16A)	103.18(14)
C(20A)—C(17A)—H(17B)	107.2
C(13A)—C(17A)—H(17B)	107.2
C(16A)—C(17A)—H(17B)	107.2
C(23A)—C(22A)—C(20A)	116.00(16)

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TABLE 4-continued

Bond angles [°] for NEL.	
C(23A)—C(22A)—H(22C)	108.3
C(20A)—C(22A)—H(22C)	108.3
C(23A)—C(22A)—H(22D)	108.3
C(20A)—C(22A)—H(22D)	108.3
H(22C)—C(22A)—H(22D)	107.4
C(25A)—C(26A)—H(26D)	109.5
C(25A)—C(26A)—H(26E)	109.5
H(26D)—C(26A)—H(26E)	109.5
C(25A)—C(26A)—H(26F)	109.5
H(26D)—C(26A)—B(26F)	109.5
H(26E)—C(26A)—H(26F)	109.5
C(20B)—C(21B)—H(21A)	109.5
C(20B)—C(21B)—H(21B)	109.5
H(21A)—C(21B)—H(21B)	109.5
C(20B)—C(21B)—H(21C)	109.5
H(21A)—C(21B)—H(21C)	109.5
H(21B)—C(21B)—H(21C)	109.5
C(20A)—C(21A)—H(21D)	109.5
C(20A)—C(21A)—H(21E)	109.5
H(21D)—C(21A)—H(21E)	109.5
C(20A)—C(21A)—H(21F)	109.5
H(21D)—C(21A)—H(21F)	109.5
H(21E)—C(21A)—H(21F)	109.5

TABLE 5

Anisotropic displacement parameters ($\text{\AA}^2 \times 10^3$) for NEL. The anisotropic displacement factor exponent takes the form: $-2\pi^2 [h^2 a^{*2} U_{11} + \dots + 2hka^* b^* U_{12}]$						
	U11	U22	U33	U23	U13	U12
O(1B)	17(1)	27(1)	31(1)	16(1)	0(1)	-2(1)
O(25A)	26(1)	23(1)	20(1)	9(1)	4(1)	1(1)
O(1A)	20(1)	26(1)	28(1)	8(1)	5(1)	3(1)
O(2B)	19(1)	24(1)	26(1)	6(1)	2(1)	2(1)
O(25B)	30(1)	24(1)	20(1)	9(1)	-2(1)	4(1)
O(2A)	21(1)	34(1)	29(1)	4(1)	2(1)	-6(1)
C(12B)	18(1)	24(1)	22(1)	11(1)	-3(1)	-4(1)
C(3B)	22(1)	22(1)	23(1)	13(1)	2(1)	4(1)
C(14A)	21(1)	19(1)	20(1)	7(1)	3(1)	1(1)
C(1A)	20(1)	20(1)	25(1)	7(1)	2(1)	-2(1)
C(1B)	18(1)	21(1)	24(1)	11(1)	3(1)	2(1)
C(7B)	23(1)	22(1)	20(1)	5(1)	1(1)	-5(1)
C(9B)	20(1)	22(1)	23(1)	11(1)	2(1)	0(1)
C(7A)	23(1)	20(1)	20(1)	5(1)	2(1)	3(1)
C(8A)	21(1)	18(1)	19(1)	5(1)	-1(1)	1(1)
C(18B)	24(1)	26(1)	24(1)	13(1)	3(1)	4(1)
C(8B)	25(1)	18(1)	15(1)	3(1)	2(1)	-1(1)
C(4A)	24(1)	21(1)	23(1)	10(1)	3(1)	2(1)
C(10B)	26(1)	27(1)	22(1)	13(1)	5(1)	3(1)
C(13A)	23(1)	19(1)	22(1)	9(1)	2(1)	1(1)
C(5A)	24(1)	17(1)	18(1)	4(1)	0(1)	-1(1)
C(13B)	20(1)	19(1)	17(1)	7(1)	0(1)	-1(1)
C(12A)	26(1)	26(1)	24(1)	12(1)	9(1)	7(1)
C(4B)	24(1)	20(1)	25(1)	9(1)	2(1)	1(1)
C(6B)	25(1)	19(1)	17(1)	4(1)	1(1)	-2(1)
C(5B)	27(1)	20(1)	18(1)	6(1)	5(1)	3(1)
C(14B)	24(1)	19(1)	18(1)	7(1)	1(1)	-2(1)
C(10A)	25(1)	25(1)	24(1)	13(1)	1(1)	1(1)
C(2B)	20(1)	19(1)	20(1)	6(1)	2(1)	3(1)
C(11B)	17(1)	24(1)	25(1)	12(1)	-2(1)	-4(1)
C(25A)	27(1)	21(1)	17(1)	8(1)	4(1)	5(1)
C(11A)	24(1)	29(1)	31(1)	17(1)	11(1)	11(1)
C(9A)	21(1)	26(1)	27(1)	14(1)	2(1)	2(1)
C(2A)	24(1)	23(1)	17(1)	6(1)	0(1)	-3(1)
C(15B)	35(1)	28(1)	22(1)	9(1)	-4(1)	-13(1)
C(19B)	22(1)	31(1)	29(1)	17(1)	2(1)	1(1)
C(22B)	26(1)	24(1)	22(1)	9(1)	0(1)	-2(1)
C(16A)	26(1)	23(1)	25(1)	10(1)	4(1)	5(1)
C(19A)	26(1)	37(1)	29(1)	17(1)	5(1)	2(1)
C(3A)	23(1)	24(1)	21(1)	11(1)	-2(1)	-1(1)
C(6A)	24(1)	18(1)	22(1)	6(1)	1(1)	2(1)
C(24A)	33(1)	19(1)	20(1)	6(1)	1(1)	3(1)
C(15A)	34(1)	27(1)	27(1)	13(1)	10(1)	12(1)

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TABLE 5-continued

Anisotropic displacement parameters ($\text{\AA}^2 \times 10^3$) for NEL. The anisotropic displacement factor exponent takes the form: $-2\pi^2 [h^2 a^{*2} U_{11} + \dots + 2hka^* b^* U_{12}]$						
	U11	U22	U33	U23	U13	U12
C(18A)	29(1)	22(1)	32(1)	13(1)	-4(1)	-3(1)
C(20B)	22(1)	24(1)	19(1)	9(1)	1(1)	-1(1)
C(26B)	26(1)	29(1)	26(1)	10(1)	1(1)	-4(1)
C(25B)	24(1)	19(1)	21(1)	8(1)	-1(1)	-1(1)
C(23B)	36(1)	23(1)	23(1)	11(1)	6(1)	1(1)
C(16B)	30(1)	26(1)	21(1)	10(1)	-1(1)	-7(1)
C(24B)	27(1)	20(1)	22(1)	8(1)	0(1)	-1(1)
C(23A)	35(1)	21(1)	21(1)	8(1)	-2(1)	2(1)
C(20A)	29(1)	19(1)	24(1)	6(1)	0(1)	3(1)
C(17B)	20(1)	20(1)	20(1)	8(1)	1(1)	0(1)
C(17A)	20(1)	17(1)	22(1)	7(1)	0(1)	0(1)
C(22A)	30(1)	21(1)	22(1)	9(1)	-1(1)	1(1)
C(26A)	30(1)	34(1)	25(1)	15(1)	3(1)	3(1)
C(21B)	43(1)	33(1)	22(1)	14(1)	-6(1)	-10(1)
C(21A)	59(2)	42(1)	23(1)	13(1)	8(1)	25(1)

TABLE 6

Hydrogen coordinates ($\times 10^4$) and isotropic displacement parameters ($\text{\AA}^2 \times 10^3$) for NEL.				
	x	y	z	U(eq)
H(1BA)	19161	17964	1490	35
H(25A)	18570	16034	1263	33
H(1AA)	17440	14003	10350	38
H(2BA)	25660	17721	897	36
H(25B)	25582	15881	10525	37
H(2AA)	24659	12701	10160	45
H(12A)	30805	18420	6459	25
H(12B)	29951	19463	7205	25
H(3BA)	24872	19664	970	25
H(14A)	23849	14164	6358	24
N(1AB)	20405	13618	9985	26
H(1BB)	23051	17459	1699	24
H(7BA)	24730	18218	4096	27
H(9BA)	29766	19618	4680	25
H(9BB)	30734	18533	4798	25
H(7AA)	20824	13061	7432	26
H(18A)	26102	19896	6397	35
H(18B)	25900	19599	7259	35
H(18C)	24494	18928	6363	35
H(4AA)	23843	11012	8972	27
H(4AB)	21582	10459	8883	27
H(10A)	21552	19485	2912	29
H(10B)	22323	18458	3178	29
H(12C)	24585	12009	4312	29
H(12D)	25726	13065	5083	29
H(4BA)	26714	20228	2451	27
H(4BB)	24412	20656	2462	27
H(6BA)	27544	19598	3608	26
H(14B)	28424	17229	5174	25
H(10C)	18361	11726	8562	29

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TABLE 6-continued

Hydrogen coordinates ($\times 10^4$) and isotropic displacement parameters ($\text{\AA}^2 \times 10^3$) for NEL.				
	x	y	z	U(eq)
H(10D)	19077	12870	8467	29
H(11A)	31562	20046	6148	26
H(11B)	29205	20381	6189	26
H(25C)	16590	16751	2294	25
H(11C)	26696	11421	5353	31
H(11D)	24327	11039	5303	31
H(9AA)	25631	11790	6817	28
H(9AB)	26460	12912	6716	28
H(15A)	25251	16354	4601	35
H(15B)	24038	17434	5137	35
H(19A)	21542	19209	194	39
H(19B)	19798	18479	454	39
H(22A)	25901	15976	7287	28
H(22B)	27952	16366	7953	28
H(16A)	20720	15457	5724	29
H(16B)	18952	14489	5269	29
H(19C)	19444	11330	11045	44
H(19D)	17576	12098	10868	44
H(3AA)	22660	11257	10408	27
H(6AA)	23960	11720	7861	26
H(24A)	18004	16316	3486	29
H(24B)	19810	16327	2892	29
H(15C)	20875	14932	6921	33
H(15D)	19488	13807	6380	33
H(18D)	19443	12371	5020	41
H(18E)	21043	11501	5166	41
H(18F)	20715	11650	4232	41
H(20A)	25243	18002	7690	26
H(26A)	20801	15579	9775	41
H(26B)	20899	15098	8731	41
H(26C)	21447	16391	9283	41
H(25D)	23893	14605	9451	26
H(23A)	23870	16840	8498	32
H(23B)	25948	17163	9157	32
H(16C)	25832	15852	5811	31
H(16D)	24128	16721	6241	31
H(24B)	24572	14884	8135	28
H(24C)	26567	15235	8835	28
H(23C)	17871	14278	2858	31
H(23D)	19853	14353	2365	31
H(20B)	19657	13272	3783	29
H(17A)	28500	17005	6615	24
H(17B)	23208	14447	4956	23
H(22C)	19938	15328	4253	29
H(22D)	21902	15184	3712	29
H(26D)	13962	15360	1598	43
H(26E)	14256	15574	2630	43
H(26F)	15183	14500	1945	43
H(21A)	28248	19245	8248	49
H(21B)	29556	18246	8354	49
H(21C)	27705	18701	8948	49
H(21D)	22673	12286	3278	61
H(21E)	23730	13402	3253	61
H(21F)	21731	12827	2591	61

Observed and calculated structure factors for NEL

h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s
0	2	-18	48	43	2	1	0	-16	58	59	1	1	0	-15	78	80	1
1	0	-18	75	71	2	2	0	-16	67	68	1	2	0	-15	127	130	2
0	3	-18	30	27	2	3	0	-16	44	45	1	3	0	-15	32	29	1
1	3	-18	35	36	1	-1	1	-16	44	45	2	4	0	-15	9	8	0
2	3	-18	26	28	2	0	1	-16	138	127	3	-1	1	-15	95	98	2
-1	4	-18	12	10	6	1	1	-16	110	118	1	0	1	-15	39	37	2
0	4	-18	55	56	2	2	1	-16	43	41	1	1	1	-15	70	68	1
1	4	-18	38	40	1	3	1	-16	44	44	1	2	1	-15	96	95	1
2	4	-18	36	34	1	4	1	-16	38	41	1	3	1	-15	73	75	1
-1	5	-18	25	23	3	-2	2	-16	24	23	3	4	1	-15	31	28	1
0	5	-18	33	29	2	-1	2	-16	86	84	2	-2	2	-15	81	87	2
1	5	-18	68	65	1	0	2	-16	106	101	2	-1	2	-15	79	74	2
0	6	-18	12	14	5	2	2	-16	63	63	1	1	2	-15	86	83	2
-1	6	-18	41	37	2	1	2	-16	67	64	1	0	2	-15	47	46	2
0	7	-18	21	20	3	3	2	-16	105	102	1	2	2	-15	72	76	1
1	6	-18	69	68	1	4	2	-16	31	29	1	3	2	-15	35	40	1
2	6	-18	13	11	5	-2	3	-16	58	60	2	4	2	-15	59	55	1
-1	7	-18	22	21	3	-1	3	-16	72	72	2	-2	3	-15	79	75	2
0	7	-18	19	22	2	0	3	-16	38	30	2	-1	3	-15	58	58	2
1	7	-18	109	102	2	1	3	-16	52	51	1	0	3	-15	13	10	3
2	7	-18	90	92	2	2	3	-16	35	32	1	1	3	-15	200	198	3
1	8	-18	58	61	1	3	3	-16	14	15	3	2	3	-15	116	121	1
-1	8	-17	77	82	2	4	3	-16	71	71	1	3	3	-15	10	13	4
0	0	-17	39	34	2	-2	4	-16	31	31	3	4	3	-15	54	53	1
1	0	-17	111	105	3	-1	4	-16	45	43	2	5	3	-15	105	111	2
2	0	-17	16	18	2	0	4	-16	90	93	2	-2	4	-15	39	42	2
-1	1	-17	87	83	2	1	4	-16	96	96	2	-1	4	-15	61	62	2
0	1	-17	211	197	5	2	4	-16	21	22	1	0	4	-15	39	44	1
1	1	-17	38	33	1	3	4	-16	54	56	1	1	4	-15	86	87	1
2	1	-17	117	113	1	4	4	-16	26	26	1	2	4	-15	109	108	1
3	1	-17	85	84	2	-2	5	-16	24	20	3	4	4	-15	67	73	1
-1	2	-17	53	54	2	-1	5	-16	97	96	2	3	4	-15	44	43	1
0	2	-17	124	117	3	0	5	-16	69	69	1	5	4	-15	31	27	2
1	2	-17	88	85	1	1	5	-16	46	47	1	-2	5	-15	27	25	3
2	2	-17	49	50	1	2	5	-16	58	56	1	1	5	-15	177	181	3
3	2	-17	48	49	1	3	5	-16	87	87	1	0	5	-15	162	200	4
-1	3	-17	42	35	2	4	5	-16	49	53	1	1	5	-15	108	106	2
0	3	-17	100	96	2	-2	6	-16	89	87	2	2	5	-15	72	72	1
1	3	-17	43	44	1	-1	6	-16	43	42	2	3	5	-15	122	120	2
2	3	-17	11	7	4	0	6	-16	122	118	2	4	5	-15	86	85	1
3	3	-17	34	34	1	1	6	-16	93	90	2	-3	6	-15	51	51	2
-2	4	-17	51	52	2	2	6	-16	18	14	2	-2	6	-15	48	51	2
0	-1	-17	46	46	2	3	6	-16	36	34	1	-1	6	-15	68	68	2
-1	4	-17	131	123	3	4	6	-16	57	62	2	0	6	-15	154	158	4
0	4	-17	18	16	3	-2	7	-16	18	25	3	1	6	-15	30	25	2
2	4	-17	51	50	1	-1	7	-16	64	61	2	2	6	-15	42	42	1
3	4	-17	10	8	7	0	7	-16	33	33	2	3	6	-15	84	84	1

TABLE 7-continued

Observed and calculated structure factors for NEL																							
h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s
-2	5	-17	42	39	2	1	7	-16	104	106	1	4	6	-15	103	107	2	4	3	-14	61	55	1
-1	5	-17	37	36	2	2	7	-16	88	86	2	3	7	-15	29	31	3	5	3	-14	17	15	4
0	5	-17	18	14	2	3	7	-16	38	35	1	-2	7	-15	127	126	3	5	4	-14	67	64	2
1	5	-17	59	60	1	-2	8	-16	64	64	2	-1	7	-15	73	70	2	-1	4	-14	182	190	3
2	5	-17	36	35	1	-1	8	-16	68	63	2	0	7	-15	51	54	1	0	4	-14	327	325	5
3	5	-17	18	17	2	0	8	-16	60	56	1	1	7	-15	48	52	1	1	4	-14	129	138	2
-2	6	-17	83	78	2	1	8	-16	21	22	2	2	7	-15	56	58	1	2	4	-14	125	123	1
-1	6	-17	41	39	2	2	8	-16	59	61	2	3	7	-15	67	69	1	3	4	-14	184	206	3
0	6	-17	16	15	3	3	8	-16	52	45	2	4	7	-15	42	40	2	4	4	-14	65	65	1
1	6	-17	105	108	2	-2	9	-16	64	62	2	-3	8	-15	81	85	2	5	4	-14	51	49	2
2	6	-17	67	68	2	-1	9	-16	84	80	2	-2	8	-15	43	43	2	-2	5	-14	53	51	2
3	6	-17	21	20	2	0	9	-16	37	32	1	-1	8	-15	66	67	2	-1	5	-14	59	54	2
-2	7	-17	103	101	2	1	9	-16	39	37	1	0	8	-15	123	121	2	0	5	-14	83	100	2
-1	7	-17	42	41	2	2	9	-16	67	65	2	1	8	-15	29	27	1	1	5	-14	73	75	1
0	7	-17	54	51	1	3	9	-16	55	58	2	2	8	-15	80	78	2	2	5	-14	171	173	2
1	7	-17	16	18	2	-2	10	-16	47	44	2	3	8	-15	85	85	1	3	5	-14	74	69	1
2	7	-17	33	30	2	-1	10	-16	36	36	2	-3	9	-15	40	43	2	4	5	-14	63	63	1
3	7	-17	15	16	3	0	10	-16	16	17	2	-2	9	-15	38	37	2	5	5	-14	62	58	2
-2	8	-17	17	18	3	1	10	-16	114	117	2	-1	9	-15	43	44	1	-3	6	-14	44	44	2
-1	8	-17	86	83	2	2	10	-16	121	122	3	0	9	-15	65	60	1	-2	6	-14	34	29	2
0	8	-17	11	9	5	-1	11	-16	19	18	2	1	9	-15	53	56	1	-1	6	-14	9	4	9
1	8	-17	77	75	1	0	11	-16	17	14	2	2	9	-15	114	107	3	0	6	-14	207	203	5
2	8	-17	35	30	2	1	11	-16	44	44	2	3	9	-15	51	53	2	1	6	-14	47	47	1
3	8	-17	13	18	4	1	11	-16	46	47	1	-2	10	-15	60	61	2	2	6	-14	84	87	1
-1	9	-17	25	25	2	0	-3	-15	108	106	2	-1	10	-15	78	74	1	3	6	-14	99	97	2
0	9	-17	50	46	1	1	3	-15	49	48	1	0	10	-15	56	56	1	4	6	-14	34	34	1
1	9	-17	47	49	1	2	-3	-15	56	53	1	1	10	-15	47	45	1	5	6	-14	43	41	2
2	9	-17	67	64	2	-1	-2	-15	57	61	1	2	10	-15	63	62	2	-3	7	-14	44	44	2
3	9	-17	61	56	2	0	-2	-15	109	103	2	-2	11	-15	49	44	2	-2	7	-14	75	74	2
1	10	-17	19	19	3	1	-2	-15	51	52	1	-1	11	-15	47	42	1	-1	7	-14	158	171	2
0	10	-17	40	37	1	2	-2	-15	30	31	1	0	11	-15	43	36	1	0	7	-14	140	143	3
-2	-2	-16	27	34	2	3	-2	-15	51	51	1	1	11	-15	90	88	2	1	7	-14	161	165	2
2	-2	-16	26	27	2	-1	-1	-15	72	66	2	2	11	-15	30	27	2	2	7	-14	82	86	1
-1	-1	-16	17	21	5	0	-1	-15	36	36	2	0	12	-15	64	60	1	3	7	-14	115	115	2
0	-1	-16	61	59	1	1	-1	-15	33	37	2	1	12	-15	67	67	2	4	7	-14	62	63	1
1	-1	-16	88	82	1	2	-1	-15	13	12	3	0	-5	-14	37	48	2	-3	8	-14	59	55	2
2	-1	-16	40	44	1	3	-1	-15	37	37	1	1	-5	-14	13	10	3	-2	8	-14	24	26	3
3	-1	-16	9	13	8	4	-1	-14	26	26	1	-1	-4	-14	19	12	3	-1	8	-14	69	76	1
-1	0	-16	94	91	2	-1	0	-15	12	7	12	0	-4	-14	39	37	1	0	8	-14	84	83	1
0	0	-16	125	125	2	0	0	-15	25	25	2	1	-4	-14	82	82	1	1	8	-14	117	119	1
-2	2	-13	173	185	4	-1	13	-13	47	47	1	-3	3	-12	48	51	2	2	12	-12	69	67	2
-1	2	-13	57	59	2	0	13	-13	5	9	4	-2	3	-12	98	102	2	-2	13	-12	73	73	1
1	2	-13	142	139	1	1	13	-13	52	51	2	-1	3	-12	89	95	1	-1	13	-12	81	83	2
2	2	-13	158	158	1	0	-7	-12	46	43	2	0	3	-12	122	127	1	0	13	-12	58	51	1
3	2	-13	55	56	1	1	-7	-12	21	24	2	1	3	-12	185	194	2	1	13	-12	30	30	1
4	2	-13	118	120	2	-1	-6	-12	44	45	2	2	3	-12	85	85	1	2	13	-12	34	38	2
5	2	-13	34	28	1	0	-6	-12	31	35	2	3	3	-12	28	29	1	-1	-7	-11	49	51	2
-4	3	-13	126	122	2	1	-6	-12	60	59	1	4	3	-12	202	204	5	0	-7	-11	60	61	2
-3	3	-13	58	57	2	2	-6	-12	111	108	2	5	3	-12	115	117	1	1	-7	-11	35	37	1

h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s
-3	3	-13	119	120	3	3	-6	-12	75	76	2	-5	4	-12	95	97	2
-2	3	-13	57	51	2	-2	-5	-12	44	43	2	-4	4	-12	32	26	2
-1	3	-13	29	34	2	-1	-5	-12	28	24	3	-3	4	-12	103	107	2
0	3	-13	311	310	3	0	-5	-12	24	27	2	-2	4	-12	22	20	2
1	3	-13	23	20	1	1	-5	-12	88	88	1	-1	4	-12	132	131	2
2	3	-13	125	127	1	2	-5	-12	29	30	2	0	4	-12	42	41	1
3	3	-13	102	103	2	3	-5	-12	139	138	2	1	4	-12	180	179	2
4	3	-13	129	134	2	4	-5	-12	71	78	2	2	4	-12	94	96	1
5	3	-13	127	119	3	-3	-4	-12	72	74	2	3	4	-12	61	63	1
-2	4	-13	138	137	3	-2	-4	-12	69	69	2	4	4	-12	30	28	1
-1	4	-13	131	130	2	-1	-4	-12	79	76	2	5	4	-12	158	161	1
0	4	-13	63	69	1	0	-4	-12	45	42	1	6	4	-12	38	37	1
1	4	-13	13	14	2	1	-4	-12	85	92	2	-4	5	-12	99	99	2
2	4	-13	80	82	1	2	-4	-12	70	65	1	-2	5	-12	55	53	2
3	4	-13	26	30	1	3	-4	-12	67	66	1	-1	5	-12	220	225	2
4	4	-13	27	22	2	4	-4	-12	27	28	1	0	5	-12	116	112	1
5	4	-13	123	116	3	-3	-3	-12	22	22	3	1	5	-12	145	147	1
-2	5	-13	104	103	3	-2	-3	-12	52	52	1	2	5	-12	110	114	1
-1	5	-13	234	233	3	-1	-3	-12	79	82	1	3	5	-12	184	182	3
0	5	-13	430	428	5	0	-3	-12	90	86	2	4	5	-12	144	145	1
1	5	-13	199	204	2	1	-3	-12	124	121	2	5	5	-12	40	42	1
2	5	-13	48	49	1	2	-3	-12	41	47	1	6	5	-12	24	25	1
3	5	-13	96	98	2	3	-3	-12	77	79	1	-3	6	-12	69	70	2
4	5	-13	122	123	2	4	-3	-12	79	76	1	-2	6	-12	154	151	3
5	5	-13	30	25	1	5	-3	-12	42	43	2	-1	6	-12	152	152	2
-3	6	-13	55	53	2	-4	-2	-12	50	47	2	0	6	-12	121	117	1
-2	6	-13	108	108	3	-3	-2	-12	121	120	3	1	6	-12	161	164	2
-1	6	-13	285	317	12	-1	-2	-12	67	65	1	2	6	-12	64	62	1
0	6	-13	156	148	2	0	-2	-12	128	124	2	3	6	-12	153	157	2
1	6	-13	58	63	1	1	-2	-12	101	109	1	5	6	-12	80	84	1
2	6	-13	110	112	2	3	-2	-12	96	127	1	-3	7	-12	122	129	3
3	6	-13	103	105	1	3	-2	-12	160	159	2	-2	7	-12	70	66	2

TABLE 7-continued

Observed and calculated structure factors for NEL																							
h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s
3	8	-13	43	43	1	0	0	-12	88	88	1	-3	9	-12	64	69	2	-2	6	-11	131	129	1
4	8	-13	60	58	1	1	0	-12	120	119	1	-2	9	-12	55	55	2	-1	6	-11	106	108	1
5	8	-13	21	18	1	2	0	-12	67	71	1	-1	9	-12	56	54	1	0	7	-11	35	31	2
-3	9	-13	108	109	3	3	0	-12	105	108	1	0	9	-12	70	75	1	1	-1	-11	259	264	6
-2	9	-13	147	145	3	4	0	-12	24	23	1	1	9	-12	118	122	2	2	7	-11	53	52	1
-1	9	-13	24	25	2	5	0	-12	148	142	2	2	9	-12	63	65	2	3	-1	-11	87	84	1
0	9	-13	102	99	2	-5	1	-12	90	87	2	3	9	-12	12	15	5	4	-1	-11	140	141	1
1	9	-13	63	61	1	-4	1	-12	33	27	2	4	9	-12	48	52	1	5	-1	-11	281	289	2
2	9	-13	127	141	3	-3	1	-12	182	179	4	5	9	-12	35	36	1	-5	0	-11	38	36	1
3	9	-13	45	42	2	-2	1	-12	59	58	2	-3	10	-12	67	65	2	-4	0	-11	44	41	2
4	9	-13	40	40	1	-1	1	-12	141	146	2	-2	10	-12	60	64	2	-3	0	-11	121	120	3
-3	10	-13	26	26	3	0	1	-12	52	51	1	-1	10	-12	3	4	3	-2	0	-11	135	143	2
-2	10	-13	71	68	2	1	1	-12	257	259	2	0	10	-12	23	19	2	-1	0	-11	130	132	1
-1	10	-13	36	36	1	2	1	-12	113	112	1	1	10	-12	47	50	1	0	0	-11	225	221	2
0	10	-13	69	69	1	3	1	-12	88	93	2	2	10	-12	37	36	2	1	0	-11	155	148	1
1	10	-13	39	37	1	4	1	-12	97	95	2	3	10	-12	30	28	2	2	0	-11	68	62	1
2	10	-13	88	81	2	5	1	-12	90	88	1	4	10	-12	67	66	1	3	0	-11	89	89	1
3	10	-13	61	62	2	-5	2	-12	95	91	2	-3	11	-12	53	56	2	4	0	-11	35	36	1
-3	11	-13	21	25	3	-4	2	-12	45	40	2	-2	11	-12	10	1	10	5	0	-11	65	61	1
-2	11	-13	52	51	2	-3	2	-12	41	41	2	-1	11	-12	84	84	1	-5	1	-11	54	54	2
-1	11	-13	97	90	2	-2	2	-12	136	140	2	0	11	-12	26	25	2	-4	1	-11	42	40	2
0	11	-13	25	22	2	-1	2	-12	104	106	2	1	11	-12	41	45	1	-3	1	-11	76	72	2
1	11	-13	78	77	1	0	2	-12	48	45	1	2	11	-12	66	63	2	-2	1	-11	55	52	1
2	11	-13	124	121	3	1	2	-12	80	83	1	3	11	-12	68	67	2	-1	1	-11	154	165	1
-2	12	-13	19	22	3	2	2	-12	33	29	1	-3	12	-12	29	31	2	0	1	-11	117	117	1
-1	12	-13	17	12	2	3	2	-12	28	26	1	-2	12	-12	49	49	2	1	1	-11	18	12	1
0	12	-13	66	62	1	4	2	-12	59	61	1	1	12	-12	38	37	1	2	1	-11	176	164	1
1	12	-13	85	80	1	5	2	-12	184	178	3	0	12	-12	62	61	1	3	1	-11	94	96	1
2	12	-13	18	16	3	-4	3	-12	37	31	2	1	12	-12	12	15	1	4	1	-11	35	35	1
-3	10	-11	16	20	4	6	-2	-10	20	27	2	1	6	-10	88	84	1	2	-6	-9	73	71	1
-2	10	-11	149	157	3	-5	-1	-10	71	70	2	2	6	-10	64	66	1	3	-6	-9	58	59	1
-1	10	-11	153	151	4	-4	-1	-10	65	69	2	3	6	-10	78	73	1	4	1	-11	35	35	1
0	10	-11	42	44	1	-3	-1	-10	72	83	2	4	6	-10	50	50	1	5	-6	-9	50	52	1
1	10	-11	169	173	3	-2	-1	-10	92	96	1	5	6	-10	89	88	1	-4	-5	-9	39	38	2
2	10	-11	104	102	2	-1	-1	-10	86	86	1	-5	7	-10	77	82	2	-3	-5	-9	62	57	2
3	10	-11	29	30	2	0	-1	-10	68	66	1	-4	7	-10	50	47	2	-2	-5	-9	106	103	3
4	10	-11	59	58	1	1	-1	-10	72	69	1	-3	7	-10	120	124	3	-1	-5	-9	117	118	3
-3	11	-11	14	10	4	2	-2	-10	116	115	1	-2	7	-10	244	241	4	0	-5	-9	9	6	4
-2	11	-11	129	124	3	3	-1	-10	53	55	1	-1	7	-10	159	164	2	1	-5	-9	116	116	1
-1	11	-11	46	46	1	4	-1	-10	79	78	1	0	7	-10	288	271	3	2	-5	-9	81	80	1
0	11	-11	72	73	1	5	-1	-10	39	41	1	1	7	-10	117	118	1	3	-5	-9	133	130	2
1	11	-11	103	99	1	-5	0	-10	151	149	3	2	7	-10	252	251	1	4	-5	-9	22	19	2
2	11	-11	147	145	3	-4	0	-10	37	47	2	3	7	-10	100	98	1	5	-5	-9	100	100	2
3	11	-11	29	32	2	-3	0	-10	153	162	4	4	7	-10	48	48	1	-5	-4	-9	24	23	3
4	11	-11	61	61	1	-2	0	-10	99	95	2	5	7	-10	75	74	1	-4	-4	-9	23	21	3
-3	12	-11	54	54	2	-1	0	-10	107	108	1	-3	8	-10	92	89	2	-2	-4	-9	120	123	3
-2	12	-11	62	69	2	0	0	-10	36	31	1	-2	8	-10	29	30	2	-1	-4	-9	88	86	1
-1	12	-11	64	62	1	1	0	-10	169	171	1	-1	8	-10	116	108	1	0	-4	-9	43	46	1
0	12	-11	57	55	1	2	0	-10	105	105	1	0	8	-10	148	139	2	1	-4	-9	62	61	1

TABLE 7-continued

Observed and calculated structure factors for NEL																								
h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s	
1	12	-11	72	71	1	3	0	-10	44	41	1	1	1	8	-10	158	156	1	2	-4	-9	56	59	1
2	12	-11	18	19	3	4	0	-10	158	158	1	2	3	8	-10	76	78	1	3	-4	-9	136	138	2
-2	13	-11	13	17	3	5	0	-10	50	47	1	3	4	8	-10	139	140	1	4	-4	-9	134	126	1
-1	13	-11	53	54	1	-5	1	-10	164	153	4	4	8	-10	60	60	1	5	-4	-9	85	84	2	
0	13	-11	28	25	1	-4	1	-10	65	76	2	5	8	-10	22	17	1	-5	-3	-9	26	22	2	
1	13	-11	58	55	1	-3	1	-10	158	167	2	-3	9	-10	60	57	2	-4	-3	-9	91	89	2	
2	13	-11	19	18	3	-2	1	-10	154	147	2	-2	9	-10	97	92	3	-3	-3	-9	98	115	3	
-1	14	-11	5	7	5	-1	1	-10	133	133	1	-1	9	-10	76	79	1	-2	-3	-9	45	46	1	
0	14	-11	30	33	1	0	1	-10	84	87	1	0	9	-10	58	55	1	-1	-3	-9	142	141	2	
-1	-8	-10	61	60	2	1	1	-10	275	283	2	1	9	-10	59	66	1	0	-3	-9	31	30	1	
0	-8	-10	86	87	2	2	1	-10	117	114	1	2	9	-10	42	37	2	1	-3	-9	39	37	1	
1	-8	-10	29	29	2	3	1	-10	14	16	1	3	9	-10	31	29	1	2	-3	-9	115	114	1	
-2	-8	-10	29	27	2	4	1	-10	193	189	2	4	9	-10	99	98	1	3	-3	-9	267	267	2	
-2	-7	-10	55	51	2	5	1	-10	116	117	1	5	9	-10	107	108	2	4	-3	-9	140	137	1	
-1	-7	-10	72	73	2	6	1	-10	75	75	1	-3	10	-10	57	57	2	5	-3	-9	47	42	1	
0	-7	-10	69	65	2	-5	2	-10	154	155	3	-2	10	-10	62	64	2	6	-3	-9	76	75	2	
1	-7	-10	62	61	1	-3	2	-10	73	79	1	-1	10	-10	136	142	2	-4	-2	-9	23	23	3	
2	-7	-10	101	97	2	-2	2	-10	64	65	1	0	10	-10	125	120	2	-4	-2	-9	104	108	3	
3	-7	-10	35	39	2	-1	2	-10	110	116	1	1	10	-10	107	104	1	-3	-2	-9	63	77	2	
-3	-6	-10	97	97	1	0	2	-10	67	64	1	2	10	-10	149	148	2	-2	-2	-9	121	120	2	
-2	-6	-10	75	76	1	1	2	-10	52	58	1	3	10	-10	13	13	2	-1	-2	-9	70	69	1	
-1	-6	-10	53	51	1	2	2	-10	42	44	1	4	10	-10	18	17	1	0	-2	-9	228	221	2	
0	-6	-10	64	62	1	3	2	-10	93	95	1	-4	11	-10	45	44	2	1	-2	-9	58	59	1	
1	-6	-10	68	68	1	4	2	-10	121	118	1	-3	11	-10	79	77	2	2	-2	-9	212	205	2	
2	-6	-10	70	68	1	5	2	-10	102	103	1	-2	11	-10	58	55	2	3	-2	-9	162	157	1	
3	-6	-10	53	52	1	6	2	-10	48	49	1	-1	11	-10	94	94	2	4	-2	-9	90	90	1	
4	-6	-10	64	63	1	-5	3	-10	233	224	5	0	11	-10	122	127	2	5	-2	-9	19	18	2	
-4	-5	-10	29	28	2	-4	3	-10	173	184	4	1	11	-10	25	29	1	6	-2	-9	110	102	3	
-3	-5	-10	126	122	2	-3	3	-10	60	56	1	3	11	-10	100	103	1	-5	-1	-9	44	47	2	
-2	-5	-10	82	76	2	-2	3	-10	128	126	1	3	11	-10	33	34	2	-3	-1	-9	126	130	2	
-1	-5	-10	142	145	2	-1	3	-10	24	25	1	4	11	-10	62	63	1	-2	-1	-9	116	121	2	
0	-5	-10	20	23	2	0	3	-10	9	8	2	-3	12	-10	38	35	2	-1	-1	-9	133	129	1	
1	-5	-10	117	118	1	1	3	-10	198	209	2	-2	12	-10	44	42	2	0	-1	-9	93	85	1	
2	-5	-10	93	95	1	2	3	-10	85	84	1	-1	12	-10	42	46	1	1	-1	-9	36	33	1	
3	-5	-10	60	62	1	3	3	-10	31	26	1	0	12	-10	65	64	1	2	-1	-9	108	105	1	
4	-5	-10	49	51	1	4	3	-10	57	55	1	1	12	-10	44	43	1	3	-1	-9	213	213	2	
5	-5	-10	27	25	2	5	3	-10	53	51	1	2	12	-10	27	25	2	4	-1	-9	155	153	1	
-4	-4	-10	17	18	5	6	3	-10	12	12	2	-2	13	-10	48	44	1	5	-1	-9	30	28	1	
-3	-4	-10	52	47	1	-5	4	-10	74	72	2	-1	13	-10	69	65	1	6	-1	-9	17	18	2	
-2	-4	-10	80	79	2	-4	4	-10	17	16	4	0	13	-10	98	93	1	-6	0	-9	32	32	2	
-1	-4	-10	46	44	1	-3	4	-10	102	103	2	1	13	-10	66	65	1	-5	0	-9	119	122	3	
0	-4	-10	171	176	2	-2	4	-10	75	77	1	2	13	-10	21	15	3	-4	0	-9	22	22	3	
1	-4	-10	29	31	1	-1	4	-10	73	66	1	-1	14	-10	101	101	1	-3	0	-9	15	13	3	
2	-4	-10	224	230	2	0	4	-10	126	124	1	0	14	-10	72	73	1	-2	0	-9	105	110	2	
3	-4	-10	109	107	2	1	4	-10	92	99	1	1	14	-10	58	59	2	-1	0	-9	327	333	3	
4	-4	-10	57	58	1	2	4	-10	98	100	1	0	-9	-9	32	31	2	0	0	-9	79	77	1	
5	-4	-10	86	85	2	3	4	-10	68	68	1	2	-9	-9	58	59	2	1	0	-9	236	243	2	
-4	-3	-10	51	51	2	4	4	-10	29	28	1	-2	-8	-9	89	81	2	2	0	-9	162	166	1	
-3	-3	-10	33	35	2	5	4	-10	77	80	1	-1	-8	-9	27	28	2	3	0	-9	236	236	2	

TABLE 7-continued

		Observed and calculated structure factors for NEL															
h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s
-2	-3	-10	85	81	2	6	4	-10	114	108	1	0	-8	-9	44	42	2
-1	-3	-10	78	82	1	-5	5	-10	92	92	2	1	-8	-9	30	29	2
0	-3	-10	109	109	1	-4	5	-10	150	149	4	2	-8	-9	54	51	1
1	-3	-10	157	164	1	-3	5	-10	82	87	1	3	-8	-9	73	74	2
2	-3	-10	69	69	1	-2	5	-10	107	107	1	-3	-7	-9	40	38	1
3	-3	-10	231	229	3	-1	5	-10	88	94	1	-2	-7	-9	89	90	2
4	-3	-10	65	65	1	0	5	-10	74	72	1	-1	-7	-9	72	72	1
5	-3	-10	17	18	3	1	5	-10	55	64	1	0	-7	-9	36	30	2
-5	-2	-10	27	23	2	2	5	-10	12	14	1	1	-7	-9	106	106	2
-4	-2	-10	30	26	2	3	5	-10	211	214	2	2	-7	-9	92	91	2
-3	-2	-10	17	15	3	4	5	-10	86	80	1	3	-7	-9	94	91	2
-1	-2	-10	62	65	1	5	5	-10	141	138	1	4	-7	-9	76	82	1
0	-2	-10	56	55	1	-5	6	-10	123	121	3	-4	-6	-9	68	71	2
1	-2	-10	98	97	1	-4	6	-10	60	58	2	-3	-6	-9	0	5	1
2	-2	-10	56	57	1	-3	6	-10	215	220	3	-2	-6	-9	116	115	3
3	-2	-10	93	96	1	-2	6	-10	72	68	1	-1	-6	-9	68	73	2
4	-2	-10	70	66	1	-1	6	-10	112	104	1	0	-6	-9	48	52	2
5	-2	-10	45	47	1	0	6	-10	137	132	1	1	-6	-9	130	128	2
0	0	-9	95	89	2	-5	-3	-8	72	71	2	4	3	-8	97	91	1
1	0	-9	97	97	1	-4	-3	-8	157	158	4	5	3	-8	47	45	1
2	0	-9	111	106	2	-3	-3	-8	193	219	5	6	3	-8	126	125	1
3	0	-9	63	63	1	-2	-3	-8	176	168	3	-6	4	-8	88	79	2
4	0	-9	79	80	1	-1	-3	-8	159	152	2	-5	4	-8	61	68	2
-4	1	-9	99	100	2	0	-3	-8	101	91	1	-4	4	-8	81	96	2
-3	1	-9	78	80	2	1	-3	-8	173	171	1	-3	4	-8	142	138	2
-2	1	-9	123	124	2	2	-3	-8	95	95	1	-2	4	-8	45	45	1
-1	1	-9	107	102	3	3	-3	-8	68	64	1	-1	4	-8	54	53	1
0	1	-9	75	72	1	4	-3	-8	231	235	2	0	4	-8	139	145	2
1	1	-9	92	89	1	5	-3	-8	27	29	1	1	4	-8	168	163	2
2	1	-9	39	37	1	6	-3	-8	32	31	1	2	4	-8	63	62	1
3	1	-9	60	61	2	-5	-2	-8	55	54	2	3	4	-8	117	123	1
4	1	-9	99	104	1	-4	-2	-8	35	32	2	4	4	-8	122	119	1
-3	12	-9	63	58	2	-3	-2	-8	142	141	2	5	4	-8	81	78	1
-1	12	-9	40	43	1	-1	-2	-8	112	103	2	-6	5	-8	36	37	2
0	12	-9	10	13	4	0	-2	-8	258	245	2	-4	5	-8	143	149	4
1	12	-9	109	111	1	1	-2	-8	32	33	1	-3	5	-8	36	34	1
2	12	-9	44	45	2	2	-2	-8	42	38	1	-2	5	-8	101	97	1
3	12	-9	10	7	5	3	-2	-8	189	188	2	-1	5	-8	166	162	1
-3	13	-9	120	118	3	4	-2	-8	201	199	2	0	5	-8	102	96	1
-2	13	-9	58	53	1	5	-2	-8	88	86	2	1	5	-8	81	85	1
-1	13	-9	35	32	1	6	-2	-8	60	57	1	2	5	-8	73	71	1
0	13	-9	58	59	1	-6	-1	-8	73	77	2	3	5	-8	170	168	1
1	13	-9	55	56	1	-5	-1	-8	35	38	2	4	5	-8	84	86	1
2	13	-9	46	42	2	-4	-1	-8	100	103	3	5	5	-8	11	14	7
-1	14	-9	30	31	1	-3	-1	-8	77	75	1	-6	6	-8	9	9	0
0	14	-9	67	65	1	-2	-1	-8	64	65	1	-5	6	-8	68	66	2
1	14	-9	20	24	3	-1	-1	-8	98	92	1	-4	6	-8	111	109	3
-2	-9	-8	54	50	2	0	-1	-8	98	89	1	-3	6	-8	102	98	2

Observed and calculated structure factors for NEL

h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s
-1	-9	-8	57	57	2	1	-1	-8	270	265	2	-2	6	-8	120	128	1
0	-9	-8	51	52	2	2	-1	-8	149	148	1	-1	6	-8	89	92	1
1	-9	-8	136	130	2	3	-1	-8	60	64	1	0	6	-8	423	414	6
2	-9	-8	25	22	3	4	-1	-8	295	296	2	2	6	-8	72	75	1
3	-9	-8	75	76	2	5	-1	-8	22	18	2	2	6	-8	179	184	1
-3	-8	-8	91	90	2	6	-1	-8	57	54	1	3	6	-8	79	81	1
-2	-8	-8	31	27	2	-6	0	-8	66	62	2	4	6	-8	245	244	4
-1	-8	-8	117	122	3	-5	0	-8	47	50	2	5	6	-8	106	106	2
0	-8	-8	22	22	3	-4	0	-8	139	139	3	-5	7	-8	85	84	2
1	-8	-8	46	46	1	-3	0	-8	58	61	1	-4	7	-8	71	70	2
2	-8	-8	106	105	2	-2	0	-8	150	144	2	-3	7	-8	120	113	1
3	-8	-8	167	165	4	-1	0	-8	138	135	1	-2	7	-8	42	40	1
4	-8	-8	32	35	1	0	0	-8	420	414	5	-1	7	-8	70	63	1
-4	-7	-8	65	71	2	1	0	-8	123	121	1	0	7	-8	109	104	1
-3	-7	-8	48	47	2	2	0	-8	111	109	1	1	7	-8	46	45	1
-2	-7	-8	71	70	2	3	0	-8	69	68	1	2	7	-8	95	94	1
-1	-7	-8	110	107	2	4	0	-8	170	173	1	3	7	-8	58	57	1
0	-7	-8	161	158	3	5	0	-8	39	36	1	4	7	-8	275	275	5
1	-7	-8	85	82	1	6	0	-8	73	73	1	-5	8	-8	43	42	2
2	-7	-8	113	109	2	-6	1	-8	34	29	2	-4	8	-8	85	81	2
3	-7	-8	33	38	1	-5	1	-8	60	60	2	-3	8	-8	133	135	3
4	-7	-8	70	69	1	-4	1	-8	126	122	3	-2	8	-8	90	92	2
5	-7	-8	25	28	3	-3	1	-8	162	159	2	-1	8	-8	76	79	1
-6	-6	-8	15	14	5	-2	1	-8	74	74	1	0	8	-8	130	124	1
-5	-6	-8	70	70	2	-1	1	-8	242	246	2	1	8	-8	48	45	1
-4	-6	-8	123	134	3	0	1	-8	95	86	1	2	8	-8	101	95	1
-3	-6	-8	113	108	2	1	1	-8	433	443	6	3	8	-8	202	194	1
-2	-6	-8	94	91	2	2	1	-8	66	64	1	4	8	-8	13	11	2
-1	-6	-8	7	3	7	3	1	-8	111	112	1	-3	9	-8	81	77	2
0	-6	-8	120	118	1	4	1	-8	27	26	1	-2	9	-8	244	251	4
1	-6	-8	84	84	1	5	1	-8	15	12	1	-1	9	-8	93	96	1
2	-6	-8	23	23	2	6	1	-8	34	33	1	0	9	-8	135	135	2
3	-6	-8	14	18	2	-6	2	-8	138	138	3	1	9	-8	254	256	

TABLE 7-continued

		Observed and calculated structure factors for NEL															
h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s
0	-4	-8	17	13	2	-3	3	-8	58	54	1	1	11	-8	48	47	1
1	-4	-8	239	242	2	-2	3	-8	120	119	1	2	11	-8	121	115	2
2	-4	-8	194	188	2	-1	3	-8	226	230	2	3	11	-8	64	61	1
3	-4	-8	106	111	1	0	3	-8	181	164	2	4	11	-8	57	57	1
4	-4	-8	85	83	1	1	3	-8	105	100	1	-3	12	-8	50	51	2
5	-4	-8	109	106	1	2	3	-8	83	74	1	-2	12	-8	171	172	3
6	-4	-8	33	39	1	3	3	-8	85	88	1	-1	12	-8	62	61	1
1	4	-7	455	435	5	-2	14	-7	79	78	1	-6	-2	-6	43	39	2
2	4	-7	51	49	1	-1	14	-7	53	59	1	-5	-2	-6	92	92	2
3	4	-7	64	64	1	0	14	-7	85	82	1	-4	4	-6	344	350	5
4	4	-7	98	91	2	1	14	-7	59	57	2	-3	-2	-6	28	23	1
5	4	-7	113	111	3	2	14	-7	36	43	2	-2	-2	-6	257	262	3
-6	5	-7	32	31	2	-2	-10	-6	16	79	2	-1	-2	-6	229	236	3
-4	5	-7	128	137	2	-1	-10	-6	78	77	2	0	-2	-6	587	573	6
-3	5	-7	226	231	3	0	-10	-6	169	162	4	1	-2	-6	115	120	1
-1	5	-7	46	48	1	3	-10	-6	107	110	3	2	-2	-6	187	182	2
0	5	-7	238	212	3	-3	-9	-6	0	9	1	4	-2	-6	37	40	1
1	5	-7	191	180	2	-2	-9	-6	75	77	2	5	-2	-6	202	199	5
2	5	-7	99	103	1	-1	-9	-6	120	118	3	6	-2	-6	57	55	1
3	5	-7	134	129	1	0	-9	-6	101	103	2	6	-1	-6	46	45	2
4	5	-7	176	177	4	1	-9	-6	108	107	2	-5	-1	-6	15	13	4
5	5	-7	168	173	4	2	-9	-6	191	192	3	-4	-1	-6	182	178	3
-6	6	-7	32	30	2	3	-9	-6	101	97	2	-3	-1	-6	51	55	1
-5	6	-7	170	162	4	4	-9	-6	17	18	3	2	-2	-6	147	139	2
-4	6	-7	43	45	2	-4	-8	-6	62	61	2	-1	-1	-6	24	17	1
-3	6	-7	93	89	1	-3	-8	-6	120	122	3	0	-1	-6	208	202	2
-2	6	-7	201	205	2	-2	-8	-6	103	111	3	1	-1	-6	71	71	1
-1	6	-7	34	27	1	-1	-8	-6	140	139	3	3	-1	-6	253	259	2
0	6	-7	41	40	1	0	-8	-6	140	139	3	3	-1	-6	115	114	1
1	6	-7	142	140	1	1	-8	-6	126	125	2	4	-1	-6	154	152	1
2	6	-7	103	99	1	2	-8	-6	151	154	2	5	-1	-6	79	81	1
3	6	-7	146	139	2	3	-8	-6	104	106	2	6	-1	-6	27	27	1
4	6	-7	94	90	2	4	-8	-6	26	25	1	-6	0	-6	82	83	2
-5	7	-7	129	129	3	5	-8	-6	55	56	2	-4	0	-6	132	131	3
-4	7	-7	164	159	4	-3	-7	-6	33	35	2	-2	0	-6	165	166	2
-3	7	-7	56	51	1	-2	-7	-6	110	127	3	-2	0	-6	77	74	1
-2	7	-7	44	46	1	-1	-7	-6	57	57	2	-1	0	-6	106	108	1
-1	7	-7	40	38	1	0	-7	-6	130	125	2	0	0	-6	379	387	3
0	7	-7	224	214	2	1	-7	-6	151	153	2	1	0	-6	165	172	1
1	7	-7	193	188	1	2	-7	-6	174	172	2	2	0	-6	322	317	4
2	7	-7	41	35	1	3	-7	-6	130	134	1	3	0	-6	112	115	1
3	7	-7	205	200	2	4	-7	-6	47	47	1	4	0	-6	200	201	1
-5	8	-7	149	147	3	5	-7	-6	76	77	1	5	0	-6	47	52	1
-4	8	-7	80	78	2	-5	-6	-6	42	40	2	6	0	-6	127	128	1
-3	8	-7	152	155	2	-4	-6	-6	86	88	2	7	0	-6	39	41	1
-2	8	-7	152	155	2	-3	-6	-6	82	84	2	-6	1	-6	44	43	2
-1	8	-7	116	116	1	-2	-6	-6	317	328	8	-5	1	-6	209	209	4

TABLE 7-continued

		Observed and calculated structure factors for NEL															
h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s
0	8	-7	136	134	1	-1	-6	-6	171	174	3	-4	1	-6	105	105	2
1	8	-7	76	71	1	0	-6	-6	13	5	3	-3	1	-6	108	105	1
2	8	-7	83	83	1	1	-6	-6	61	63	1	-2	1	-6	220	217	2
3	8	-7	230	219	2	2	-6	-6	328	333	3	-1	1	-6	345	343	4
4	8	-7	242	249	3	3	-6	-6	201	203	2	0	1	-6	280	279	2
-3	9	-7	133	123	3	4	-6	-6	134	132	2	1	1	-6	332	335	3
-2	9	-7	316	319	5	5	-6	-6	65	67	1	2	1	-6	253	245	3
-1	9	-7	65	63	1	6	-6	-6	29	34	1	3	1	-6	113	110	1
0	9	-7	67	69	1	-5	-5	-5	23	25	3	4	1	-6	126	121	1
1	9	-7	77	75	1	-4	-5	-6	75	73	2	5	1	-6	131	134	1
2	9	-7	226	235	1	-3	-5	-6	121	122	3	6	1	-6	70	76	1
3	9	-7	176	169	1	-2	-5	-6	195	190	3	7	1	-6	37	42	1
4	9	-7	86	84	1	-1	-5	-6	37	38	1	-6	2	-6	61	63	2
-3	10	-7	10	11	10	0	-5	-6	72	76	1	-5	2	-6	45	46	2
-2	10	-7	128	123	3	1	-5	-6	52	51	1	-4	2	-6	49	41	1
-1	10	-7	62	58	1	2	-5	-6	224	222	2	-3	2	-6	72	69	1
0	10	-7	99	101	1	3	-5	-6	89	89	1	-2	1	-6	98	97	1
1	10	-7	54	54	1	4	-5	-6	100	100	1	-1	2	-6	139	136	1
2	10	-7	18	12	2	5	-5	-6	105	102	1	0	2	-6	181	172	1
3	10	-7	129	133	1	6	-5	-6	74	74	1	1	2	-6	414	421	4
4	10	-7	20	27	1	-5	-4	-6	40	37	2	2	2	-6	185	180	2
-4	11	-7	85	90	2	-4	-4	-6	190	187	4	3	2	-6	229	236	2
-3	11	-7	43	43	2	-3	-4	-6	49	45	1	4	2	-6	150	154	1
-2	11	-7	174	180	2	-2	-4	-6	113	115	2	5	2	-6	85	91	1
-1	11	-7	82	89	2	-1	-4	-6	106	96	2	6	2	-6	57	56	1
0	11	-7	47	52	2	0	-4	-6	82	86	1	7	2	-6	38	44	1
1	11	-7	46	46	1	1	-4	-6	129	130	1	-6	3	-6	95	92	2
2	11	-7	282	282	4	2	-4	-6	266	266	2	-5	3	-6	42	41	2
3	11	-7	108	107	1	3	-4	-6	109	108	1	-4	3	-6	21	19	2
4	11	-7	67	68	1	4	-4	-6	48	51	1	-3	3	-6	9	2	4
-4	12	-7	17	18	4	5	-4	-6	36	38	1	-2	4	-6	121	111	2
-3	12	-7	117	117	3	6	-4	-6	15	20	3	-1	3	-6	283	281	3
-2	12	-7	89	86	1	-6	-3	-6	72	70	2	0	3	-6	164	155	1
-1	12	-7	103	109	2	-5	-3	-6	25	14	2	1	3	-6	257	254	2
0	12	-7	15	11	2	-4	-3	-6	128	129	3	2	3	-6	271	263	3
1	12	-7	81	80	1	-3	-3	-6	77	79	1	3	3	-6	83	82	1
2	12	-7	108	106	3	-2	-3	-6	182	173	3	4	3	-6	99	98	1
3	12	-7	52	55	2	-1	-3	-6	97	102	1	5	3	-6	47	45	1
4	12	-7	73	77	1	0	-3	-6	59	55	1	-6	4	-6	31	29	2
-3	13	-7	11	12	8	1	-3	-6	121	115	1	-5	4	-6	163	192	4
-2	13	-7	58	57	1	2	-3	-6	176	173	1	-4	4	-6	28	26	1
-1	13	-7	88	84	1	3	-3	-6	206	215	2	-3	4	-6	91	88	1
0	13	-7	126	134	1	4	-3	-6	101	102	1	-2	4	-6	63	57	1
1	13	-7	22	28	1	5	-3	-6	88	96	1	-1	4	-6	343	332	3
2	13	-7	80	80	2	6	-3	-6	71	68	1	0	4	-6	294	281	2
3	13	-5	135	130	1	-5	4	-5	76	79	2	3	13	-5	116	113	3
4	-3	-5	60	58	1	-4	4	-5	52	49	1	-2	13	-5	48	45	1
5	-3	-5	66	73	1	-3	4	-5	143	143	2	-1	13	-5	37	39	1
6	-3	-5	31	33	2	-2	4	-5	183	188	3	0	13	-5	81	78	1

TABLE 7-continued

Observed and calculated structure factors for NEL																							
h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s
7	-3	-5	18	16	4	-1	4	-5	223	216	3	1	13	-5	49	52	1	-5	-3	-4	162	169	4
-6	-2	-5	36	35	2	0	4	-5	368	363	3	2	13	-5	40	39	2	-4	-3	-4	50	50	2
-5	-2	-5	94	97	2	1	4	-5	271	265	2	-2	14	-5	71	70	1	-3	-3	-4	84	87	1
-4	-2	-5	250	263	4	2	4	-5	144	141	3	-1	14	-5	45	44	1	-2	-3	-4	142	135	2
-3	-2	-5	253	268	4	3	4	-5	79	81	1	0	14	-5	61	55	1	-1	-3	-4	332	336	4
-2	-2	-5	164	162	2	4	4	-5	240	224	3	1	14	-5	37	38	2	0	-3	-4	322	314	3
-1	-2	-5	178	174	2	5	4	-5	69	72	1	2	14	-5	57	63	2	1	-3	-4	330	324	3
0	-2	-5	69	69	1	-6	5	-5	67	65	2	-2	-11	-4	44	40	2	2	-3	-4	96	87	1
1	-2	-5	213	204	2	-5	5	-5	79	92	2	-1	-11	-4	130	127	3	3	-3	-4	99	90	1
2	-2	-5	93	91	1	-4	5	-5	243	241	4	0	-11	-4	89	88	2	4	-3	-4	53	55	1
3	-2	-5	208	213	1	-3	5	-5	85	86	1	1	-11	-4	72	68	2	5	-3	-4	33	34	1
4	-2	-5	140	143	1	-2	5	-5	52	48	1	2	-11	-4	35	36	2	6	-3	-4	47	50	1
5	-2	-5	107	108	1	-1	5	-5	338	331	5	3	-11	-4	92	92	2	7	-3	-4	46	46	2
6	-2	-5	78	76	1	0	5	-5	608	595	6	-3	-10	-4	120	117	3	-6	-2	-4	83	85	2
-6	-1	-5	39	40	2	1	5	-5	46	38	1	-2	-10	-4	48	49	2	-5	-2	-4	185	189	4
-5	-1	-5	130	127	3	2	5	-5	104	88	2	-1	-10	-4	58	57	2	-4	-2	-4	125	122	3
-4	-1	-5	101	101	2	3	5	-5	35	24	2	0	-10	-4	223	211	5	-3	-2	-4	68	69	1
-3	-1	-5	263	266	4	4	5	-5	149	142	2	1	-10	-4	73	68	3	-2	-2	-4	151	151	2
-2	-1	-5	176	184	2	-6	6	-5	71	67	2	2	-10	-4	30	27	2	-1	-2	-4	162	159	2
-1	-1	-5	199	206	2	-5	6	-5	58	69	2	3	-10	-4	59	57	1	0	-2	-4	300	292	3
0	-1	-5	315	324	3	-4	6	-5	242	235	4	4	-10	-4	103	102	2	1	-2	-4	32	23	1
1	-1	-5	332	325	3	-3	6	-5	204	203	2	-3	-9	-4	61	62	2	2	-2	-4	248	247	2
2	-1	-5	96	95	1	-2	6	-5	111	119	1	-2	-9	-4	111	117	3	3	-2	-4	149	152	1
3	-1	-5	101	104	1	-1	6	-5	286	278	3	-1	-9	-4	75	87	2	4	-2	-4	28	29	1
4	-1	-5	119	119	1	0	6	-5	514	492	6	0	-9	-4	29	29	3	5	-2	-4	147	144	1
5	-1	-5	111	113	1	1	6	-5	75	76	1	1	-9	-4	74	70	1	6	-2	-4	55	52	1
6	-1	-5	113	115	1	2	6	-5	78	82	1	2	-9	-4	133	133	2	7	-2	-4	97	98	2
7	-1	-5	68	63	1	3	6	-5	33	24	2	3	-9	-4	80	80	2	-6	-1	-4	25	21	3
-6	0	-5	37	38	2	-5	7	-5	101	102	3	4	-9	-4	32	34	1	-5	-1	-4	130	135	3
-5	0	-5	124	123	3	-4	7	-5	275	265	6	5	-9	-4	52	55	2	-4	-1	-4	188	195	3
-4	0	-5	42	39	1	-3	7	-5	182	187	2	-4	-8	-4	78	78	2	-3	-1	-4	183	196	4
-3	0	-5	96	101	1	-2	7	-5	129	136	1	-3	-8	-4	76	76	2	-2	-1	-4	48	46	1
-2	0	-5	314	302	3	-1	7	-5	131	130	1	-1	-8	-4	80	89	2	-1	-1	-4	166	166	2
-1	0	-5	113	115	1	0	7	-5	179	166	1	0	-8	-4	38	31	1	0	-1	-4	399	409	3
0	0	-5	307	311	2	1	7	-5	135	135	1	1	-8	-4	78	82	1	1	-1	-4	133	135	1
1	0	-5	36	42	1	2	7	-5	25	27	1	2	-8	-4	100	103	1	2	-1	-4	229	223	2
2	0	-5	21	23	1	3	7	-5	51	57	1	3	-8	-4	86	86	1	3	-1	-4	145	147	1
3	0	-5	288	285	3	-6	8	-5	78	79	2	4	-8	-4	98	100	1	4	-1	-4	87	92	1
4	0	-5	84	79	1	-5	8	-5	24	20	3	5	-8	-4	62	62	1	5	-1	-4	143	138	1
5	0	-5	138	138	1	-4	8	-5	285	281	7	-5	-7	-4	58	62	2	6	-1	-4	37	34	1
6	0	-5	40	43	1	-3	8	-5	43	37	1	-4	-7	-4	57	56	2	7	-1	-4	68	71	1
7	0	-5	48	45	1	-2	8	-5	185	188	2	-3	-7	-4	92	89	2	-6	0	-4	66	65	2
-6	1	-5	110	111	3	-1	8	-5	69	67	1	-2	-7	-4	122	122	2	-5	0	-4	168	169	4
-5	1	-5	129	128	3	0	8	-5	173	164	2	-1	-7	-4	24	19	2	-4	0	-4	192	194	3
-4	1	-5	160	164	2	1	8	-5	134	130	1	0	-7	-4	128	129	2	-3	0	-4	63	56	1
-3	1	-5	116	114	1	2	8	-5	193	202	1	1	-7	-4	89	85	1	-2	0	-4	83	87	1
-2	1	-5	109	105	1	3	8	-5	46	46	1	2	-7	-4	83	80	1	-1	0	-4	97	102	1
-1	1	-5	222	228	2	4	8	-5	88	88	1	3	-7	-4	29	29	1	0	0	-4	189	195	1
0	1	-5	190	186	1	-5	9	-5	26	27	3	4	-7	-4	50	53	1	1	0	-4	127	128	1

Observed and calculated structure factors for NEL																	
h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s
1	1	-5	247	254	2	-4	9	-5	49	49	2	5	-7	-4	66	66	1
2	1	-5	87	86	1	-3	9	-5	291	296	7	6	-7	-4	80	78	2
3	1	-5	92	87	1	-2	9	-5	257	258	4	-5	-6	-4	21	20	3
4	1	-5	168	172	1	-1	9	-5	66	67	1	-4	-6	-4	33	33	2
5	1	-5	163	160	1	0	9	-5	45	43	1	-3	-6	-4	142	144	2
6	1	-5	127	126	1	1	9	-5	83	88	1	-2	-6	-4	60	53	1
7	1	-5	52	58	1	2	9	-5	321	321	2	-1	-6	-4	114	112	2
-6	2	-5	28	30	2	3	9	-5	73	77	1	0	-6	-4	49	48	1
-5	2	-5	117	117	3	4	9	-5	68	68	1	1	-6	-4	166	170	2
-4	2	-5	21	24	2	-3	10	-5	159	160	4	2	-6	-4	210	207	2
-3	2	-5	85	88	1	-2	10	-5	141	144	2	3	-6	-4	43	40	1
-2	2	-5	157	157	2	-1	10	-5	49	52	1	4	-6	-4	79	81	1
-1	2	-5	212	209	2	0	10	-5	79	79	1	5	-6	-4	73	74	1
0	2	-5	113	106	1	1	10	-5	96	100	1	6	-6	-4	41	43	1
1	2	-5	325	328	3	2	10	-5	151	152	2	2	-5	-4	94	98	2
2	2	-5	302	291	4	3	10	-5	24	28	1	-4	-5	-4	77	79	2
4	2	-5	82	83	1	4	10	-5	80	98	1	-3	-5	-4	46	47	1
5	2	-5	173	177	2	5	10	-5	76	76	1	-2	-5	-4	136	132	2
6	2	-5	80	82	1	-3	11	-5	85	86	2	-1	-5	-4	142	142	2
7	2	-5	55	54	1	-2	11	-5	121	124	2	0	-5	-4	110	111	1
-6	3	-5	198	190	4	-1	11	-5	90	95	2	1	-5	-4	173	178	2
-5	3	-5	35	36	2	0	11	-5	70	73	1	2	-5	-4	135	138	1
-4	3	-5	95	89	1	1	11	-5	54	56	1	3	-5	-4	56	57	1
-3	3	-5	118	117	1	2	11	-5	96	95	1	4	-5	-4	36	36	1
-2	3	-5	237	231	3	3	11	-5	82	85	1	5	-5	-4	37	35	1
-1	3	-5	496	510	4	4	11	-5	37	36	1	6	-5	-4	51	47	1
0	3	-5	219	210	1	-3	12	-5	51	52	2	0	-5	-4	19	20	4
1	3	-5	175	176	1	-2	12	-5	100	100	2	-4	-4	-4	62	64	2
2	3	-5	224	220	3	-1	12	-5	59	61	1	-3	-4	-4	89	92	1
3	3	-5	59	56	1	0	12	-5	62	60	1	-2	-4	-4	48	43	1
4	3	-5	74	71	1	1	12	-5	27	26	1	-1	-4	-4	129	131	1
5	3	-5	53	53	1	2	12	-5	137	136	3	0	-4	-4	325	314	4
6	3	-5	69	81	2	3	12	-5	49	53	2	1	-4	-4	140	136	1
-6	4	-5	68	62	2	4	12	-5	45	46	2	2	-4	-4	58	50	1
3	11	-4	145	145	2	3	-5	-3	121	118	1	6	2	-3	87	107	2
4	11	-4	52	49	2	4	-5	-3	70	76	1	7	3	-3	0	8	1
5	11	-4	29	32	1	5	-5	-3	43	46	1	-6	3	-3	50	49	2
-3	12	-4	16	14	5	6	-5	-3	26	25	2	-5	3	-3	55	57	1
-2	12	-4	91	90	2	-3	-4	-3	19	22	3	-4	3	-3	127	124	2
-1	12	-4	48	47	1	-2	-4	-3	183	168	2	-3	3	-3	84	75	2
0	12	-4	57	59	1	-1	-4	-3	136	145	1	-2	3	-3	89	84	2
1	12	-4	43	44	1	0	-4	-3	127	123	2	0	1	3	279	295	3
2	12	-4	101	100	1	1	-4	-3	208	213	2	0	3	-3	320	320	3
3	12	-4	160	164	4	2	-4	-3	351	355	5	1	3	-3	259	259	2
-3	13	-4	55	55	2	3	-4	-3	73	72	1	3	3	-3	44	38	2
-2	13	-4	90	89	1	4	-4	-3	125	122	1	4	3	-3	58	59	1
-1	13	-4	77	79	1	5	-4	-3	52	58	1	5	3	-3	176	181	4
0	13	-4	58	56	1	6	-4	-3	68	70	1	6	3	-3	154	171	3
1	13	-4	55	55	1	7	-4	-3	50	52	2	-7	4	-3	33	33	2

TABLE 7-continued

Observed and calculated structure factors for NEL																														
h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s							
2	13	-4	47	48	2	-3	-3	-3	181	177	4	-6	4	-3	53	48	2	0	12	-3	42	47	1	-1	-4	-2	221	222	2	2
-2	14	-4	46	49	1	-2	-3	-3	175	171	2	-5	4	-3	28	29	2	1	12	-3	55	53	1	0	-4	-2	174	176	1	1
-1	14	-4	41	39	1	-1	-3	-3	84	78	1	-4	4	-3	197	191	3	2	12	-3	71	70	1	1	-4	-2	103	101	2	2
0	14	-4	11	10	2	0	-3	-3	533	535	6	-3	4	-3	106	101	1	3	12	-3	104	109	2	2	-4	-2	230	210	4	4
1	14	-4	56	57	2	1	-3	-3	101	99	1	-2	4	-3	142	145	3	-3	13	-3	72	71	2	3	-4	-2	147	148	1	1
-2	-12	-3	71	68	2	2	-3	-3	242	237	3	-1	4	-3	111	117	1	-2	13	-3	49	45	1	4	-4	-2	83	81	1	1
-1	-12	-3	85	83	2	3	-3	-3	280	275	2	0	4	-3	134	139	1	-1	13	-3	3	12	2	5	-4	-2	65	66	1	1
1	-12	-3	39	38	3	4	-3	-3	19	22	1	1	4	-3	178	170	1	0	13	-3	20	22	1	6	-4	-2	76	75	1	3
-3	-11	-3	24	22	2	5	-3	-3	124	122	1	3	4	-3	91	89	1	1	13	-3	17	18	1	7	-4	-2	114	113	3	3
-2	-11	-3	38	34	2	6	-3	-3	79	81	1	4	4	-3	39	42	1	2	13	-3	64	61	2	-3	-3	-2	82	78	2	2
-1	-11	-3	60	60	2	7	-3	-3	138	125	3	5	4	-3	246	241	5	-2	14	-3	63	62	2	-2	-3	-2	311	313	6	3
0	-11	-3	29	26	2	-3	-2	-3	196	202	3	6	4	-3	123	112	3	-1	14	-3	33	34	1	-1	-3	-2	309	295	3	3
1	-11	-3	67	68	3	-2	-2	-3	322	335	5	-7	5	-3	27	22	2	0	14	-3	34	30	1	0	-3	-2	116	120	1	1
2	-11	-3	121	118	2	-1	-2	-3	706	721	7	-5	5	-3	103	126	3	-2	-12	-2	54	53	2	2	-3	-2	190	186	1	1
3	-11	-3	25	18	2	0	-2	-3	101	104	1	-4	5	-3	119	113	2	-1	-12	-2	68	65	2	3	-3	-2	209	203	2	2
4	-11	-3	34	40	2	1	-2	-3	101	104	1	-4	5	-3	119	113	2	-1	-12	-2	70	71	1	4	-3	-2	126	123	1	1
-4	-10	-3	71	70	2	2	-2	-3	443	435	4	-3	5	-3	45	43	1	0	-12	-2	49	48	3	5	-3	-2	47	44	1	1
-3	-10	-3	43	38	2	3	-2	-3	153	145	1	-2	5	-3	169	171	2	1	-12	-2	49	48	3	5	-3	-2	47	44	1	1
-2	-10	-3	22	19	3	4	-2	-3	198	203	1	-1	5	-3	206	201	4	2	-12	-2	43	41	2	6	-3	-2	67	67	1	1
-1	-10	-3	63	65	2	5	-2	-3	61	60	1	0	5	-3	92	91	1	3	-12	-2	39	37	1	7	-3	-2	55	55	2	2
0	-10	-3	45	38	2	6	-2	-3	21	20	1	1	5	-3	385	374	4	-3	-11	-2	28	27	2	3	-2	-2	314	315	6	6
1	-10	-3	28	23	4	-3	-1	-3	121	124	2	3	5	-3	205	195	3	-2	-11	-2	85	81	2	-2	-2	-2	399	379	6	6
2	-10	-3	123	119	2	-2	-1	-3	229	233	2	4	5	-3	43	39	2	-1	-11	-2	135	133	3	-1	-2	-2	430	439	5	5
3	-10	-3	94	95	2	-1	-1	-3	248	259	3	5	5	-3	161	157	3	0	-11	-2	56	53	2	0	-2	-2	168	169	2	2
4	-10	-3	22	22	2	0	-1	-3	538	566	5	-6	6	-3	44	42	2	1	-11	-2	57	56	3	1	-2	-2	624	638	5	5
-4	-9	-3	83	80	2	1	-1	-3	385	400	3	-5	6	-3	32	37	2	2	-11	-2	50	48	1	3	-2	-2	291	284	2	2
-3	-9	-3	58	59	2	2	-1	-3	259	257	2	-4	6	-3	186	186	3	3	-11	-2	67	66	1	3	-2	-2	143	142	1	1
-2	-9	-3	82	83	2	3	-1	-3	366	349	4	-3	6	-3	80	78	1	4	-11	-2	27	26	2	4	-2	-2	95	96	1	1
-1	-9	-3	89	116	2	4	-1	-3	47	52	1	-2	6	-3	48	50	1	-4	-10	-2	98	102	2	5	-2	-2	188	185	1	1
0	-9	-3	50	48	2	5	-1	-3	35	33	1	-1	6	-3	391	391	5	-3	-10	-2	79	83	2	6	-2	-2	17	17	1	1
1	-9	-3	74	77	1	6	-1	-3	141	144	1	0	6	-3	176	170	2	-2	-10	-2	59	59	2	7	-2	-2	20	18	3	3
2	-9	-3	96	101	2	7	-1	-3	42	40	1	1	6	-3	315	315	3	-1	-10	-2	54	63	2	-3	-1	-2	158	165	4	4
3	-9	-3	67	66	1	-7	0	-3	17	22	4	2	6	-3	160	156	1	0	-10	-2	12	12	6	-2	-1	-2	288	287	4	4
4	-9	-3	38	37	1	-6	0	-3	16	7	4	3	6	-3	96	104	1	1	-10	-2	61	62	2	-1	-1	-2	422	425	6	6
5	-9	-3	30	37	1	-4	0	-3	151	151	3	4	6	-3	135	137	3	2	-10	-2	105	102	2	0	-1	-2	605	633	7	7
-5	-8	-3	28	31	2	-3	0	-3	179	173	2	-6	7	-3	13	12	5	3	-10	-2	91	91	2	1	-1	-2	474	489	4	4
-4	-8	-3	56	54	2	-2	0	-3	205	208	2	-5	7	-3	40	43	2	4	-10	-2	40	40	1	2	-1	-2	110	105	1	1
-3	-8	-3	99	103	2	-1	0	-3	179	189	2	-4	7	-3	135	133	2	5	-10	-2	27	26	3	3	-1	-2	121	115	1	1
-2	-8	-3	76	76	2	0	0	-3	181	191	1	-3	7	-3	128	127	1	-4	-9	-2	75	80	2	4	-1	-2	147	142	1	1
0	-8	-3	21	14	2	1	0	-3	90	91	1	-2	7	-3	149	152	1	-4	-9	-2	91	96	2	5	-1	-2	36	34	1	1
1	-8	-3	61	63	1	2	0	-3	98	91	1	-1	7	-3	190	193	2	-1	-9	-2	149	155	4	6	-1	-2	98	102	1	1
2	-8	-3	96	96	1	3	0	-3	229	225	2	0	7	-3	214	209	2	1	-9	-2	172	178	2	7	-1	-2	14	9	2	2
3	-8	-3	42	50	1	4	0	-3	209	208	2	1	7	-3	183	192	1	2	-9	-2	61	60	2	-3	0	-2	327	320	5	5
4	-8	-3	151	183	3	5	0	-3	113	113	1	3	7	-3	80	70	1	3	-9	-2	189	193	3	-2	0	-2	194	195	2	2
5	-8	-3	63	62	1	6	0	-3	180	178	1	2	7	-3	68	63	1	4	-9	-2	63	62	1	-1	0	-2	283	295	4	4
-5	-7	-3	22	21	3	7	0	-3	113	111	1	-5	8	-3	38	33	2	5	-9	-2	9	10	5	0	0	-2	448	469	4	4
-4	-7	-3	43	40	2	-7	1	-3	58	58	2	-4	8	-3	39	39	2	-4	-8	-2	67	72	2	1	0	-2	255	264	2	2
-3	-7	-3	133	135	3	-6	1	-3	108	101	2	-3	8	-3	139	141	1	-3	-8	-2	41	47	2	2	0	-2	197	198	2	2
-1	-7	-3	153	152	2	-5	1	-3	138	128	3	-2	8	-3	195	197	2	-2	-8	-2	84	84	1	3	0	-2	53	62	1	1

TABLE 7-continued

Observed and calculated structure factors for NEL																													
h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s						
1	-7	-3	136	138	1	-4	1	-3	167	166	2	-1	8	-3	76	80	1	-1	-8	-2	184	182	3	4	0	-2	200	199	2
2	-7	-3	145	144	1	-3	1	-3	119	108	2	0	8	-3	141	129	1	0	-8	-2	57	56	1	5	0	-2	126	125	1
3	-7	-3	79	82	1	-2	1	-3	136	140	1	1	8	-3	52	54	1	1	-8	-2	23	23	1	6	0	-2	49	48	1
4	-7	-3	127	146	2	-1	1	-3	156	169	2	2	8	-3	84	79	1	2	-8	-2	123	120	1	7	0	-2	39	35	1
5	-7	-3	42	47	1	0	1	-3	193	195	1	3	8	-3	168	165	1	3	-8	-2	78	79	1	-7	1	-2	33	37	2
6	-7	-3	58	59	1	1	1	-3	93	95	1	4	8	-3	86	92	1	4	-8	-2	65	72	1	-6	1	-2	65	62	2
-4	-6	-3	178	174	4	2	1	-3	131	133	1	-5	9	-3	72	73	2	5	-8	-2	102	102	1	-5	1	-2	41	42	2
-3	-6	-3	162	164	2	4	1	-3	229	226	2	-4	9	-3	67	71	2	6	-8	-2	78	77	2	-4	1	-2	149	149	3
-2	-6	-3	200	196	3	5	1	-3	98	97	1	-3	9	-3	145	145	3	-4	-7	-2	103	105	2	-3	1	-2	179	168	2
-1	-6	-3	163	164	2	6	1	-3	135	136	1	-2	9	-3	101	100	1	-2	-7	-2	119	122	2	-2	1	-2	97	101	1
0	-6	-3	174	169	1	7	1	-3	56	51	1	-1	9	-3	120	113	1	-1	-7	-2	91	88	1	-1	1	-2	299	306	4
1	-6	-3	111	114	1	-7	2	-3	68	70	2	0	9	-3	255	256	2	0	-7	-2	92	92	1	0	1	-2	381	397	3
2	-6	-3	83	81	1	-6	2	-3	135	129	3	1	9	-3	46	43	1	1	-7	-2	91	86	1	1	1	-2	226	235	2
3	-6	-3	69	71	1	-5	2	-3	154	154	2	2	9	-3	74	74	1	2	-7	-2	29	27	1	2	1	-2	361	374	8
4	-6	-3	41	46	1	-4	2	-3	49	51	1	3	9	-3	42	41	1	3	-7	-2	107	113	1	3	1	-2	69	65	2
5	-6	-3	74	79	1	-3	2	-3	4	4	4	4	9	-3	75	74	1	4	-7	-2	45	48	1	4	1	-2	180	184	1
6	-6	-3	56	55	1	-2	2	-3	160	156	2	5	9	-3	35	36	1	5	-7	-2	78	75	1	5	1	-2	172	172	2
-3	-5	-3	61	60	1	-1	2	-3	458	468	6	-3	10	-3	61	64	2	6	-7	-2	39	39	1	6	1	-2	37	33	1
-2	-5	-3	230	233	3	0	2	-3	143	147	1	-2	10	-3	218	213	3	-6	-6	-2	143	146	3	7	1	-2	64	64	1
-1	-5	-3	115	118	1	1	2	-3	177	183	1	-1	10	-3	139	142	1	-1	-6	-2	133	131	2	-7	2	-2	25	28	3
0	-5	-3	251	244	3	3	2	-3	133	128	3	0	10	-3	29	30	1	-1	-6	-2	19	19	1	-6	2	-2	120	119	3
1	-5	-3	206	202	2	4	2	-3	158	159	2	1	10	-3	230	240	2	0	-6	-2	129	131	1	-5	2	-2	109	99	2
2	-5	-3	231	236	2	5	2	-3	233	227	3	2	10	-3	140	138	2	1	-6	-2	75	74	1	-4	2	-2	53	50	1
-3	2	-2	115	119	2	-4	9	-2	32	35	2	-1	-7	-1	61	62	1	4	1	-1	94	96	1	-5	8	-1	55	54	2
-2	2	-2	228	229	3	-3	9	-2	65	64	1	0	-7	-1	83	86	1	5	1	-1	177	182	2	-4	8	-1	121	116	3
-1	2	-2	436	445	6	-2	9	-2	74	75	1	1	-7	-1	99	100	1	6	1	-1	76	79	1	-3	8	-1	80	77	1
0	2	-2	578	596	5	-1	9	-2	133	129	1	2	-7	-1	109	109	1	7	1	-1	49	44	1	-2	8	-1	61	62	1
1	2	-2	378	390	3	0	9	-2	29	32	1	3	-7	-1	132	134	1	-7	2	-1	94	93	2	-1	8	-1	150	149	1
2	2	-2	191	219	4	1	9	-2	147	145	1	4	-7	-1	130	136	1	-6	2	-1	43	40	2	0	8	-1	108	109	1
3	2	-2	163	164	4	2	9	-2	53	52	1	5	-7	-1	12	13	3	-5	2	-1	218	218	5	1	8	-1	70	73	1
4	2	-2	136	132	1	3	9	-2	80	77	1	6	-7	-1	54	55	1	-4	2	-1	69	71	1	2	8	-1	150	149	1
5	2	-2	32	36	2	4	9	-2	14	9	2	-2	-6	-1	133	142	3	-3	2	-1	237	242	5	3	8	-1	91	95	1
6	2	-2	49	56	2	5	9	-2	80	79	1	-1	-6	-1	70	66	2	-2	2	-1	222	217	2	4	8	-1	126	116	1
7	2	-2	18	13	1	-3	10	-2	65	59	2	0	-6	-1	64	62	1	-1	2	-1	665	679	7	5	8	-1	45	40	1
-7	3	-2	62	59	2	-2	10	-2	182	182	3	1	-6	-1	180	175	2	0	2	-1	273	281	2	-5	9	-1	0	8	1
-6	3	-2	31	30	2	-1	10	-2	88	89	1	2	-6	-1	55	51	1	1	2	-1	600	624	5	-4	9	-1	51	50	2
-5	3	-2	26	23	2	0	10	-2	24	28	1	3	-6	-1	162	158	1	2	2	-1	213	253	5	-3	9	-1	46	47	2
-4	3	-2	154	155	2	1	10	-2	58	60	1	4	-6	-1	117	111	1	3	2	-1	913	392	9	-2	9	-1	98	96	1
-3	3	-2	111	110	2	2	10	-2	96	97	1	5	-6	-1	21	23	1	4	2	-1	133	137	1	-1	9	-1	13	8	2
-2	3	-2	182	183	2	3	10	-2	98	95	1	6	-6	-1	77	71	1	5	2	-1	197	189	4	0	9	-1	149	147	1
-1	3	-2	77	75	1	4	10	-2	32	33	1	-2	-5	-1	153	147	2	6	2	-1	19	19	1	1	9	-1	123	117	1
0	3	-2	68	70	1	5	10	-2	61	55	1	-1	-5	-1	131	137	2	7	2	-1	37	27	1	2	9	-1	188	192	1
1	3	-2	293	307	2	-3	11	-2	92	90	2	0	-5	-1	160	162	2	-7	3	-1	57	54	2	3	9	-1	127	125	1
2	3	-2	194	193	4	-2	11	-2	111	112	2	1	-5	-1	76	77	1	-6	3	-1	62	63	2	4	9	-1	42	45	1
3	3	-2	46	50	1	-1	11	-2	158	163	2	2	-5	-1	164	157	2	-5	3	-1	277	279	4	5	9	-1	70	65	1
4	3	-2	53	55	2	0	11	-2	105	103	2	3	-5	-1	189	173	2	-4	3	-1	76	71	1	-3	10	-1	41	46	3
5	3	-2	52	45	2	1	11	-2	107	109	1	4	-5	-1	127	123	1	-3	3	-1	221	210	4	-2	10	-1	44	38	1
6	3	-2	30	26	2	2	11	-2	104	104	2	5	-5	-1	35	32	1	-2	3	-1	377	386	4	-1	10	-1	88	91	1
-7	4	-2	130	127	3	3	11	-2	75	75	2	6	-5	-1	134	133	2	-1	3	-1	145	148	1	0	10	-1	20	19	1

TABLE 7-continued

		Observed and calculated structure factors for NEL															
h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s
-5	4	-2	111	116	2	-3	12	-2	69	65	2	-3	-4	-1	25	31	2
-4	4	-2	195	194	3	-2	12	-2	102	105	2	-2	-4	-1	213	190	3
-3	4	-2	147	150	2	-1	12	-2	43	40	1	-1	-4	-1	155	152	2
-2	4	-2	320	304	6	0	12	-2	80	81	1	0	-4	-1	341	354	5
-1	4	-2	55	52	1	1	12	-2	39	34	1	1	-4	-1	31	32	1
0	4	-2	208	208	1	2	12	-2	93	96	1	2	-4	-1	476	461	5
1	4	-2	181	186	2	3	12	-2	23	25	2	3	-4	-1	150	148	1
3	4	-2	210	212	3	-3	13	-2	53	54	2	4	-4	-1	57	57	1
4	4	-2	33	30	1	-2	13	-2	72	73	1	5	-4	-1	179	179	1
5	4	-2	90	85	2	-1	13	-2	38	42	1	6	-4	-1	87	81	2
6	4	-2	199	197	4	0	13	-2	67	64	1	-3	-3	-1	338	340	7
-7	5	-2	25	28	2	1	13	-2	14	14	1	-2	-3	-1	72	72	1
-6	5	-2	118	116	3	2	13	-2	96	97	2	-1	-3	-1	421	421	5
-5	5	-2	86	98	2	-1	14	-2	28	30	1	0	-3	-1	376	382	4
-4	5	-2	49	50	1	0	14	-2	44	45	1	1	-3	-1	398	401	3
-3	5	-2	103	97	1	1	14	-2	82	83	2	2	-3	-1	63	56	1
-2	5	-2	65	61	1	-1	-13	-1	42	42	2	3	-3	-1	339	317	4
-1	5	-2	350	355	7	0	-13	-1	101	101	3	4	-3	-1	118	118	1
0	5	-2	106	113	1	1	-13	-1	64	64	2	5	-3	-1	130	132	1
1	5	-2	227	219	2	-3	-12	-1	34	37	2	6	-3	-1	70	74	1
2	5	-2	321	322	5	-2	-12	-1	89	88	2	-3	-2	-1	272	260	5
3	5	-2	211	206	3	-1	-12	-1	48	46	2	2	-2	-1	123	120	2
4	5	-2	109	107	2	0	-12	-1	32	29	2	-1	-2	-1	659	682	10
5	5	-2	25	27	2	1	-12	-1	132	130	3	0	-2	-1	808	843	10
6	5	-2	122	113	2	2	-12	-1	164	162	3	1	-2	-1	784	818	6
-6	6	-2	34	33	2	3	-12	-1	42	45	1	2	-2	-1	412	405	3
-5	6	-2	73	82	2	-3	-11	-1	46	45	2	3	-2	-1	380	360	4
-4	6	-2	147	148	2	-2	-11	-1	128	130	3	4	-2	-1	133	130	1
-3	6	-2	152	151	2	-1	-11	-1	73	78	2	5	-2	-1	117	112	1
-2	6	-2	105	93	1	0	-11	-1	74	72	2	6	-2	-1	72	72	1
-1	6	-2	338	327	5	2	-11	-1	152	153	2	7	-2	-1	151	147	3
0	6	-2	232	232	2	3	-11	-1	114	113	2	-3	-1	-1	121	114	2
1	6	-2	97	96	1	4	-11	-1	11	9	5	-2	-1	-1	151	147	3
2	6	-2	265	270	2	-4	-10	-1	73	77	2	-1	-1	-1	608	629	12
3	6	-2	120	115	1	-3	-10	-1	6	8	6	0	-1	-1	146	147	2
4	6	-2	98	91	2	1	-10	-1	35	35	2	1	-1	-1	821	845	7
5	6	-2	63	63	2	2	-10	-1	57	51	1	2	-1	-1	215	215	1
-6	7	-2	23	18	3	3	-10	-1	21	22	2	4	-1	-1	426	407	4
-5	7	-2	48	52	2	4	-10	-1	42	43	2	4	-1	-1	48	51	1
-4	7	-2	135	142	2	5	-10	-1	28	34	2	5	-1	-1	195	195	1
-3	7	-2	81	79	1	-4	-9	-1	79	85	2	6	-1	-1	63	65	1
-2	7	-2	117	116	1	-2	-9	-1	124	122	3	7	-1	-1	11	3	3
-1	7	-2	138	141	1	-1	-9	-1	79	77	1	-3	0	-1	90	92	1
0	7	-2	155	152	1	0	-9	-1	146	151	2	-1	0	-1	120	127	2
1	7	-2	49	53	1	1	-9	-1	42	35	2	0	0	-1	76	82	1
2	7	-2	90	96	1	2	-9	-1	178	178	2	1	0	-1	53	54	1
3	7	-2	221	221	2	3	-9	-1	28	32	2	2	0	-1	406	401	3
4	7	-2	12	12	6	4	-9	-1	129	136	2	3	0	-1	101	98	1
-6	8	-2	20	20	3	5	-9	-1	98	97	1	4	0	-1	219	221	2

TABLE 7-continued

Observed and calculated structure factors for NEL																		
h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s	
-5	8	-2	34	67	2	5	0	-1	136	137	1	-5	7	-1	34	40	2	
-4	8	-2	86	181	3	6	0	-1	38	32	1	-4	7	-1	114	117	2	
-3	8	-2	167	141	2	7	0	-1	20	21	1	-3	7	-1	176	173	3	
-2	8	-2	84	53	1	0	-1	-1	84	79	2	-2	7	-1	107	102	1	
-1	8	-2	58	60	1	1	-1	-1	173	167	4	-1	7	-1	155	159	1	
0	8	-2	39	41	1	2	-1	-1	127	118	2	0	7	-1	139	138	1	
1	8	-2	126	123	1	3	-1	-1	458	459	7	1	7	-1	134	136	1	
2	8	-2	181	183	1	4	-1	-1	566	583	8	2	7	-1	72	75	1	
3	8	-2	25	21	1	5	1	-1	368	385	3	3	7	-1	226	218	2	
4	8	-2	113	114	1	6	-1	-1	930	924	21	4	7	-1	63	65	1	
5	8	-2	43	38	1	-3	-1	-1	280	280	6	5	7	-1	25	27	4	
-5	9	-2	29	27	2	2	3	1	-1	227	201	5	-6	8	-1	35	37	2
-2	-8	0	23	24	2	0	1	0	140	148	1	5	7	0	115	114	1	
-1	-8	0	138	136	3	1	1	0	828	873	7	6	7	0	12	6	3	
0	-8	0	47	43	1	2	1	0	225	227	3	-6	8	0	64	66	2	
1	-8	0	215	216	2	3	1	0	264	260	6	-5	8	0	76	75	2	
2	-8	0	38	36	1	4	1	0	68	67	1	-4	8	0	13	9	8	
3	-8	0	61	64	1	5	1	0	104	103	1	-3	8	0	61	64	1	
4	-8	0	7	9	6	6	1	0	165	171	1	-2	8	0	41	36	1	
5	-8	0	76	75	1	7	1	0	72	70	1	-1	8	0	215	216	2	
6	-8	0	66	65	1	-7	2	0	66	63	2	0	8	0	47	43	1	
-2	-7	0	178	176	4	-6	2	0	182	183	4	1	8	0	137	137	1	
-1	-7	0	224	222	5	-5	2	0	121	119	3	2	8	0	25	24	1	
0	-7	0	71	74	1	-4	2	0	142	138	2	3	8	0	130	129	1	
1	-7	0	164	168	2	-3	2	0	412	403	9	4	8	0	127	125	1	
2	-7	0	195	195	2	-2	2	0	270	259	3	-5	8	0	66	62	1	
3	-7	0	125	116	1	-1	2	0	243	250	3	-5	9	0	89	92	2	
4	-7	0	70	70	1	0	2	0	597	604	5	-4	9	0	22	20	3	
5	-7	0	100	94	1	1	2	0	350	368	3	-3	9	0	46	49	2	
6	-7	0	73	71	1	3	2	0	142	144	3	-2	9	0	54	52	1	
-2	-6	0	143	137	3	4	2	0	80	76	1	-1	9	0	33	35	1	
-1	-6	0	50	52	1	5	2	0	34	30	1	0	9	0	99	95	1	
0	-6	0	65	66	1	6	2	0	76	80	1	1	9	0	77	76	1	
1	-6	0	111	108	1	7	2	0	60	59	1	2	9	0	114	113	1	
2	-6	0	142	135	1	-7	3	0	77	74	2	3	9	0	73	70	2	
3	-6	0	69	68	1	-6	3	0	171	167	4	4	9	0	108	105	1	
4	-6	0	108	106	1	-5	3	0	47	48	1	5	9	0	55	58	1	
5	-6	0	91	92	1	-4	3	0	44	39	1	-3	10	0	90	93	2	
6	-6	0	138	136	2	-3	3	0	229	213	5	-2	10	0	107	103	2	
-2	-5	0	177	166	2	-2	3	0	201	196	2	-1	10	0	239	243	4	
-1	-5	0	133	132	1	-1	3	0	411	416	5	0	10	0	80	78	1	
0	-5	0	26	26	1	0	3	0	882	918	7	1	10	0	134	157	2	
1	-5	0	161	165	1	1	3	0	295	292	2	2	10	0	58	56	1	
2	-5	0	94	85	1	2	3	0	201	201	2	3	10	0	102	104	2	
3	-5	0	191	183	2	3	3	0	108	109	3	-3	11	0	95	93	2	
4	-5	0	61	55	1	4	3	0	50	48	1	-2	11	0	80	80	1	
5	-5	0	15	17	2	5	3	0	110	103	2	-1	11	0	72	75	1	
6	-5	0	100	98	2	6	3	0	43	47	1	0	11	0	166	165	3	
-2	-4	0	647	625	10	7	3	0	20	19	1	1	11	0	115	119	1	

TABLE 7-continued

Observed and calculated structure factors for NEL																							
h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s
-1	-4	0	121	120	1	-7	4	0	52	53	2	2	11	0	73	72	1	-2	-4	1	160	147	2
0	-4	0	63	66	1	-6	4	0	133	131	3	3	11	0	35	32	2	-1	-4	1	154	147	1
1	-4	0	131	134	1	-5	4	0	106	104	2	-3	12	0	35	36	2	0	-4	1	456	464	5
2	-4	0	348	337	4	-4	4	0	27	29	1	-2	12	0	121	122	2	1	-4	1	57	58	1
3	-4	0	219	217	2	-3	4	0	220	216	3	-1	12	0	99	98	1	2	-4	1	218	219	2
4	-4	0	27	29	1	-2	4	0	352	337	7	0	12	0	66	65	1	3	-4	1	207	210	2
5	-4	0	105	104	1	-1	4	0	130	134	1	1	12	0	247	240	3	4	-4	1	140	142	1
6	-4	0	134	130	2	0	4	0	65	67	1	2	12	0	44	41	2	5	-4	1	145	147	1
-2	-3	0	202	200	3	1	4	0	120	120	1	3	12	0	25	25	2	6	-4	1	36	33	1
-1	-3	0	292	291	3	2	4	0	658	625	8	-2	13	0	105	104	2	-2	-3	1	199	197	4
0	-3	0	888	919	9	3	4	0	100	94	2	-1	13	0	110	109	1	-1	-3	1	296	296	3
1	-3	0	407	416	3	4	4	0	101	95	2	0	13	0	78	75	1	0	-3	1	298	297	4
2	-3	0	206	198	2	5	4	0	38	40	1	1	13	0	138	143	2	1	-3	1	142	148	1
3	-3	0	224	213	2	6	4	0	110	116	1	2	13	0	78	79	2	2	-3	1	384	387	3
4	-3	0	45	39	1	-7	5	0	113	103	3	0	-14	1	13	11	8	3	-3	1	215	210	2
5	-3	0	45	48	1	-6	5	0	96	97	2	1	-14	1	57	62	2	4	-3	1	77	71	1
6	-3	0	172	167	2	-5	5	0	11	18	7	-2	-13	1	172	170	4	5	-3	1	277	280	2
7	-3	0	74	74	2	-4	5	0	59	55	1	-1	-13	1	89	83	2	6	-3	1	60	63	1
0	-2	0	599	604	7	-3	5	0	195	183	3	0	-13	1	36	35	2	7	-3	1	58	54	2
1	-2	0	242	250	2	-2	5	0	91	84	2	1	-13	1	54	51	3	-1	-2	1	590	624	14
2	-2	0	271	260	2	-1	5	0	167	166	2	2	-13	1	19	20	5	0	-2	1	-281	281	3
3	-2	0	413	402	4	0	5	0	26	26	1	3	-13	1	48	50	2	1	-2	1	642	679	6
4	-2	0	146	138	1	1	5	0	135	133	1	-3	-12	1	35	35	2	2	-2	1	220	217	2
5	-2	0	124	119	1	2	5	0	178	166	2	-1	-12	1	53	54	2	3	-2	1	239	241	2
6	-2	0	185	184	1	3	5	0	90	79	1	4	-12	1	57	59	1	4	-2	1	69	72	1
7	-2	0	63	63	2	4	5	0	106	107	1	3	-12	1	55	53	1	5	-2	1	220	218	2
-3	-1	0	263	260	3	5	5	0	58	58	1	4	-12	1	53	51	1	6	-2	1	40	39	1
-2	-1	0	224	227	4	6	5	0	48	56	1	-4	-11	1	18	22	3	7	-2	1	92	94	2
-1	-1	0	761	873	18	-6	6	0	143	136	3	-2	-11	1	91	89	2	0	-1	1	377	385	8
0	-1	0	138	148	1	-4	6	0	106	105	2	-1	-11	1	57	68	2	1	-1	1	556	583	5
1	-1	0	787	821	7	-3	6	0	68	68	1	0	-11	1	37	36	2	2	-1	1	458	459	4
2	-1	0	307	298	2	-2	6	0	142	135	2	2	-11	1	57	60	2	3	-1	1	126	118	1
3	-1	0	219	217	2	-1	6	0	113	108	1	3	-11	1	98	98	2	4	-1	1	176	167	1
4	-1	0	62	60	1	0	6	0	67	65	1	4	-11	1	59	56	1	5	-1	1	243	241	2
5	-1	0	108	105	1	1	6	0	51	52	1	-4	-10	1	12	10	9	6	-1	1	126	121	1
6	-1	0	44	45	1	2	6	0	142	136	1	-3	-10	1	89	90	2	7	-1	1	86	80	2
7	-1	0	38	43	1	3	6	0	180	177	1	-2	-10	1	101	94	2	-3	0	1	98	98	2
-2	0	0	118	117	2	4	6	0	125	133	1	-1	-10	1	116	121	3	-2	0	1	411	402	8
-1	0	0	348	341	7	5	6	0	28	33	1	0	-10	1	17	18	3	-1	0	1	52	55	1
1	0	0	126	133	2	6	6	0	28	18	1	1	-10	1	87	92	1	0	0	1	123	127	1
2	0	0	344	341	3	-4	7	0	69	71	2	3	-10	1	44	38	2	1	0	1	195	197	2
3	0	0	119	117	1	-3	7	0	125	117	2	4	-10	1	106	103	2	3	0	1	92	93	1
4	0	0	307	302	3	-2	7	0	196	196	2	5	-10	1	6	5	6	4	0	1	146	146	1
5	0	0	12	8	2	-1	7	0	165	168	1	-3	-9	1	124	125	3	5	0	1	74	78	1
6	0	0	45	38	1	0	7	0	71	74	1	-1	-9	1	123	117	3	6	0	1	94	91	1
7	0	0	64	63	1	1	7	0	219	222	2	0	-9	1	143	147	2	7	0	1	96	91	1
-3	1	0	214	218	5	2	7	0	184	177	1	1	-9	1	14	8	3	-3	1	1	420	408	9
-2	1	0	304	297	3	3	7	0	88	88	1	2	-9	1	97	95	2	-2	1	1	212	214	2

TABLE 7-continued

		Observed and calculated structure factors for NEL															
h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s
-1	1	0	792	821	9	4	7	0	68	72	1	3	-9	1	47	46	1
2	7	1	92	91	1	2	-9	2	73	75	1	7	0	2	60	64	1
3	7	1	68	74	1	3	-9	2	69	64	1	-3	1	2	117	115	2
4	7	1	71	74	1	4	-9	2	37	36	1	-2	1	2	110	105	1
5	7	1	63	60	1	5	-9	2	29	27	1	-1	1	2	479	489	5
6	7	1	66	69	1	-2	-8	2	179	183	3	0	1	2	604	633	5
-5	8	1	83	87	2	-1	-8	2	123	123	2	1	1	2	417	426	3
-4	8	1	107	101	3	0	-8	2	38	41	1	2	1	2	295	287	3
-3	8	1	140	142	2	1	-8	2	59	61	1	3	1	2	167	165	1
-2	8	1	130	131	1	2	-8	2	86	84	1	4	1	2	182	181	1
-1	8	1	60	62	1	3	-8	2	170	167	1	5	1	2	31	30	1
0	8	1	52	53	1	4	-8	2	85	88	1	6	1	2	112	107	1
1	8	1	137	141	1	5	-8	2	33	33	1	7	1	2	51	52	1
2	8	1	181	181	1	6	-8	2	25	20	2	-7	2	2	25	18	3
3	8	1	67	67	1	-2	-7	2	93	95	2	-6	2	2	17	17	4
4	8	1	152	162	1	-1	-7	2	46	52	2	-5	2	2	185	186	4
5	8	1	4	4	3	0	-7	2	154	152	2	-4	2	2	93	96	1
-5	9	1	95	97	2	1	-7	2	139	142	1	-3	2	2	140	142	3
-4	9	1	133	135	3	2	-7	2	116	116	1	-2	2	2	292	283	3
-3	9	1	33	33	2	3	-7	2	82	79	1	-1	2	2	630	638	7
-2	9	1	178	179	2	4	-7	2	140	142	1	0	2	2	169	169	1
-1	9	1	36	34	1	5	-7	2	55	52	1	1	2	2	430	439	3
0	9	1	150	151	1	6	-7	2	11	17	1	2	2	2	403	380	4
1	9	1	80	78	1	-1	-6	2	97	96	2	3	2	2	324	316	4
2	9	1	120	122	1	0	-6	2	232	231	3	4	2	2	44	46	1
3	9	1	85	90	2	1	-6	2	333	327	4	5	2	2	60	57	1
5	9	1	75	77	1	2	-6	2	106	94	1	6	2	2	119	119	1
-3	10	1	58	51	1	4	-6	2	151	151	1	7	2	2	59	55	1
-2	10	1	29	35	1	5	-6	2	81	82	1	-6	3	2	54	55	2
0	10	1	100	121	2	6	-6	2	35	33	2	-5	3	2	47	44	1
1	10	1	119	124	1	-1	-5	2	225	220	3	-4	3	2	126	123	2
2	10	1	55	53	1	0	-5	2	107	113	1	-3	3	2	213	202	4
3	10	1	8	8	7	1	-5	2	363	354	5	-2	3	2	40	40	1
-3	11	1	114	114	3	2	-5	2	68	61	1	-1	3	2	191	186	2
-2	11	1	152	153	2	3	-5	2	101	97	1	0	3	2	115	119	1
-1	11	1	168	164	3	4	-5	2	51	50	1	1	3	2	307	295	2
0	11	1	72	72	1	5	-5	2	99	98	1	2	3	2	317	314	3
1	11	1	82	78	1	6	-5	2	116	115	2	3	3	2	84	78	1
2	11	1	124	130	2	-3	-4	2	210	211	5	4	3	2	26	24	1
3	11	1	44	46	2	-2	-4	2	232	232	5	5	3	2	57	55	1
-3	12	1	47	45	2	-1	-4	2	178	186	2	6	3	2	68	68	1
-2	12	1	164	162	2	0	-4	2	211	208	3	-7	4	2	114	113	3
-1	12	1	131	129	2	1	-4	2	53	52	3	-6	4	2	76	75	2
0	12	1	28	29	1	2	-4	2	314	304	3	-5	4	2	67	66	2
1	12	1	47	46	1	3	-4	2	149	150	1	-4	4	2	81	82	1
2	12	1	90	89	2	4	-4	2	195	194	2	-3	4	2	145	147	2
-2	13	1	105	105	2	5	-4	2	113	117	1	-2	4	2	230	210	5
-1	13	1	66	64	1	6	-4	2	131	127	2	-1	4	2	102	101	1

TABLE 7-continued

Observed and calculated structure factors for NEL																								
h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s	
0	13	1	102	102	1	7	-4	2	28	26	2	0	0	4	2	176	176	1	-1	-14	3	94	93	2
1	13	1	41	43	2	-3	-3	2	197	194	4	1	4	2	2	222	221	2	0	-14	3	34	30	2
-1	-14	2	85	83	2	-1	-3	2	296	307	4	2	4	2	338	315	3	1	-14	3	35	34	2	
0	-14	2	45	45	2	0	-3	2	69	70	1	3	4	2	96	94	1	2	-14	3	60	62	2	
1	-14	2	29	30	3	1	-3	2	73	74	1	4	4	2	79	77	1	-3	-13	3	31	32	2	
-2	-13	2	99	97	2	2	-3	2	188	184	1	5	4	2	91	92	1	-2	-13	3	65	61	2	
0	-13	2	68	64	2	3	-3	2	107	111	1	6	4	2	69	63	1	-1	-13	3	20	18	3	
1	-13	2	41	42	3	4	-3	2	154	154	1	-6	5	2	29	26	2	0	-13	3	19	22	3	
-3	-13	2	73	73	2	5	-3	2	27	23	1	-5	5	2	105	120	3	2	-13	3	44	45	3	
3	-13	2	54	54	1	6	-3	2	35	29	1	-4	5	2	142	147	2	3	-13	3	73	72	1	
-3	-12	2	26	25	2	7	-3	2	58	59	2	-3	5	2	45	47	1	-3	-12	3	106	108	2	
-2	-12	2	97	96	2	-1	-2	2	365	390	9	-2	5	2	240	239	3	-2	-12	3	73	71	2	
-1	-12	2	38	35	2	0	-2	2	596	596	8	-1	5	2	29	26	1	-1	-12	3	50	53	2	
0	-12	2	83	81	2	1	-2	2	430	446	4	0	5	2	92	96	1	0	-12	3	45	47	2	
-2	-12	2	103	105	2	2	-2	2	224	227	2	1	5	2	275	268	2	1	-12	3	63	62	2	
3	-12	2	65	64	1	3	-2	2	112	118	1	2	5	2	100	92	1	2	-12	3	92	93	2	
4	-12	2	53	52	1	4	-2	2	53	50	1	3	5	2	57	56	1	4	-12	3	26	25	2	
-4	-11	2	53	54	2	5	-2	2	106	99	1	4	5	2	90	86	1	4	-12	3	56	52	2	
-3	-11	2	74	75	2	6	-2	2	115	119	2	5	5	2	78	83	1	-3	-11	3	172	179	4	
-2	-11	2	106	104	2	7	-2	2	29	28	2	6	5	2	30	29	1	-2	-11	3	116	113	3	
-1	-11	2	93	109	3	-1	-1	2	223	236	4	-6	6	2	58	57	2	-1	-11	3	73	77	2	
0	-11	2	95	104	3	0	-1	2	377	397	4	-5	6	2	35	47	2	0	-11	3	68	78	2	
1	-11	2	156	163	4	1	-1	2	295	306	2	-4	6	2	139	148	2	1	-11	3	54	55	2	
-2	-11	2	110	112	3	2	-1	2	96	100	1	-3	6	2	100	90	1	2	-11	3	89	82	2	
3	-11	2	95	91	2	3	-1	2	179	168	1	-2	6	2	176	178	2	3	-11	3	73	71	2	
4	-11	2	52	53	1	4	-1	2	149	149	1	-1	6	2	75	74	1	4	-11	3	9	5	9	
-3	-10	2	97	96	2	5	-1	2	44	43	1	0	6	2	129	131	1	-3	-10	3	13	16	6	
-2	-10	2	94	97	2	6	-1	2	64	62	1	0	6	2	18	19	1	-2	-10	3	140	138	3	
-1	-10	2	57	60	2	7	-1	2	38	37	2	2	6	2	133	130	1	-1	-10	3	235	240	5	
0	-10	2	25	28	2	-3	0	2	52	61	1	3	6	2	145	146	1	0	-10	3	27	30	2	
1	-10	2	89	90	1	-2	0	2	191	198	4	4	6	2	56	57	1	1	-10	3	140	142	2	
-2	-10	2	182	182	4	-1	0	2	253	265	3	5	6	2	12	11	3	2	-10	3	216	213	5	
3	-10	2	61	59	1	0	0	2	450	469	4	6	6	2	57	56	1	3	-10	3	65	64	1	
4	-10	2	84	80	2	1	0	2	284	295	3	-6	7	2	35	39	2	4	-10	3	40	38	2	
5	-10	2	57	55	1	2	0	2	195	195	1	-5	7	2	78	75	2	5	-10	3	37	38	1	
-2	-9	2	52	52	1	3	0	2	326	319	3	-4	7	2	48	48	2	-2	-9	3	74	74	1	
-1	-9	2	147	145	2	4	0	2	173	165	1	-3	7	2	110	113	2	-1	-9	3	48	43	1	
0	-9	2	28	31	2	5	0	2	90	83	1	-2	7	2	28	28	1	0	-9	3	251	256	4	
1	-9	2	132	129	3	6	0	2	114	115	1	-1	7	2	89	85	1	1	-9	3	120	114	3	
6	0	3	11	7	2	1	7	3	151	152	1	5	-8	4	81	76	1	6	1	-9	3	24	21	1
7	0	3	23	21	3	2	7	3	100	95	1	6	-8	4	26	29	1	-7	2	4	94	98	2	
-3	1	3	357	349	8	3	7	3	135	135	2	-1	-7	4	176	171	4	-6	2	4	54	52	2	
-2	1	3	258	256	3	4	7	3	44	41	2	0	-7	4	349	334	4	-5	2	4	146	145	3	
-1	1	3	391	401	4	5	7	3	28	21	1	1	-7	4	357	355	4	-4	2	4	28	29	1	
0	1	3	544	566	4	-5	8	3	60	62	2	2	-7	4	84	82	1	-3	2	4	151	152	3	
1	1	3	244	258	2	-4	8	3	180	184	3	3	-7	4	300	302	3	-2	2	4	248	247	3	
2	1	3	230	232	2	-3	8	3	46	50	1	4	-7	4	72	73	1	-1	2	4	31	23	1	
3	1	3	123	123	1	-2	8	3	95	95	1	5	-7	4	87	88	2	0	2	4	290	292	2	
4	1	3	26	20	1	-1	8	3	63	63	1	6	-7	4	105	115	2	1	2	4	165	159	1	

TABLE 7-continued

		Observed and calculated structure factors for NEL															
h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s
5	1	3	94	94	1	0	8	3	19	14	1	-1	-6	4	4	155	152
6	1	3	73	72	1	1	8	3	184	190	2	0	-6	4	4	69	70
7	1	3	23	23	2	2	8	3	74	76	1	1	-6	4	4	130	122
-7	2	3	49	55	2	3	8	3	100	103	1	2	-6	4	4	186	190
-6	2	3	14	20	5	4	8	3	57	54	2	3	-6	4	4	83	85
-5	2	3	62	61	2	-3	9	3	69	66	2	4	-6	4	4	48	46
-4	2	3	197	203	3	-2	9	3	97	101	2	5	-6	4	4	47	50
-3	2	3	153	145	3	-1	9	3	77	77	1	6	-6	4	4	36	35
-2	2	3	443	434	5	0	9	3	44	48	1	-1	-5	4	4	54	55
-1	2	3	101	103	1	1	9	3	94	116	2	0	-5	4	4	96	89
0	2	3	692	721	5	2	9	3	88	84	1	1	-5	4	4	94	87
1	2	3	127	119	1	3	9	3	54	59	1	2	-5	4	4	333	325
2	2	3	331	334	3	-3	10	3	94	96	2	3	-5	4	4	312	314
3	2	3	199	202	1	-2	10	3	123	119	2	4	-5	4	4	345	337
4	2	3	131	131	1	-1	10	3	23	23	1	5	-5	4	4	140	135
5	2	3	89	88	1	0	10	3	43	38	1	6	-5	4	4	84	87
6	2	3	38	38	1	1	10	3	69	65	1	-3	-4	4	4	51	50
-7	3	3	136	125	3	2	10	3	20	19	1	-2	-4	4	4	167	170
-6	3	3	76	81	2	3	10	3	43	38	2	-1	-4	4	4	30	30
-5	3	3	122	123	2	-3	11	3	24	18	3	0	-4	4	4	58	59
-4	3	3	21	22	2	-2	11	3	122	118	2	1	-4	4	4	71	72
-3	3	3	280	276	4	-1	11	3	68	67	1	2	-4	4	4	52	52
-2	3	3	237	237	3	0	11	3	29	26	1	3	-4	4	4	169	166
-1	3	3	99	99	1	1	11	3	59	59	1	4	-4	4	4	58	51
0	3	3	524	535	4	2	11	3	37	33	1	5	-4	4	4	139	136
1	3	3	84	77	1	3	11	3	22	22	3	6	-4	4	4	315	314
2	3	3	179	172	1	-2	12	3	125	121	3	-3	-3	4	4	128	131
3	3	3	178	177	1	-1	12	3	42	37	1	-2	-3	4	4	51	43
4	3	3	102	103	1	0	12	3	39	35	1	-1	-3	4	4	89	92
5	3	3	90	91	1	1	12	3	81	82	1	0	-3	4	4	64	64
6	3	3	87	86	1	-2	-14	4	25	25	2	1	-3	4	4	20	21
-7	4	3	54	53	2	0	-14	4	14	10	4	2	-3	4	4	68	76
-6	4	3	70	70	2	1	-14	4	40	39	2	3	-3	4	4	53	47
-5	4	3	53	58	2	-2	-13	4	48	48	2	4	-3	4	4	36	36
-4	4	3	123	122	2	-1	-13	4	57	55	2	5	-3	4	4	35	36
-3	4	3	75	71	1	0	-13	4	58	56	2	6	-3	4	4	58	57
-2	4	3	358	355	7	2	-13	4	89	89	3	7	-3	4	4	138	138
-1	4	3	207	214	3	3	-13	4	52	55	1	-3	-2	4	4	172	178
0	4	3	123	123	1	-3	-12	4	165	164	4	-2	-2	4	4	106	111
1	4	3	136	145	1	-2	-12	4	102	100	2	-1	-2	4	4	142	142
2	4	3	176	168	1	-1	-12	4	41	44	2	0	-2	4	4	133	132
3	4	3	21	22	1	0	-12	4	57	59	2	1	-2	4	4	45	46
4	4	3	81	82	1	1	-12	4	51	47	2	2	-2	4	4	78	79
5	4	3	53	55	1	2	-12	4	92	90	2	3	-2	4	4	96	97
6	4	3	87	82	1	3	-12	4	18	14	3	4	-2	4	4	67	83
-6	5	3	27	25	3	4	-12	4	156	154	4	5	-2	4	4	42	42
-5	5	3	43	46	2	-3	-11	4	51	50	2	6	-2	4	4	68	74
-4	5	3	69	75	1	-2	-11	4	144	145	3	7	-2	4	4	44	40
-3	5	3	121	119	2	0	-11	4	57	72	2	-2	-1	4	4	209	207

TABLE 7-continued

		Observed and calculated structure factors for NEL															
h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s
-2	5	3	232	236	3	1	-11	4	92	90	2	-1	-1	4	328	346	3
-1	5	3	206	202	3	2	-11	4	25	26	3	0	-1	4	237	248	2
0	5	3	247	244	3	3	-11	4	139	135	2	1	-1	4	258	272	2
1	5	3	114	117	1	4	-11	4	13	10	5	2	6	4	67	72	1
2	5	3	225	233	1	-3	-10	4	90	94	2	3	-1	4	77	77	1
3	5	3	62	60	1	-2	-10	4	119	114	3	4	-1	4	147	144	1
4	5	3	137	136	1	-1	-10	4	43	41	1	6	-1	4	123	122	2
5	5	3	48	41	1	0	-10	4	94	91	2	7	-1	4	69	66	2
6	5	3	13	13	3	1	-10	4	49	47	1	-3	0	4	138	144	3
-6	6	3	58	55	2	2	-10	4	63	63	2	-2	0	4	236	243	3
-5	6	3	65	79	2	3	-10	4	77	76	1	-1	0	4	125	127	1
-4	6	3	36	47	2	4	-10	4	86	87	2	0	0	4	192	195	1
-3	6	3	67	70	1	5	-10	4	21	19	2	1	0	4	96	101	1
-2	6	3	83	82	1	-2	-9	4	171	173	3	2	0	4	80	87	1
-1	6	3	110	115	1	-1	-9	4	187	179	3	3	0	4	63	56	1
0	6	3	169	168	1	0	-9	4	44	44	1	4	0	4	189	194	1
1	6	3	164	164	1	1	-9	4	136	132	2	5	0	4	165	168	1
2	6	3	201	196	1	2	-9	4	87	81	2	6	0	4	65	64	1
3	6	3	165	165	1	3	-9	4	260	261	3	7	0	4	15	18	3
4	6	3	178	174	1	4	-9	4	111	109	2	-3	1	4	143	148	3
5	6	3	69	71	1	5	-9	4	63	64	1	-2	1	4	229	223	2
-6	7	3	59	59	2	-2	-8	4	121	119	3	-1	1	4	132	135	1
-5	7	3	45	47	2	-1	-8	4	310	306	5	0	1	4	401	409	3
-4	7	3	146	145	3	0	-8	4	109	98	2	1	1	4	169	165	1
-3	7	3	77	81	1	1	-8	4	263	257	3	2	1	4	49	47	1
-2	7	3	144	144	1	2	-8	4	178	184	1	3	1	4	185	196	1
-1	7	3	138	139	1	3	-8	4	231	231	2	4	1	4	199	195	1
0	7	3	92	84	1	4	-8	4	122	123	2	5	1	4	135	135	1
3	-6	5	205	204	2	-6	3	5	29	32	2	-1	-13	6	68	70	2
4	-6	5	241	234	2	-5	3	5	71	75	2	0	-13	6	81	85	2
5	-6	5	69	69	1	-4	3	5	63	57	1	1	-13	6	59	67	2
6	-6	5	65	67	1	-3	3	5	137	130	2	2	-13	6	78	78	2
-1	-5	5	48	39	1	-2	3	5	146	147	2	3	-13	6	24	28	3
0	-5	5	609	595	9	-1	3	5	413	400	4	-2	-12	6	99	99	2
1	-5	5	342	331	4	0	3	5	295	288	3	-1	-12	6	36	43	2
2	-5	5	53	48	1	1	3	5	233	226	2	0	-12	6	84	80	2
3	-5	5	86	86	1	2	3	5	117	125	1	1	-12	6	32	31	2
4	-5	5	243	241	2	3	3	5	52	50	1	2	-12	6	42	40	2
5	-5	5	87	92	1	4	3	5	115	118	2	3	-12	6	145	143	3
6	-5	5	65	64	1	5	3	5	2	9	2	4	-12	6	71	71	2
-2	-4	5	146	142	3	-6	4	5	118	119	3	-3	-11	6	119	120	3
-1	-4	5	263	265	4	-5	4	5	118	119	3	-3	-11	6	119	120	3
0	-4	5	366	363	5	-4	4	5	42	41	1	-2	-11	6	17	15	4
1	-4	5	221	217	2	-3	4	5	65	65	1	-1	-11	6	182	186	4
2	-4	5	180	188	2	-2	4	5	158	150	2	0	-11	6	81	91	2
3	-4	5	140	143	1	-1	4	5	283	283	4	1	-11	6	28	24	3
4	-4	5	52	49	1	0	4	5	157	159	1	2	-11	6	80	74	2
5	-4	5	83	79	1	1	4	5	296	305	2	3	-11	6	185	184	3
6	-4	5	66	62	2	2	4	5	205	196	1	4	-11	6	31	31	3

TABLE 7-continued

		Observed and calculated structure factors for NEL															
h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s
-3	-3	5	57	56	2	3	4	5	143	140	1	-2	-10	6	114	116	3
-2	-3	5	220	220	5	4	4	5	124	127	2	-1	-10	6	150	144	2
-1	-3	5	174	176	2	-6	5	5	14	12	5	0	-10	6	39	40	1
0	-3	5	218	210	3	-5	5	5	102	117	3	1	-10	6	86	83	1
1	-3	5	497	511	5	-4	5	5	120	128	3	2	-10	6	137	140	3
2	-3	5	236	232	2	-3	5	5	78	80	1	3	-10	6	148	150	2
3	-3	5	116	116	1	-2	5	5	86	84	1	4	-10	6	85	85	2
4	-3	5	93	89	1	-1	5	5	259	264	2	5	-10	6	90	95	1
5	-3	5	35	36	1	0	5	5	92	98	1	-2	-9	6	90	93	1
6	-3	5	191	189	5	1	5	5	169	164	1	-1	-9	6	221	221	3
-3	-2	5	107	104	3	2	5	5	169	169	1	0	-9	6	53	53	1
-2	-2	5	295	291	4	3	5	5	262	266	2	1	-9	6	159	160	2
-1	-2	5	328	328	4	4	5	5	105	107	2	2	-9	6	18	15	3
0	-2	5	114	106	1	-6	6	5	46	42	2	3	-9	6	140	141	2
1	-2	5	209	209	2	-5	6	5	55	55	2	4	-9	6	63	78	2
2	-2	5	160	157	2	-4	6	5	31	39	2	5	-9	6	71	71	1
3	-2	5	85	88	1	-3	6	5	142	144	2	-1	-8	6	166	163	2
4	-2	5	23	24	1	-2	6	5	31	29	1	0	-8	6	65	62	1
5	-2	5	114	118	2	-1	6	5	113	112	1	1	-8	6	134	131	2
6	-2	5	30	30	1	0	6	5	61	59	1	2	-8	6	95	94	1
7	-2	5	58	60	2	1	6	5	144	137	1	3	-8	6	268	269	3
-3	-1	5	91	88	2	2	6	5	203	195	2	4	-8	6	20	25	2
-2	-1	5	86	86	1	3	6	5	21	16	1	5	-8	6	138	134	2
-1	-1	5	247	254	2	4	6	5	29	24	3	6	-8	6	52	50	2
0	-1	5	191	186	2	-5	7	5	50	46	2	-1	-7	6	173	180	3
1	-1	5	217	228	2	-4	7	5	43	44	2	0	-7	6	169	163	2
2	-1	5	110	105	1	-3	7	5	160	162	4	1	-7	6	331	332	4
3	-1	5	116	113	1	-2	7	5	245	254	3	2	-7	6	47	54	1
4	-1	5	158	165	1	-1	7	5	59	62	1	3	-7	6	110	108	1
5	-1	5	125	129	3	0	7	5	123	128	1	4	-7	6	63	63	1
6	-1	5	108	111	2	1	7	5	190	192	2	5	-7	6	100	99	2
-3	0	5	283	285	6	2	7	5	183	188	2	6	-7	6	48	44	2
-2	0	5	23	23	1	3	7	5	89	92	1	-1	-6	6	274	271	5
-1	0	5	36	41	1	4	7	5	35	33	2	0	-6	6	270	261	4
0	0	5	306	311	2	-4	8	5	64	58	2	1	-6	6	82	84	1
1	0	5	109	116	1	-2	8	5	30	24	2	2	-6	6	148	150	1
2	0	5	308	302	3	-1	8	5	110	113	1	3	-6	6	151	157	1
3	0	5	99	101	1	0	8	5	103	104	1	4	-6	6	157	157	1
4	0	5	43	40	1	1	8	5	194	198	3	5	-6	6	127	125	2
5	0	5	125	123	3	2	8	5	79	78	1	6	-6	6	32	34	1
6	0	5	38	37	1	3	8	5	22	19	2	-1	-5	6	362	344	8
-4	1	5	116	119	3	4	8	5	35	40	2	0	-5	6	124	113	2
-3	1	5	101	103	2	-3	9	5	110	107	3	1	-5	6	387	368	5
-2	1	5	94	94	1	-2	9	5	137	141	3	2	-5	6	111	113	1
-1	1	5	332	325	4	-1	9	5	67	63	1	3	-5	6	176	169	2
0	1	5	315	324	2	0	9	5	103	100	2	4	-5	6	158	159	2
1	1	5	199	206	2	1	9	5	117	114	2	5	-5	6	163	168	2
2	1	5	182	184	1	2	9	5	119	119	1	6	-5	6	22	22	3
3	1	5	264	266	1	3	9	5	32	24	2	-2	-4	6	207	206	5

TABLE 7-continued

		Observed and calculated structure factors for NEL															
h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s
4	1	5	100	101	1	-3	10	5	23	20	3	-1	-4	6	305	297	7
5	1	5	129	127	3	-2	10	5	54	52	2	0	-4	6	296	280	6
6	1	5	43	40	1	-1	10	5	49	47	1	1	-4	6	339	333	5
-7	2	5	51	48	2	0	10	5	51	46	1	2	-4	6	64	57	1
-6	2	5	77	76	2	1	10	5	107	108	1	3	-4	6	88	88	1
-5	2	5	106	109	2	2	10	5	90	89	1	4	-4	6	29	26	2
-4	2	5	139	143	2	-2	11	5	21	19	2	5	-4	6	186	192	3
-3	2	5	210	213	3	-1	11	5	98	94	1	6	-4	6	34	30	2
-2	2	5	89	90	1	0	11	5	71	67	1	-2	-3	6	263	262	4
-1	2	5	213	204	2	1	11	5	73	71	1	-1	-3	6	255	254	4
0	2	5	68	69	1	-2	-14	6	45	42	1	0	-3	6	168	155	3
1	2	5	178	174	2	-1	-14	6	78	74	2	1	-3	6	286	281	3
2	2	5	165	162	1	0	-14	6	47	46	2	2	-3	6	124	112	1
3	2	5	262	268	1	1	-14	6	84	85	2	3	-3	6	8	2	3
4	2	5	256	263	1	2	-14	6	9	12	9	4	-3	6	21	19	2
5	2	5	39	36	2	-2	-13	6	80	78	2	6	-3	6	42	41	1
6	2	5	39	36	2	-2	-13	6	80	78	2	6	-3	6	93	92	2
7	2	5	44	41	1	1	1	7	435	439	6	-1	-14	8	52	51	2
-1	-8	7	139	135	2	3	1	7	61	53	1	0	-14	8	99	95	2
0	-8	7	117	116	1	4	1	7	275	274	2	-3	-13	8	60	62	2
1	-8	7	155	155	2	5	1	7	88	91	1	-2	-13	8	134	131	3
2	-8	7	92	85	1	6	1	7	78	75	2	0	-13	8	146	142	3
3	-8	7	77	79	1	-5	2	7	54	54	1	0	-13	8	50	51	2
4	-8	7	145	147	2	-6	2	7	50	47	2	3	-13	8	56	58	2
5	-8	7	194	188	3	-4	2	7	162	162	4	-3	-12	8	59	60	2
6	-8	7	224	213	3	-3	2	7	95	93	1	-2	-12	8	112	112	3
7	-8	7	43	46	1	-1	2	7	181	177	3	0	-12	8	143	150	4
8	-8	7	59	51	1	0	2	7	111	110	1	1	-12	8	82	73	2
9	-8	7	160	159	2	1	2	7	84	85	1	2	-12	8	61	61	2
10	-8	7	121	118	2	2	2	7	56	50	1	3	-12	8	168	172	4
11	-8	7	128	128	3	3	2	7	48	44	1	-3	-11	8	48	51	2
12	-8	7	143	140	3	4	2	7	149	149	1	4	-11	8	18	20	3
13	-8	7	40	41	1	5	2	7	64	62	2	-3	-11	8	64	62	2
14	-8	7	35	28	1	-6	3	7	122	115	3	-2	-11	8	122	115	3
15	-8	7	204	204	2	-5	3	7	46	47	2	-1	-11	8	46	47	2
16	-8	7	93	89	1	-4	3	7	39	33	2	1	-11	8	24	29	3
17	-8	7	42	44	1	-3	3	7	46	47	2	3	-11	8	39	33	2
18	-8	7	164	162	2	-2	3	7	36	31	2	4	-11	8	46	47	2
19	-8	7	31	31	1	-1	3	7	87	87	2	4	-11	8	36	31	2
20	-8	7	98	103	2	0	3	7	93	87	2	4	-11	8	87	87	2
21	-8	7	189	179	4	1	3	7	155	148	3	5	-10	8	155	148	3
22	-8	7	238	212	5	2	3	7	195	199	3	6	-10	8	195	199	3
23	-8	7	47	48	1	3	3	7	45	42	1	-5	0	8	45	42	1
24	-8	7	89	84	1	4	3	7	105	100	2	-4	0	8	105	100	2
25	-8	7	224	230	2	5	3	7	219	214	5	-3	0	8	219	214	5
26	-8	7	133	137	1	-6	4	7	61	62	2	-2	0	8	61	62	2
27	-8	7	108	112	1	-5	4	7	87	80	2	0	-10	8	87	80	2
28	-8	7	136	135	1	-5	4	7	54	52	2	0	-10	8	54	52	2
29	-8	7	145	149	3	-2	4	7	214	219	3	1	-9	8	214	219	3
30	-8	7	138	135	1	0	8	8	214	219	3	1	-9	8	214	219	3
31	-8	7	138	135	1	0	8	8	214	219	3	1	-9	8	214	219	3
32	-8	7	138	135	1	0	8	8	214	219	3	1	-9	8	214	219	3
33	-8	7	138	135	1	0	8	8	214	219	3	1	-9	8	214	219	3
34	-8	7	138	135	1	0	8	8	214	219	3	1	-9	8	214	219	3
35	-8	7	138	135	1	0	8	8	214	219	3	1	-9	8	214	219	3
36	-8	7	138	135	1	0	8	8	214	219	3	1	-9	8	214	219	3
37	-8	7	138	135	1	0	8	8	214	219	3	1	-9	8	214	219	3
38	-8	7	138	135	1	0	8	8	214	219	3	1	-9	8	214	219	3
39	-8	7	138	135	1	0	8	8	214	219	3	1	-9	8	214	219	3
40	-8	7	138	135	1	0	8	8	214	219	3	1	-9	8	214	219	3
41	-8	7	138	135	1	0	8	8	214	219	3	1	-9	8	214	219	3
42	-8	7	138	135	1	0	8	8	214	219	3	1	-9	8	214	219	3
43	-8	7	138	135	1	0	8	8	214	219	3	1	-9	8	214	219	3
44	-8	7	138	135	1	0	8	8	214	219	3	1	-9	8	214	219	3
45	-8	7	138	135	1	0	8	8	214	219	3	1	-9	8	214	219	3
46	-8	7	138	135	1	0	8	8	214	219	3	1	-9	8	214	219	3
47	-8	7	138	135	1	0	8	8	214	219	3	1	-9	8	214	219	3
48	-8	7	138	135	1	0	8	8	214	219	3	1	-9	8	214	219	3
49	-8	7	138	135	1	0	8	8	214	219	3	1	-9	8	214	219	3
50	-8	7	138	135	1	0	8	8	214	219	3	1	-9	8	214	219	3
51	-8	7	138	135	1	0	8	8	214	219	3	1	-9	8	214	219	3
52	-8	7	138	135	1	0	8	8	214	219	3	1	-9	8	214	219	3
53	-8	7	138	135	1	0	8	8	214	219	3	1	-9	8	214	219	3
54	-8	7	138	135	1	0	8	8	214	219	3	1	-9	8	214	219	3
55	-8	7	138	135	1	0	8	8	214	219	3	1	-9	8	214	219	3
56	-8	7	138	135	1	0	8	8	214	219	3	1	-9	8	214	219	3
57	-8	7	138	135	1	0	8	8	214	219	3	1	-9	8	214	219	3
58	-8	7	138	135	1	0	8	8	214	219	3	1	-9	8	214	219	3
59	-8	7	138	135	1	0	8	8	214	219	3	1	-9	8	214	219	3
60	-8	7	138	135	1	0	8	8	214	219	3	1	-9	8	214	219	3
61	-8	7	138	135	1	0	8	8	214	219	3	1	-9	8	214	219	3
62	-8	7	138	135	1	0	8	8	214	219	3	1	-9	8	214	219	3
63	-8	7	138	135	1	0	8	8	214	219	3	1	-9	8	214	219	3
64	-8	7	138	135	1	0	8	8	214	219	3	1	-9	8	214	219	3
65	-8	7	138	135	1	0	8	8	214	219	3	1	-9	8	214	219	3
66	-8	7	138	135	1	0	8	8	214	219	3	1	-9	8	214	219	3
67	-8	7	138	135	1	0	8	8	214	219	3	1	-9	8	214	219	3
68	-8	7	138	135	1	0	8	8	214	219	3	1	-9	8	214	219	3
69	-8	7	138	135	1	0	8	8	214	219	3	1	-9	8	214	219	3
70	-8	7	138	135	1	0	8	8	214	219	3	1	-9	8	214	219	3
71	-8	7	138	135	1	0	8	8	214	219	3	1	-9	8	214	219	3
72	-8	7	138	135	1	0	8	8	214	219	3	1	-9	8	214	219	3
73	-8	7	138	135	1	0	8	8	214	219	3	1	-9	8	214	219	3
74	-8	7	138	135	1	0	8	8	214	219	3	1	-9	8	214	219	3
75	-8	7	138	135	1	0	8	8	214	219	3	1	-9	8	214	219	3

TABLE 7-continued

		Observed and calculated structure factors for NEL															
h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s
6	-5	7	32	31	2	-4	4	7	22	26	3	-1	-9	8	261	256	4
-2	-4	7	50	49	1	-3	4	7	118	110	2	0	-9	8	135	135	2
-1	-4	7	462	435	10	-2	4	7	54	50	1	1	-9	8	94	96	2
0	-4	7	97	106	2	-1	4	7	204	206	2	2	-9	8	248	252	6
1	-4	7	111	115	1	0	4	7	63	62	1	3	-9	8	83	78	2
2	-4	7	98	94	1	1	4	7	347	344	3	4	-9	8	105	107	2
3	-4	7	59	58	1	2	4	7	89	81	1	5	-9	8	95	94	2
4	-4	7	121	124	1	3	4	7	231	230	3	-2	-8	8	100	96	2
5	-4	7	31	29	1	4	4	7	142	141	2	-1	-8	8	49	45	1
6	-4	7	84	82	2	5	4	7	54	48	2	0	-8	8	130	123	2
-2	-3	7	99	97	1	-6	5	7	85	87	2	1	-8	8	76	79	1
-1	-3	7	145	147	2	-5	5	7	138	137	3	2	-8	8	89	92	2
0	-3	7	198	182	4	-3	5	7	189	187	4	3	-8	8	136	135	2
1	-3	7	87	87	1	-2	5	7	61	59	1	4	-8	8	78	81	2
2	-3	7	92	92	1	-1	5	7	80	85	1	5	-8	8	44	42	1
3	-3	7	118	123	1	0	5	7	86	81	1	-2	-7	8	97	95	2
4	-3	7	46	41	1	1	5	7	103	107	1	-1	-7	8	43	45	1
5	-3	7	106	104	1	2	5	7	77	74	1	0	-7	8	107	104	2
6	-3	7	52	46	2	3	5	7	207	203	2	1	-7	8	70	63	1
-2	-2	7	76	75	1	4	5	7	22	19	2	2	-7	8	41	40	1
-1	-2	7	309	308	4	-5	6	7	50	49	2	3	-7	8	120	113	1
0	-2	7	216	205	3	-4	6	7	81	80	2	4	-7	8	70	70	2
1	-2	7	260	252	3	-3	6	7	72	72	2	5	-7	8	83	83	1
2	-2	7	177	173	2	-2	6	7	237	238	3	6	-7	8	10	10	0
3	-2	7	33	40	1	-1	6	7	141	142	1	-2	-6	8	180	184	4
4	-2	7	77	82	1	0	6	7	167	161	1	-1	-6	8	71	75	1
5	-2	7	124	118	2	1	6	7	34	33	1	0	-6	8	416	414	5
6	-2	7	54	52	2	2	6	7	70	81	1	1	-6	8	91	92	1
-3	-1	7	94	92	2	3	6	7	32	30	1	2	-6	8	120	127	1
-2	-1	7	302	296	5	4	6	7	56	55	2	3	-6	8	101	99	1
-1	-1	7	177	166	2	-4	7	7	24	28	3	4	-6	8	107	109	2
0	-1	7	12	10	1	-3	7	7	113	115	2	5	-6	8	65	65	1
1	-1	7	494	499	7	-2	7	7	84	85	2	6	-6	8	6	9	6
2	-1	7	99	95	1	-1	7	7	101	103	2	-2	-5	8	77	72	2
3	-1	7	27	25	1	0	7	7	81	79	1	-1	-5	8	83	85	2
4	-1	7	149	152	1	1	7	7	26	28	1	0	-5	8	95	96	1
5	-1	7	109	114	2	2	7	7	58	58	1	1	-5	8	168	161	2
6	-1	7	11	14	4	3	7	7	150	153	2	2	-5	8	102	97	1
-3	0	7	105	102	1	4	7	7	64	62	2	3	-5	8	36	34	1
-2	0	7	137	137	2	-2	8	7	67	66	2	4	-5	8	151	149	2
-1	0	7	333	332	4	-1	8	7	115	112	2	5	-5	8	36	39	1
0	0	7	139	135	1	0	8	7	33	36	1	6	-5	8	33	37	2
1	0	7	115	123	2	1	8	7	76	76	1	-2	-4	8	64	62	1
2	0	7	85	87	1	2	8	7	59	60	1	-1	-4	8	173	164	3
3	0	7	124	123	1	3	8	7	111	115	2	0	-4	8	136	144	2
4	0	7	158	162	1	-2	9	7	33	26	2	1	-4	8	55	53	1
5	0	7	59	60	2	-1	9	7	99	96	2	1	-4	8	44	45	1
6	0	7	36	35	1	0	9	7	5	5	5	2	-4	8	138	138	1
-6	1	7	89	91	2	1	9	7	50	50	1	4	-4	8	91	96	1

TABLE 7-continued

		Observed and calculated structure factors for NEL															
h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s
-5	1	7	177	180	4	2	2	9	7	73	70	1	5	-4	8	69	68
-4	1	7	117	119	2	-2	6	-4	8	85	79	2	4	4	8	40	38
-3	1	7	149	156	2	-1	10	7	8	83	74	2	5	4	8	16	14
-2	1	7	284	285	3	0	10	7	103	104	1	-1	-3	8	104	101	3
-1	1	7	241	225	2	1	10	7	22	22	2	0	-3	8	189	164	4
0	1	7	78	83	1	-2	1	-14	8	89	92	2	-3	5	8	114	110
-2	-6	9	56	59	1	0	2	9	227	221	2	-2	3	0	10	155	162
-1	-6	9	71	75	1	1	2	9	70	70	1	-1	-9	10	41	37	2
0	-6	9	99	100	2	2	2	2	9	121	120	1	0	-9	10	60	66
1	-6	9	124	127	1	3	2	9	66	77	1	1	-6	1	10	55	55
2	-6	9	186	190	2	4	2	9	106	107	1	2	-9	10	75	80	1
3	-6	9	78	74	1	5	2	9	24	23	3	3	-9	10	98	91	3
4	-6	9	121	122	2	-6	3	9	81	75	2	4	-9	10	50	48	2
5	-6	9	29	27	1	-5	3	9	46	42	2	5	-9	10	33	35	2
6	-6	9	34	33	2	-4	3	9	126	137	3	-2	-8	10	74	78	1
-2	-5	9	49	42	1	-3	3	9	262	267	3	-1	-8	10	157	156	2
-1	-5	9	249	259	4	-2	3	9	115	114	1	0	-8	10	143	139	2
0	-5	9	89	93	1	-1	3	9	40	37	1	1	-8	10	114	109	2
1	-5	9	163	176	2	0	3	9	34	30	1	2	-8	10	30	31	2
2	-5	9	63	68	1	1	3	9	141	142	1	3	-8	10	89	88	2
3	-5	9	110	112	1	2	3	9	45	45	1	4	-8	10	42	40	1
4	-5	9	118	116	2	3	3	9	101	115	2	5	-8	10	26	24	2
5	-5	9	54	56	1	4	3	9	89	89	1	-2	-7	10	252	251	4
6	-5	9	21	18	3	5	3	9	24	22	3	-1	-7	10	114	118	2
-2	-4	9	61	61	1	-5	4	9	87	84	2	0	-7	10	275	271	4
-1	-4	9	150	142	2	-3	4	9	138	137	3	1	-7	10	158	164	2
0	-4	9	94	92	1	-2	4	9	57	58	1	2	-7	10	237	241	4
1	-4	9	58	64	1	-1	4	9	57	61	1	3	-7	10	117	125	2
2	-4	9	50	57	1	0	4	9	44	46	1	4	-7	10	46	47	2
3	-4	9	188	192	2	1	4	9	88	86	1	5	-7	10	82	82	1
4	-4	9	155	166	2	2	4	9	114	123	1	-2	-6	10	67	66	1
5	-4	9	96	96	1	3	4	9	84	84	1	-1	-6	10	90	85	1
6	-4	9	37	38	2	4	4	9	23	21	3	0	-6	10	139	132	2
-2	-3	9	171	172	2	-5	5	9	103	101	2	1	-6	10	110	103	1
-1	-3	9	21	15	1	-4	5	9	20	19	4	2	-6	10	71	67	1
0	-3	9	127	121	1	-3	5	9	138	130	3	3	-6	10	211	219	2
1	-3	9	241	247	2	-2	5	9	82	80	1	4	-6	10	56	58	2
2	-3	9	107	107	1	-1	5	9	113	116	2	0	-6	10	120	121	2
3	-3	9	67	66	1	0	5	9	11	6	5	-2	-5	10	13	14	3
4	-3	9	81	78	1	1	5	9	114	118	1	-1	-5	10	55	64	1
5	-3	9	100	95	1	2	5	9	106	102	2	0	-5	10	75	72	1
6	-3	9	81	78	2	3	5	9	63	57	1	1	-5	10	90	95	1
-3	-2	9	97	100	1	4	5	9	38	38	2	2	-5	10	110	107	1
-2	-2	9	98	104	1	-5	6	9	18	18	3	3	-5	10	82	87	1
-1	-2	9	193	194	2	-4	6	9	51	52	2	4	-5	10	151	149	4
0	-2	9	92	99	1	-3	6	9	59	59	2	5	-5	10	92	92	1
1	-2	9	106	113	1	-2	6	9	75	71	2	-2	-4	10	97	99	1
2	-2	9	18	14	1	-1	6	9	126	128	2	-1	-4	10	95	99	1
3	-2	9	17	19	2	0	6	9	48	52	1	0	-4	10	125	124	1

TABLE 7-continued

Observed and calculated structure factors for NEL																								
h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s	
4	-2	9	99	117	3	1	1	-4	10	71	66	1	2	4	10	79	79	1	-3	-5	11	33	33	2
5	-2	9	138	134	2	2	2	-4	10	75	77	1	3	4	10	50	47	1	-2	-5	11	159	158	2
6	-2	9	59	60	1	3	3	-4	10	98	103	1	4	4	10	23	18	3	-1	-5	11	125	125	2
-4	-1	9	137	138	3	4	4	-4	10	19	16	2	-5	5	10	22	25	3	0	-5	11	111	110	2
-3	-1	9	134	139	2	-2	7	9	92	91	2	5	-4	4	10	75	72	1	-4	-5	11	86	86	1
-2	-1	9	85	83	1	-1	7	9	106	106	2	-3	-3	5	10	61	61	2	2	-5	11	93	96	1
-1	-1	9	245	244	2	0	7	9	34	30	1	-2	5	5	10	51	52	2	1	-5	11	103	110	1
0	-1	9	26	24	1	1	7	9	73	72	1	-1	-1	5	10	91	95	2	3	-5	11	85	85	2
1	-1	9	113	118	1	2	7	9	91	89	1	0	8	5	10	22	23	2	5	-5	11	22	21	2
2	-1	9	72	68	1	3	7	9	39	38	2	1	1	5	10	148	145	2	-3	-4	11	60	61	1
3	-1	9	44	42	1	-2	8	9	57	51	2	2	2	5	10	76	76	1	-2	-4	11	81	81	1
4	-1	9	25	20	2	-1	8	9	29	29	2	3	-3	5	10	128	122	1	-1	-4	11	15	19	3
5	-1	9	87	89	1	0	8	9	43	42	1	4	-3	5	10	30	29	2	0	-4	11	106	105	1
6	-1	9	48	48	1	1	8	9	27	27	1	5	-3	6	10	67	68	2	1	-4	11	164	167	2
-6	0	9	58	53	2	2	8	9	86	81	1	-4	-2	6	10	68	69	2	2	-4	11	60	60	2
-5	0	9	78	77	2	-1	9	9	66	68	1	-3	-2	6	10	65	62	1	3	-4	11	64	63	1
-4	0	9	103	104	2	0	9	9	32	31	1	-2	-2	6	10	55	52	1	4	-4	11	203	194	3
-3	0	9	235	237	4	1	9	9	63	62	2	-1	-2	6	10	79	77	1	5	-4	11	39	36	1
-2	0	9	163	167	2	-1	-14	10	62	59	2	0	-2	6	10	101	96	1	-4	-3	11	183	184	4
-1	0	9	237	243	2	-3	-13	10	44	49	2	1	-2	7	10	100	98	3	-3	-3	11	94	99	1
0	0	9	79	77	1	-2	-13	10	19	15	3	2	-2	7	10	62	61	1	-2	-3	11	114	114	2
1	0	9	330	332	3	-1	-13	10	69	65	2	3	-2	7	10	69	65	1	0	-3	11	60	62	1
2	0	9	107	110	1	0	-13	10	100	93	2	4	-2	7	10	72	72	1	0	-3	11	462	460	5
3	0	9	7	14	6	-3	-12	10	20	20	3	5	-2	7	10	53	51	1	1	-3	11	128	134	1
4	0	9	23	22	2	-2	-12	10	25	25	3	-5	-1	8	10	29	27	2	2	-3	11	97	98	1
5	0	9	116	122	3	-1	-12	10	44	43	2	-4	-1	8	10	29	28	2	3	-3	11	87	88	2
-6	1	9	18	19	3	0	-12	10	67	64	2	-3	-1	8	10	86	87	1	4	-3	11	143	145	2
-5	1	9	31	27	2	1	-12	10	41	45	2	-2	-1	8	10	62	60	1	5	-3	11	36	36	1
-4	1	9	156	153	4	3	-12	10	33	36	2	-1	-1	14	11	98	98	2	-5	-2	11	92	94	2
-3	1	9	213	213	3	-3	-11	10	33	34	2	0	-1	-13	11	25	18	2	-4	-2	11	118	112	3
-2	1	9	111	106	1	-2	-11	10	103	102	2	1	-1	-13	11	58	55	2	-3	-2	11	115	119	2
-1	1	9	35	32	1	-1	-11	10	26	29	2	2	-1	-13	11	27	25	3	-2	-2	11	19	14	2
0	1	9	94	85	1	0	-11	10	110	128	3	3	-1	-12	11	88	85	2	-1	-2	11	91	89	1
1	1	9	137	129	1	1	-11	10	92	94	2	4	-1	-12	11	21	19	3	0	-2	11	196	194	2
2	1	9	117	121	1	2	-11	10	56	56	2	5	-1	-12	11	68	71	2	1	-2	11	139	136	1
3	1	9	127	130	1	3	-11	10	81	77	2	-6	0	-12	11	58	55	2	2	-2	11	57	57	1
4	1	9	147	150	2	4	-11	10	47	43	2	-5	0	-12	11	62	62	2	3	-2	11	39	41	2
5	1	9	50	47	2	-3	-10	10	14	13	6	-4	0	-12	11	53	54	2	4	-2	11	84	83	1
-6	2	9	111	103	3	-2	-10	10	152	148	3	-3	0	-11	11	34	33	2	5	-2	11	21	24	1
-5	2	9	15	19	5	-1	-10	10	95	104	3	-2	0	-11	11	141	145	3	-6	-1	11	86	82	2
-4	2	9	88	90	2	1	-10	10	135	142	3	-1	0	-11	11	91	99	3	-5	-1	11	126	127	3
-3	2	9	159	157	2	2	-10	10	64	64	2	0	0	-11	11	67	73	2	-4	-1	11	39	36	2
-2	2	9	207	205	2	3	-10	10	59	57	2	1	0	-11	11	50	46	2	-3	-1	11	93	97	1
-1	2	9	58	60	1	4	-10	10	85	82	2	2	0	-11	11	123	124	3	-2	-1	11	174	164	3
0	-1	11	13	11	3	0	-11	12	25	25	3	-4	-1	-9	13	108	109	3	-5	1	13	31	32	2
1	-1	11	117	117	1	1	-11	12	81	84	2	-3	-1	-9	13	63	60	2	-4	1	13	33	34	2
2	-1	11	160	166	1	2	-11	12	0	1	1	-2	-3	-8	13	42	42	2	-3	1	13	106	108	3

TABLE 7-continued

Observed and calculated structure factors for NEL																							
h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s
2	-1	11	58	52	1	3	-11	12	48	56	2	-1	-1	12	260	259	4	-2	-8	13	66	60	2
3	-1	11	72	72	1	-3	-10	12	32	28	2	0	-1	12	53	52	1	-1	-8	13	64	67	2
4	-1	11	42	40	1	-2	-10	12	39	36	2	1	-1	12	144	145	1	0	-8	13	62	63	2
5	-1	11	53	54	2	-1	-10	12	44	50	2	2	-1	12	57	57	1	1	-8	13	102	104	2
-6	0	11	84	86	2	0	-10	12	25	19	3	3	-1	12	178	178	3	2	-8	13	128	131	3
-5	0	11	62	62	2	1	-10	12	8	4	8	4	-1	12	33	27	1	3	-8	13	18	16	5
-4	0	11	35	36	2	2	-10	12	60	63	2	-5	0	12	147	142	3	4	-8	13	88	89	2
-3	0	11	88	89	1	3	-10	12	63	65	2	-4	0	12	22	23	3	-4	-7	13	91	93	2
-2	0	11	66	61	1	4	-10	12	38	36	2	-3	0	12	98	108	3	-3	-7	13	26	24	3
-1	0	11	154	149	2	-3	-9	12	13	15	6	-2	0	12	65	70	1	-2	-7	13	161	166	4
0	0	11	218	221	2	-2	-9	12	66	65	2	-1	0	12	120	119	2	-1	-7	13	74	81	2
1	0	11	134	133	1	-1	-9	12	99	122	3	0	0	12	87	88	1	0	-7	13	171	159	4
2	0	11	136	143	1	0	-9	12	68	75	2	1	0	12	90	85	1	1	-7	13	35	32	1
3	0	11	115	120	2	1	-9	12	54	54	2	2	0	12	46	44	1	2	-7	13	89	93	3
4	0	11	43	41	1	2	-9	12	57	54	2	3	0	12	80	82	1	3	-7	13	100	103	3
5	0	11	61	62	2	3	-9	12	67	69	2	4	0	12	45	41	1	4	-7	13	88	82	2
-6	1	11	52	50	2	4	-9	12	39	32	2	-5	1	12	93	92	2	-4	-6	13	103	105	2
-5	1	11	39	40	2	-3	-8	12	153	153	4	-4	1	12	42	43	2	-3	-6	13	113	111	3
-4	1	11	140	141	3	-2	-8	12	87	89	2	-2	1	12	201	209	3	-2	-6	13	60	64	2
-3	1	11	118	135	2	-1	-8	12	198	208	4	-1	1	12	81	82	1	-1	-6	13	143	148	4
-2	1	11	154	157	2	0	-8	12	106	109	3	0	1	12	234	249	4	0	-6	13	312	317	4
-1	1	11	236	238	2	1	-8	12	218	222	5	1	1	12	37	33	1	1	-6	13	105	102	2
0	1	11	87	85	1	2	-8	12	44	54	3	2	1	12	99	101	1	2	-6	13	105	109	3
1	1	11	167	167	1	3	-8	12	109	105	3	3	1	12	78	78	1	3	-6	13	52	53	2
2	1	11	239	244	3	4	-8	12	54	53	2	4	1	12	27	28	1	4	-6	13	79	78	1
3	1	11	100	95	2	-3	-7	12	115	117	3	-5	2	12	71	72	2	-4	-5	13	124	122	3
4	1	11	24	21	1	-2	-7	12	135	129	3	-4	2	12	79	78	2	-3	-5	13	99	98	2
5	1	11	15	20	4	-1	-7	12	160	158	2	-3	2	12	157	158	4	-2	-5	13	50	49	2
-5	2	11	52	49	2	0	-7	12	127	124	2	-1	2	12	104	109	2	-1	-5	13	193	204	3
-4	2	11	117	121	3	1	-7	12	186	186	2	0	2	12	233	230	4	0	-5	13	427	428	7
-3	2	11	20	28	3	2	-7	12	69	65	2	1	2	12	125	124	1	1	-5	13	226	232	5
-2	2	11	75	72	1	3	-7	12	123	130	3	2	2	12	68	65	1	2	-5	13	101	103	2
-1	2	11	83	88	1	4	-7	12	80	81	1	3	2	12	120	119	1	3	-5	13	100	101	3
0	2	11	76	71	1	-3	-6	12	154	157	3	4	2	12	51	47	2	4	-5	13	112	112	2
1	2	11	98	97	1	-2	-6	12	66	61	1	-5	3	12	45	43	2	-5	-4	13	121	117	3
2	2	11	126	129	2	-1	-6	12	160	164	2	-4	3	12	81	75	2	-4	-4	13	28	22	3
3	2	11	160	161	2	0	-6	12	121	117	2	-3	3	12	76	79	2	-3	-4	13	31	31	2
4	2	11	31	33	1	1	-6	12	147	153	2	-1	3	12	126	121	3	-2	-4	13	82	83	2
-5	3	11	39	38	2	2	-6	12	147	152	2	0	3	12	91	85	1	-1	-4	13	16	14	2
-4	3	11	15	13	5	3	-6	12	67	69	2	1	3	12	73	83	1	0	-4	13	65	69	1
-3	3	11	96	94	2	4	-6	12	75	73	1	2	3	12	54	52	1	1	-4	13	129	131	2
-2	3	11	88	89	2	5	-6	12	56	59	1	3	3	12	25	22	1	2	-4	13	137	138	2
-1	3	11	55	53	1	-3	-5	12	184	183	4	-4	4	12	32	27	2	3	-4	13	93	101	2
0	3	11	37	29	1	-2	-5	12	111	113	2	-3	4	12	63	66	2	4	-4	13	69	62	2
1	3	11	77	73	1	-1	-5	12	145	147	2	-1	4	12	89	92	2	5	-3	13	124	118	3
2	3	11	75	81	1	0	-5	12	122	113	2	0	4	12	47	43	1	-4	-3	13	132	134	3

TABLE 7-continued

		Observed and calculated structure factors for NEL															
h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s
3	3	11	104	102	1	1	1	4	12	81	76	1	-3	-3	105	103	2
4	3	11	18	12	3	2	2	4	12	69	69	1	-2	-3	122	127	3
-5	4	11	21	20	3	3	3	4	12	76	74	1	-1	-3	123	21	2
-4	4	11	23	23	3	4	-5	5	12	86	88	2	0	-3	13	308	309
-3	4	11	11	14	10	5	5	12	27	28	2	1	-3	13	33	35	2
-2	4	11	142	139	3	-4	4	5	12	26	24	2	2	-3	13	54	52
-1	4	11	62	64	2	-3	4	5	12	48	44	1	3	-3	13	117	119
0	4	11	93	91	1	-2	4	6	12	57	58	2	4	-3	13	57	57
1	4	11	65	67	1	-1	4	6	12	34	35	1	-5	-2	13	125	122
2	4	11	82	80	1	0	4	6	12	48	46	1	-4	-2	13	34	27
3	4	11	58	57	1	1	2	6	12	77	77	2	-3	-2	13	117	121
4	4	11	49	50	2	2	4	7	12	23	24	3	-2	-2	13	52	56
-3	5	11	56	55	2	3	-4	12	101	107	2	0	7	-2	13	161	158
-1	5	11	83	77	2	4	-4	12	30	27	3	-2	-13	-2	13	143	139
0	5	11	26	25	2	5	-4	12	97	98	1	-1	-13	-2	13	59	58
1	5	11	86	83	1	-5	3	12	115	117	3	0	9	1	13	175	185
2	5	11	51	47	1	-4	3	12	200	204	5	-3	-12	3	13	141	141
3	5	11	113	114	1	-3	3	12	27	29	3	-2	-12	3	13	56	52
-2	6	11	66	67	2	-2	3	12	86	84	1	-1	-12	3	13	134	129
-1	6	11	39	38	2	-1	3	12	190	194	3	0	-4	-1	13	44	44
0	6	11	92	87	2	0	-3	12	124	127	1	-3	-11	3	13	73	73
1	6	11	59	55	1	1	-3	12	90	95	1	-2	-11	3	13	20	24
2	6	11	100	97	1	2	-3	12	98	102	1	-1	-11	3	13	149	155
-2	7	11	78	80	2	3	-3	12	46	51	1	0	-11	3	13	49	46
-1	7	11	36	37	2	4	-3	12	37	31	2	3	-11	3	13	74	78
0	7	11	61	61	1	5	-3	12	81	96	1	-3	-10	3	13	98	97
1	7	11	53	50	1	-5	-2	12	179	178	4	-2	-10	3	13	153	156
-1	8	11	65	67	2	-4	-2	12	64	62	2	-1	-10	3	13	48	46
-2	-13	12	39	38	2	-3	-2	12	29	26	2	0	-10	3	13	89	90
-1	-13	12	33	31	2	-2	-2	12	33	29	1	1	-10	3	13	10	10
0	-13	12	59	52	2	-1	-2	12	81	83	1	2	-10	3	13	60	75
-3	-12	12	27	24	2	0	-2	12	47	46	1	3	-10	3	13	14	20
-2	-12	12	67	66	2	1	-2	12	104	105	1	-3	-9	3	13	159	153
-1	-12	12	17	15	4	2	-2	12	139	140	1	-2	-9	3	13	37	39
0	-12	12	62	61	2	3	-2	12	37	41	1	-1	-9	3	13	28	30
-3	-11	12	72	67	2	4	-2	12	42	40	1	0	-9	3	13	116	121
-2	-11	12	60	63	2	5	-2	12	95	91	2	2	-9	3	13	75	72
-1	-11	12	40	46	2	-5	-1	12	88	88	2	4	-9	3	13	21	18
-5	-4	14	49	49	2	3	1	14	8	8	8	3	0	3	15	113	106
-4	-4	14	64	65	2	-4	2	14	92	85	2	-4	-5	15	65	58	2
-2	-4	14	110	123	3	-3	2	14	44	41	2	-3	-5	15	125	120	3
-1	-4	14	126	138	3	-2	2	14	30	35	2	-1	-5	15	107	107	3
0	-4	14	331	325	8	-1	2	14	42	41	3	1	-5	15	179	181	4
1	-4	14	186	190	4	0	2	14	38	43	3	2	-5	15	23	25	4
2	-4	14	69	63	2	1	2	14	35	35	2	3	-5	15	39	39	2

TABLE 7-continued

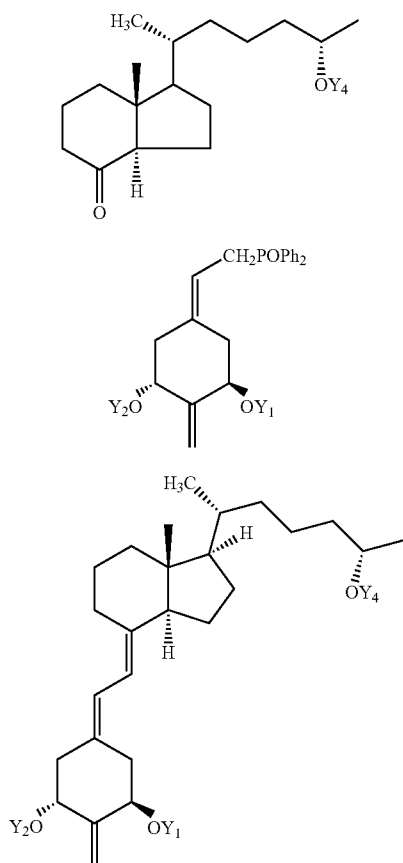
Observed and calculated structure factors for NEL																							
h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s	h	k	l	10Fo	10Fc	10s
3	-4	14	41	40	2	2	2	14	38	37	1	-4	-4	15	46	43	2	-3	-9	16	55	58	2
4	-4	14	80	77	1	-1	3	14	34	29	3	-3	-4	15	71	73	2	-2	-9	16	69	65	2
-5	-3	14	10	15	10	0	3	14	22	18	3	-1	-4	15	87	87	2	-1	-9	16	42	37	2
-4	-3	14	58	56	2	1	3	14	64	61	1	0	-4	15	46	44	2	0	-9	16	36	31	2
-3	-3	14	196	197	4	2	3	14	61	54	1	2	-4	15	41	42	2	-3	-8	16	53	44	2
-1	-3	14	121	125	3	-1	4	14	80	82	2	3	-4	15	57	54	2	-2	-8	16	62	61	2
0	-3	14	238	244	5	0	4	14	41	38	1	-4	-3	15	54	53	2	-1	-8	16	20	22	3
1	-3	14	228	227	5	1	4	14	16	12	3	-3	-3	15	9	13	8	0	-8	16	61	57	2
2	-3	14	145	149	6	0	5	14	39	49	2	-2	-3	15	106	121	3	2	-8	16	67	64	2
3	-3	14	19	18	3	-1	-12	15	74	67	2	-1	-3	15	199	198	5	-4	-7	16	59	59	2
4	-3	14	69	67	2	-2	-11	15	30	27	2	1	-3	15	62	58	2	-3	-7	16	38	35	2
-5	-2	14	22	21	3	-1	-11	15	95	87	2	2	-3	15	83	75	2	-2	-7	16	93	86	2
-4	-2	14	20	16	3	0	-11	15	41	37	2	3	-3	15	84	81	2	-1	-7	16	107	106	2
-3	-2	14	69	76	2	-3	-10	15	105	100	2	-4	-2	15	59	55	2	0	-7	16	30	33	2
-1	-2	14	91	88	2	-2	-10	15	61	62	2	-3	-2	15	39	39	2	2	-7	16	23	25	3
0	-2	14	226	229	4	-1	-10	15	49	46	2	-2	-2	15	72	75	2	3	-7	16	74	76	2
1	-2	14	95	93	2	0	-10	15	57	56	2	-1	-2	15	87	83	2	-4	-6	16	58	62	2
2	-2	14	103	108	1	2	-10	15	60	60	2	0	-2	15	51	47	2	-3	-6	16	34	34	2
3	-2	14	46	44	1	-3	-9	15	54	52	2	1	-2	15	76	74	2	-2	-6	16	18	14	3
4	-2	14	43	46	1	-2	-9	15	112	107	3	3	-2	15	56	54	2	-1	-6	16	92	90	2
-5	-1	14	25	24	2	-1	-9	15	55	56	2	-4	-1	15	29	28	2	0	-6	16	120	118	3
-4	-1	14	11	19	10	0	-9	15	65	60	2	-3	-1	15	73	75	2	1	-6	16	42	42	3
-3	-1	14	109	116	3	2	-9	15	34	37	3	-2	-1	15	96	96	2	2	-6	16	89	87	2
-2	-1	14	95	101	2	3	-9	15	43	43	2	-1	-1	15	71	69	2	3	-6	16	42	41	2
-1	-1	14	7	7	6	-4	-8	15	107	102	2	0	-1	15	40	38	3	-4	-5	16	52	53	2
0	-1	14	50	51	3	-3	-8	15	91	86	2	1	-1	15	92	98	2	-3	-5	16	87	88	2
1	-1	14	69	72	1	-2	-8	15	82	78	2	2	-1	15	64	64	1	-2	-5	16	57	56	2
2	-1	14	57	60	1	-1	-8	15	33	27	2	3	-1	15	34	33	2	-1	-5	16	46	46	2
3	-1	14	26	24	2	0	-8	15	122	122	3	-4	0	15	0	9	1	1	-5	16	96	96	3
4	-1	14	20	27	2	2	-8	15	42	44	2	-2	0	15	32	28	2	2	-5	16	26	20	3
-5	0	14	74	67	2	3	-8	15	89	85	2	-2	0	15	127	131	3	3	-5	16	40	35	2
-4	0	14	68	66	2	-4	-7	15	40	40	2	0	0	15	26	26	3	-4	-4	16	23	26	3
-3	0	14	111	111	3	-3	-7	15	67	69	2	1	0	15	10	7	9	-3	-4	16	56	56	2
-2	0	14	98	101	2	-2	-7	15	58	58	2	2	0	15	55	56	1	-2	-4	16	21	22	3
-1	0	14	46	46	2	-1	-7	15	50	52	2	3	0	15	34	40	2	-1	-4	16	98	96	2
0	0	14	87	86	2	0	-7	15	55	54	2	-4	1	15	23	27	3	1	-4	16	46	43	2
1	0	14	64	63	1	2	-7	15	128	127	3	-2	1	15	7	11	6	2	-4	16	37	31	2
2	0	14	125	128	2	3	-7	15	35	31	2	0	1	15	37	36	3	3	-4	16	0	10	1
3	0	14	11	10	6	-4	-6	15	110	107	2	1	1	15	72	65	1	-4	-3	16	72	71	2
-4	1	14	57	52	2	-3	-6	15	86	84	2	2	1	15	45	47	1	-3	-3	16	15	14	5
-3	1	14	43	42	2	-2	-6	15	38	42	2	-1	2	15	50	51	2	-2	-3	16	35	32	2
-2	1	14	114	117	3	-1	-6	15	27	24	2	0	2	15	110	103	3	-1	-3	16	51	51	2
0	1	14	55	53	2	0	-6	15	158	158	4	1	2	15	58	60	1	2	-3	16	59	60	2
1	1	14	69	69	1	1	-6	15	66	68	2	2	2	15	21	21	2	3	-3	16	26	29	3
2	1	14	85	82	1	2	-6	15	46	52	2	-1	3	15	48	48	2	-4	-2	16	28	28	2

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EXAMPLE 3

Synthesis of NEL

The preparation of NEL having the basic structure I can be accomplished by a common general method, i.e. the condensation of a bicyclic Windaus-Grundmann type ketone II with the allylic phosphine oxide III to the corresponding 2-methylene-19-nor-vitamin D analog IV followed by deprotection at C-1, C-3 and C-25 in the latter compound IV to obtain compound I, i.e. NEL.



In ketone II, Y_4 is preferably a hydroxy-protecting group such as a silyl protecting group. The t-butyldimethyl-silyl (TBDMS) group is an example of a particularly useful hydroxy-protecting group. In phosphine oxide III, Y_1 and Y_2 are preferably hydroxy-protecting groups such as silyl protecting groups. The t-butyldimethylsilyl (TMDMS) group is an example of a particularly useful hydroxy-protecting group. The process described above represents an application of the convergent synthesis concept, which has been applied effectively to the preparation of numerous vitamin D compounds (see Lythgoe et al., *J. Chem. Soc. Perkin Trans. I*, 590 (1978); Lythgoe, *Chem. Soc. Rev.* 9, 449 (1983); Toh et al., *J. Org. Chem.* 48, 1414 (1983); Baggolini et al., *J. Org. Chem.* 51, 3098 (1986); Sardina et al., *J. Org. Chem.* 51, 1264 (1986); *J. Org. Chem.* 51, 1269 (1986); DeLuca et al., U.S. Pat. No. 5,086,191; DeLuca et al., U.S. Pat. No. 5,536,713; and DeLuca et al., U.S. Pat. No. 5,843,928 all of which are hereby incorporated by reference in their entirety and for all purposes as if fully set forth herein.

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Phosphine oxide III is a convenient reagent that can be used to prepare a large number of 19-nor-vitamin D compounds and is prepared according to the procedures described by Sicinski et al., *J. Med. Chem.*, 41, 4662 (1998), DeLuca et al., U.S. Pat. No. 5,843,928; Perlman et al., *Tetrahedron Lett.* 32, 7663 (1991); and DeLuca et al., U.S. Pat. No. 5,086,191 which, are hereby incorporated by reference in their entirety as if fully set forth herein.

The overall process of the synthesis of compound I is illustrated and described more completely in U.S. Pat. No. 5,843,928 entitled "2-Alkylidene-19-Nor-Vitamin D Compounds" and in U.S. Pat. No. 7,528,122 entitled "Vitamin D Analog—NEL, Methods and Uses Thereof," the specifications of which are specifically incorporated herein by reference.

We claim:

1. (20R,25S)-2-methylene-19,26-dinor-1 α ,25-dihydroxyvitamin D_3 in crystalline form.

2. The crystalline form of (20R,25S)-2-methylene-19,26-dinor-1 α ,25-dihydroxyvitamin D_3 having molecular packing arrangement defined by space group P1 and unit cell dimensions $a=6.4$ Å, $b=12.6$ Å, $c=16.0$ Å, $\alpha=110.9^\circ$, $\beta=95.3^\circ$ and $\gamma=90.6^\circ$.

3. A three dimensional structure for (20R,25S)-2-methylene-19,26-dinor-1 α ,25-dihydroxyvitamin D_3 as defined by the molecular packing arrangement set forth in claim 2.

4. A method of purifying (20R,25S)-2-methylene-19,26-dinor-1 α ,25-dihydroxyvitamin D_3 , comprising the steps of:
(a) preparing a solvent comprising water and methanol;
(b) dissolving a product containing (20R,25S)-2-methylene-19,26-dinor-1 α ,25-dihydroxyvitamin D_3 to be purified in said solvent;

(c) cooling said solvent and dissolved product below ambient temperature for a sufficient amount of time to form a precipitate of (20R,25S)-2-methylene-19,26-dinor-1 α ,25-dihydroxyvitamin D_3 crystals; and

(d) separating the (20R,25S)-2-methylene-19,26-dinor-1 α ,25-dihydroxyvitamin D_3 crystals from the solvent.

5. The method of claim 4 including the further step of maintaining said solvent and dissolved product at ambient temperature for a period of time prior to cooling below ambient temperature.

6. The method of claim 4 wherein said solvent comprises 20% water and 80% methanol, by volume.

7. The method of claim 4 wherein said solvent and dissolved product are cooled to about -20° C.

8. The method of claim 4 wherein the step of separating comprises filtering the solvent and precipitate to obtain the crystals.

9. The method of claim 4 including a further step (e) comprising repeating steps (a) through (d) using the recovered crystals from step (d) as the product of step (b).

10. The method of claim 7 wherein said solvent and dissolved product are maintained at -20° C. for up to 7 weeks.

11. A method of purifying (20R,25S)-2-methylene-19,26-dinor-1 α ,25-dihydroxyvitamin D_3 , comprising the steps of
(a) preparing a solvent comprising 80% methanol and 20% water, by volume;

(b) dissolving a product containing (20R,25S)-2-methylene-19,26-dinor-1 α ,25-dihydroxyvitamin D_3 to be purified in said solvent;

(c) cooling said solvent and dissolved product below ambient temperature for a sufficient amount of time to form a precipitate of (20R,25S)-2-methylene-19,26-dinor-1 α ,25-dihydroxyvitamin D_3 crystals; and

(d) recovering the (20R,25S)-2-methylene-19,26-dinor-1 α ,25-dihydroxyvitamin D_3 crystals having a molecular

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packing arrangement defined by space group P1 and unit cell dimensions $a=6.4 \text{ \AA}$, $b=12.6 \text{ \AA}$, $c=16.0 \text{ \AA}$, $\alpha=110.9^\circ$, $\beta=95.3^\circ$ and $\gamma=90.6^\circ$, or any other space group that yields substantially the same crystalline packing arrangement.

12. The method of claim 11 wherein said solvent and dissolved product is maintained at ambient temperature for a period of time prior to cooling below ambient temperature.

13. The method of claim 11 wherein said solvent and dissolved product are cooled to about -20°C .

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14. The method of claim 13 wherein said solvent and dissolved product are maintained at about -20°C . for up to 7 weeks.

15. The method of claim 11 wherein the step of recovering comprises filtering.

16. The method of claim 11 further including the step of (e) repeating steps (a) through (d) using the recovered crystals from step (d) as the product of step (b).

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