

US011395914B2

(12) United States Patent

Ludwig et al.

(54) PENETRATION OF CEREBRAL SPINAL FLUID INTO THE BRAIN PARENCHYMA USING TEMPORALLY PATTERNED NEUROMODULATION

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- (*) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 0 days.
- (21) Appl. No.: 16/935,386
- (22) Filed: Jul. 22, 2020

(65) **Prior Publication Data**

US 2021/0038884 A1 Feb. 11, 2021

Related U.S. Application Data

- (60) Provisional application No. 62/884,002, filed on Aug. 7, 2019.
- (51) Int. Cl.

A61N 1/05	(2006.01)
A61N 1/04	(2006.01)
A61N 1/36	(2006.01)

(10) Patent No.: US 11,395,914 B2

(45) **Date of Patent:** Jul. 26, 2022

(58) Field of Classification Search
 CPC A61N 1/0548; A61N 1/0432; A61N 1/36025; A61N 1/0526; A61N 2005/0606
 See application file for complete search history.

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(57) **ABSTRACT**

Electrical stimulation of specific facial and lingual nerves creates a more sustained pulsatility activity compared to stimulation of other cranial nerves. Pulsatility of arteries has intrinsic time constraints related to the time for vasodilation/ constriction and time to return to baseline (T_{BL}) after electrical stimulation which may affect the pulsatility response. Control of temporal patterning and the stimulation waveform maximizes the physiological response to cerebral pulsatility and its resulting effects on cerebral spinal fluid penetration into the brain parenchyma for a multitude of therapeutic uses including clearing misfolded proteins and/ or administered pharmacological agents, diluting endogenous neurochemical concentrations within the brain, and reducing non-synaptic coupling.

22 Claims, 4 Drawing Sheets



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FIG. 5





FIG. 7





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PENETRATION OF CEREBRAL SPINAL FLUID INTO THE BRAIN PARENCHYMA **USING TEMPORALLY PATTERNED NEUROMODULATION**

CROSS-REFERENCE TO RELATED APPLICATIONS

This application claims the benefit of U.S. Provisional Application No. 62/884,002, filed Aug. 7, 2019, hereby incorporated by reference.

STATEMENT REGARDING FEDERALLY SPONSORED RESEARCH OR DEVELOPMENT

This invention was made with government support under 15 N66001-17-2-4010 awarded by the DOD/DARPA. The government has certain rights in the invention.

BACKGROUND OF THE INVENTION

The present invention relates to electrical stimulation of target nerves to enhance waste clearance in the brain.

The central nervous system (CNS) lymphatic system is made up of multiple components and pathways including the glymphatic system. The glymphatic system (or glymphatic 25 clearance pathway) is a macroscopic waste clearance system for the vertebrate CNS utilizing a unique system of perivascular tunnels formed by glial cells to promote efficient elimination of soluble and insoluble proteins and metabolites from the CNS. The pathway provides a para-arterial 30 influx route for cerebral spinal fluid (CSF) to travel in the perivascular space surrounding descending vasculature and enter the brain parenchyma through AQP4 channels, and a clearance mechanism via convective movement of interstitial fluid (ISF) for extracellular solutes such as misfolded 35 proteins and unwanted metabolites to be removed from the brain.

The aggregation of pathogenic proteins β -amyloid, α -synuclein, and C-tau in the brain may cause the deleterious effects of numerous diseases and disorders such as traumatic 40 brain injury/chronic traumatic encephalopathy, epilepsy, Alzheimer's disease, and Parkinson's disease. Removal of these pathogenic proteins has been found to have substantial therapeutic benefit, for example, in treating traumatic brain injury/chronic traumatic encephalopathy, epilepsy, Alzheim- 45 er's disease, and Parkinson's disease.

Increasing the penetration of CSF into the brain parenchyma can serve many therapeutic purposes, including diluting endogenous neurochemical transmitter concentrations within the brain, altering the clearance rates of drugs deliv- 50 ered orally that penetrate through the blood-brain barrier or delivered via a catheter system to the brain, and reducing non-synaptic coupling between neurons to treat diverse conditions leading to increased neural activity including anxiety disorders, tremor, and seizure.

Transport of CSF along the periarterial spaces into the brain parenchyma and into the cervical and thoracic lymph nodes is driven by cerebral arterial pulsation to the brain. It has previously been found that ligation of the carotid artery or administration of a central sympatholytic such as dobu- 60 tamine can alter the pulsatility of the cerebral vasculature to drive CSF movement in the associated perivascular space.

SUMMARY OF THE INVENTION

The present inventors have found that electrical stimulation of easily accessible neural inputs located outside of the 2

brain and amenable to minimally invasive or non-invasive stimulation strategies can induce cardiovascular and respiratory changes, dilate arterial vessels and increase the pulsatility (change in the vessel diameters over time relative to a mean vessel diameter) of penetrating arterial vessels in the brain thus leading to increased clearance of misfolded proteins from the brain. Specifically, electrical stimulation of cranial nerves or local areas around the cranial nerves may selectively cause oscillations in pressure and dilation of arteries that help to improve waste clearance in the brain. However, these methods are limited by the body's compensation responses that quickly habituate these effects over time and do not maintain a sustained response when nerves are continuously and repeatedly electrically stimulated. In this respect, continuous stimulation of the cranial nerves only causes brief transient changes in blood flow.

The present inventors recognize that pulsatility of arteries has intrinsic time constraints related to the time for vasodi-20 lation/constriction and time to return to baseline (T_{BL}) after electrical stimulation, which may affect the pulsatility response. In this respect, these time constraints for stimulation induced vasodilation/constriction and subsequent return to baseline define the maximum and minimum changes to pulsatility. The present invention provides control of temporal patterning and the stimulation waveform in order to maximize the physiological response to cerebral pulsatility and its resulting effects on brain waste clearance. Thus, the electrical stimulation is temporally patterned to generate multiple vasodilation/constriction pulses in succession to optimize and sustain the pulsating action to continuously drive CSF into the brain parenchyma over long periods of time.

Electrical stimulation of specific cranial nerves such as the branches of the trigeminal nerve, i.e., buccal and lingual branch nerves, and the facial nerve creates a more sustained pulsatility activity compared to stimulation of other cranial nerves. One possible explanation for this is that the facial and trigeminal nerves have direct sympathetic/parasympathetic innervation of the cerebral vasculature through several routes, including through the sphenopalatine ganglion (SPG), which are part of neural pathways that directly control the vasodilation/constriction of the cerebral arteries. As a result, the time course for dilation and constriction after a stimulation burst can be quicker than other cranial nerves because the response is quicker than inputs from the spinal cord which change peripheral sympathetic tone or peripheral inputs such as the sciatic nerve that change blood flow primarily through sensory activity mediated neurovascular coupling.

Also, stimulation through pathways that change sympathetic/parasympathetic tone outside the brain dilate the peripheral vasculature outside of the brain. The change in blood flow in the brain is primarily in response to this change in peripheral blood flow to maintain perfusion (there are also occasionally indirect connections between the vagus and facial nerve in some subjects). As vagus nerve stimulation only indirectly influences blood flow in cerebral vasculature, it has a slower time constant between burst of stimulation for changes in flow to return to normal.

Therefore, the present invention provides 1) a unique intraoral device to conveniently and non-invasively activate the facial/trigeminal nerves and 2) unique temporal stimulation patterns to increase CSF flow via the trigeminal/facial nerves, nerve inputs associated with the baroreflex (vagus, aortic depressor, carotid sinus, baroreceptor beds in the bulb,

aorta), and peripheral nerve inputs not clearly associated with the baroreflex (median nerve, sciatic nerve, tibial nerve, spinal cord).

1) A Unique Intraoral Device to Conveniently and Non-Invasively Activate the Facial/Trigeminal Nerves

Specifically, the present invention provides an electrical stimulation device for improving waste clearance through the perivascular system of the blood brain barrier including at least one electrode configured to stimulate a facial nerve; an electrical generator generating a carrier wave having a carrier frequency stimulating the perivascular system into increased CSF/ISF flow; a modulator receiving the carrier wave and a modulation wave to modulate the carrier wave for application to at least one electrode; and an electrical modulation generator generating the modulation wave having a predetermined periodicity providing a first period of stimulation of the perivascular system and a second period of relaxation of the perivascular system, the predetermined periodicity selected to increase pulsatility over continuous 20 stimulation of the perivascular system by the carrier frequency.

It is thus a feature of at least one embodiment of the present invention to utilize increased cerebral blood flow through arterial vessels to improve the penetration of cere- 25 brospinal fluid into the brain parenchyma.

The electrode may include a cathode positioned distally with respect to a lingual or facial nerve ending and an anode positioned proximally with respect to the lingual or facial nerve ending. The cathode and the anode may be spaced 30 apart along an axis substantially parallel to the nerve. The cathode and anode may be reversed depending on local anatomy.

It is thus a feature of at least one embodiment of the present invention to generate a circuit of electrical impulses 35 along the nerve fibers.

At least one electrode may be adapted to stimulate at least one of a trigeminal nerve, buccal branch nerve, mental branch nerve and facial nerve.

It is thus a feature of at least one embodiment of the 40 present invention to create stimulus locked changes in cerebral blood flow as compared to stimulation of nerves where habituation occurs.

The at least one electrode may be supported by a mouthpiece engaging a jaw of a user's mouth.

It is thus a feature of at least one embodiment of the present invention to utilize the anatomical consistency of the nerves in the jaw region with respect to the jawbone to easily approximate nerve stimulation locations, for example, through the mental foramen.

The mouthpiece may be comprised of a curved tube having an inner and outer wall flanking a channel receiving an upper or lower dental arch of a user and covering an outer labia gingiva of the teeth. At least one electrode may be supported by an inner surface of the outer wall to contact the 55 labia gingiva.

It is thus a feature of at least one embodiment of the present invention to utilize the hydrated epithelial tissue below the gingiva mucosa to provide a conductive path for more efficient electrical stimulation of nerves.

A cathode electrode may be positioned toward a front of the curved mouthpiece receiving the anterior teeth and an anode electrode is positioned toward a rear of the mouthpiece receiving the premolar teeth. The cathode electrode may be positioned to overlay nerve endings of the mental 65 branch nerve with less than 1 cm distance between the cathode electrode and the nerve endings.

It is thus a feature of at least one embodiment of the present invention to provide precise electrical access to the nerve endings where the nerves are positioned close to the outer epidermis of the epithelial tissue.

The mouthpiece may support a first anode-cathode electrode pair on a left side of the mouthpiece and a second anode-cathode electrode pair on a right side of the mouthpiece.

It is thus a feature of at least one embodiment of the present invention to carry multiple electrode pairs for simultaneous multi-nerve stimulation.

The at least one electrode may be supported by a dental filling inserted within a cavity of the tooth. The at least one electrode may be supported by a dental implant inserted within a jawbone.

It is thus a feature of at least one embodiment of the present invention to utilize precise electrical access to the nerve endings of the molar teeth in close proximity to the roots of the molar teeth.

Sensors detecting salivary biomarkers may indicate a change to CSF flow selected from at least one of the following: amyloid beta peptide, tau protein, lactoferrin, alpha-synuclein, DJ-1 protein, chromogranin A, huntingtin protein, DNA methylation disruptions, and micro-RNA.

It is thus a feature of at least one embodiment of the present invention to provide quick visual indication of improved waste clearance through known biomarkers in the patient's saliva.

Electrodes may be used to record electrophysiological signals to detect changes in low frequency power brain waves that propagate outside the calvarium. Electrodes may also be used to pick up heart rate and heart rate variability.

It is thus a feature of at least one embodiment of the present invention to provide quick visual indication of engagement of the stimulating electrodes with the nerves.

2) Unique Temporal Stimulation Patterns to Increase CSF Flow via the Trigeminal/Facial Nerves, Nerve Inputs Associated with the Baroreflex (Vagus, Aortic Depressor, Carotid Sinus, Baroreceptor Beds in the Bulb, Aorta), and Peripheral Nerve Inputs not Clearly Associated with the Baroreflex (Median Nerve, Sciatic Nerve, Tibial Nerve, Spinal Cord)

An alternative embodiment of the present invention may provide a method of improving waste clearance through the perivascular system of the blood brain barrier including positioning at least one electrode in close proximity to a nerve; generating a carrier wave having a carrier frequency stimulating the perivascular system into increased CSF/ISF flow; generating the modulation wave having a predetermined periodicity providing a first period of stimulation of the perivascular system and a second period of relaxation of the perivascular system, the predetermined periodicity selected to increase pulsatility over continuous stimulation of the perivascular system by the carrier frequency; and modulating the carrier wave and applying the carrier wave to the electrode.

For stimulation of the facial nerves, trigeminal nerves, and sphenopalatine ganglia the carrier frequency of the carrier wave may be between 25 Hz and 55 Hz and centered around 50 Hz. The modulation wave may have a frequency 60 between 0.5 Hz and 0.1 Hz. The modulation wave may have a time duration ("bursts") of between 1 second and 10 seconds with a pulse interval (unstimulated period between "bursts") between 1 second and 10 seconds.

For stimulation of the vagus nerve, carotid sinus nerve, and baroreceptors the carrier frequency of the carrier wave may be between 20 Hz and 50 Hz and centered around 30 Hz. The modulation wave may have a frequency between

 $\frac{1}{45}$ Hz and $\frac{1}{180}$ Hz. The modulation wave may have a time duration ("bursts") of between 15 second and 60 seconds and around 30 seconds with a pulse interval (unstimulated period between "bursts") between 30 seconds and 120 seconds and around 60 seconds.

For stimulation of the sciatic nerve and peripheral nerve the carrier frequency of the carrier wave may be between 20 Hz and 55 Hz and centered around 50 Hz. The modulation wave may have a frequency between ½300 Hz and ½40 Hz. The modulation wave may have a time duration ("bursts") of ¹⁰ between 1 minute and 4 minutes and around 3 minutes with a pulse interval (unstimulated period between "bursts") between 4 minutes and 6 minutes and around 5 minutes.

It is thus a feature of at least one embodiment of the ¹⁵ present invention to introduce periods of relaxation into the electrical stimulation parameters to improve recovery processes of the dilated blood vessels.

At least one electrode may be positioned over the mental branch nerve. At least one electrode may be positioned over 20 the inferior alveolar nerve.

These particular objects and advantages may apply to only some embodiments falling within the claims and thus do not define the scope of the invention.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. **1** is a schematic diagram of a human skull receiving electrical stimulation from electrodes positioned on facial and lingual nerves of the head in the tooth and jaw region in 30 accordance with the present invention;

FIG. **2** is a block diagram showing an electrical stimulator modulating a carrier wave to produce a modified electrical signal providing increased CSF flow through arterial vessels to the head and therefore increasing waste clearance;

FIG. **3** is a graph showing a magnitude of vasodilation/ constriction of arterial vessels relative to a mean vessel diameter as a function of a time to return to baseline (T_{BL}) at a given electrical stimulation frequency and duty cycle;

FIG. **4** is a top plan view of a mouthpiece placed in a 40 user's mouth and over the lower jaw to deliver directed electrical stimulation to mental branch nerves within the oral mucosa;

FIG. **5** is a perspective cutaway view of FIG. **5** showing the mouthpiece placed within the user's mouth and elec- 45 trodes of the mouthpiece contacting the oral mucosa to stimulate the mental branch nerves;

FIG. **6** is a sectional view of a dental filling and dental implant placed within a user's jaw to deliver directed electrical stimulation to, for example, an inferior alveolar 50 nerve of the second and third molars;

FIG. **7** is a schematic diagram of a human head receiving electrodes on or in a check region to deliver directed electrical stimulation to a buccal branch of the lingual nerve within the check region;

FIG. 8 is a graph, similar to FIG. 3, showing a magnitude of vasodilation/constriction of arterial vessels relative to a mean vessel diameter as a function of a time to return to baseline (T_{BL}) at an optimal electrical stimulation frequency and duty cycle for stimulation of the facial nerves, trigemi- 60 nal nerves, and sphenopalatine ganglia;

FIG. **9** is a graph, similar to FIG. **3**, showing a magnitude of vasodilation/constriction of arterial vessels relative to a mean vessel diameter as a function of a time to return to baseline (T_{BL}) at an optimal electrical stimulation frequency 65 and duty cycle stimulation of the vagus nerve, carotid sinus nerve, and baroreceptors; and

FIG. **10** is a graph, similar to FIG. **3**, showing a magnitude of vasodilation/constriction of arterial vessels relative to a mean vessel diameter as a function of a time to return to baseline (T_{BL}) at an optimal electrical stimulation frequency and duty cycle for stimulation of the sciatic nerve and peripheral nerve.

DETAILED DESCRIPTION OF THE INVENTION

Background-Facial/Trigeminal Nerves

Referring now to FIG. 1, a typical human skull 10 supports a number of cranial nerves 12 emerging directly from the brain, located within the skull 10, and emerging out through cranial foramina 14, or holes, in the skull 10 to reach their final destinations on the exterior of the skull 10 and around the jaw and neck region. These cranial nerves 12 relay information between the brain and other parts of the body.

The trigeminal nerve 20 (fifth cranial nerve) is the largest of the cranial nerves 12 and provides sensation to the face and various motor functions such as biting and chewing functions. The trigeminal nerve 20 includes three major branches: the ophthalmic nerve (V1) 22, the maxillary nerve (V2) 24, and the mandibular nerve (V3) 26. The mandibular nerve (V3) 26 includes several sub-branches including the lingual nerve 28 and the inferior alveolar nerve 30 that have shown to be particularly receptive to electrical stimulation. The facial nerve (seventh nerve) has also been shown to be receptive to electrical stimulation.

The mental branch nerves 40 are a sub-branch of the inferior alveolar nerve 30 and provide sensation to the front of the chin, lower lip, labial gingiva of the mandibular 35 anterior teeth and the premolars. The buccal branch nerves 42 are a sub-branch of the lingual nerve 28 that provides sensation to the cheek and the second and third molar teeth. The locations of the mental branch nerves 40 and buccal branch nerves 42 in and around the jawbone 44 place the stimulation points or respective nerve endings 46 close to the outermost epidermis of the skin making it an ideal location for electrical stimulation where the distance and impedance between an electrode 50 and the target nerve may be minimized. In this respect lower amounts of electrical energy may be needed to stimulate these sensory nerves compared to nerves located deeper within the skin and which may require more invasive procedures to stimulate the nerves.

Electrodes **50** placed at or proximate to the mental branch ⁵⁰ nerves **40** and buccal branch nerves **42** allow for electrical stimulation of the respective nerves to therefore elicit a sustained response of the arterial vessels to dilate/constrict in a pulsating manner, as further discussed below. In one embodiment of the present invention, the electrodes **50** are ⁵⁵ positioned over the mental foramen which may transmit electrical stimulation to the terminal branches of the inferior alveolar nerve and vessels of the mental artery

In one embodiment of the present invention, as further discussed below with respect to FIGS. 4 through 6, the electrodes 50 may be a part of an intraoral device 52 placed in the mouth, such as a mouthguard, dental filling or dental implant, to electrically stimulate the inferior alveolar nerve 30 and mental branch nerves 40 located near or around the lower jawbone 44 region. In an alternative embodiment of the present invention, as further discussed below with respect to FIG. 7, the electrodes 50 may be surface electrodes placed on an outer surface of the cheek, or subcuta-

neous electrodes inserted under the skin in the cheek region to electrically stimulate the buccal branch nerves **42** located in the upper jawbone **44** region and the facial nerves below the cheek.

Temporal Stimulation Patterns to Increase CSF Flow

Referring now to FIG. **2**, an optimization of the temporal patterning and stimulation parameters may maximize the ¹⁰ cerebral pulsatility and increase the CSF flow to maximize waste clearance from the brain. The pulsatility may be defined as a change in the vessel diameter over time relative to a mean vessel diameter.

Electrical stimulation of the target nerves may be accomplished using an electrical stimulator **58** such as those commercially available from Tucker-Davis Technologies of Alachua, Fla. or A-M Systems of Sequim, Wash. The electrical stimulator **58** may include a carrier wave generator **60** having a processor **102** being an electronic computer 20 having a self-contained nonvolatile memory **103** holding an operating program **105** and necessary storage variables as will be described below. The nonvolatile memory **103** may comprise, for example, flash memory and/or read only memory, or other similar nonvolatile memory as context 25 requires, which may store data values to be retained even in the absence of electrical power. The processor **102** may be a STM32 Nulceo board or PIC microcontroller as known in the art.

The processor **102** provides various inputs and output 30 lines communicating, for example, with one or more stored programs **105** stored in non-transitory memory **103** and the carrier wave generator **60** to generate a carrier wave **62** at a carrier frequency and amplitude. In one embodiment, the processor **102** may be external to the intraoral device **52** and 35 communicate wirelessly with the carrier wave generator **60** on the intraoral device **52**. In an alternative embodiment, the processor **102** may be mounted on a flexible printed circuit board and incorporated or molded onto the intraoral device **52** to communicate with the carrier wave generator **60** on the 40 intraoral device **52** via a wired connection.

The carrier wave 62 is delivered to a modulator 64 modulating the carrier wave 62 amplitude according to a modulating signal 70. In a simplest configuration, modulator 64 passes the carrier wave 62 without modification during a 45 first stimulation period 66 and/or turns off the carrier wave 62 during a second period 68. In this case, the modulating signal 70 may be a discontinuous waveform such as a pulse or square wave. As is understood in the art, signal modulation by the modulator 64 may provide an envelope of the 50 peaks of the carrier wave 62, the latter being of much higher frequency than the modulating signal 70. Although the modulating signal 70 is shown as a square wave in FIG. 2, the modulating signal 70 may also be a smooth curve as shown in FIG. 3. Referring also to FIG. 3, the stimulation 55 parameters of the modulating signal 70 may be empirically set in order to maximize CSF flow through arterial vessels to the brain. This set point may be established, for example, by monitoring a set of patients being scanned in a computed tomography (CT) scanner or magnetic resonance imaging 60 (MRI) scanner with contrast media to detect CSF/ISF flow and adjusting the stimulation time and relaxation time to maximize the area 80 beneath the CSF/ISF flow curve 82. These settings may then be used generally for all patients or may be optimized for particular patient classes such as by 65 age, height and weight, and sex. Ideally the set point will provide a relaxation time (pulse interval 68) that is no less

than the time to return to baseline (T_{BL}) measured after brief periods of stimulation (pulse duration **66**). While the inventors do not wish to be bound by a particular theory, it is believed that the accommodation or acclamation of the tissue to the stimulation effectively limits the clearance when continuous stimulation is provided as understood in the prior art. By interleaving stimulation (pulse duration **66**) with periods of rest (pulse interval **68**), recovery processes of the glymphatic and meningeal lymphatic system may be accommodated to allow greater clearance long run.

Thus, the dilation/constriction of arterial vessels at various modulating signal frequencies may be compared to maximize the area **80** under the curve **82** of FIG. **3**, for example, slow, large amplitude changes in clearance (produced by prolonged carrier frequency stimulation) may be compared with faster, smaller amplitude changes in clearance (produced by shortened carrier frequency stimulation) to provide the greatest increases in CSF flow over time in the perivascular space. Similar comparisons may be done with respect to the spacing between stimulation provided by the relaxation period.

The following are exemplary embodiments of modulating signal frequencies for specific target nerves optimized to create a full pulse without attenuating the peak flow response but accelerating the return to baseline.

Example 1

Facial Nerves, Trigeminal Nerves, and Sphenopalatine Ganglia

Referring to FIG. 8, the carrier wave 62 may be a single frequency waveform (e.g. a sine wave) with the frequency of the carrier wave 62 less than 75 hertz, and between 20 hertz and 60 hertz and preferably between 25 hertz and 55 hertz, with the preferred range centered around 50 hertz. At higher frequencies (75 Hz or above), habituation occurs before peak flow change is obtained, causing a weaker effective pulse.

In some embodiments, the modulating signal **70** of the modulator **64** may be a single frequency, monophasic signal such as a sine wave creating "bursts" of electrical stimulation. The frequency of the modulating signal **70** is preferably between 0.5 hertz and 0.1 hertz. The modulating signal **70** may provide electrical stimulation **72** with electrical pulses **74** having a time duration **66** between 1 second and 10 seconds, and preferably 5 seconds, and preferably 5 seconds between 1 second and 10 seconds, and preferably 5 seconds between 1 second and 10 seconds, and preferably 5 seconds between pulses. Although the inventors do not wish to be bound by a particular theory, the introduction of a relaxation period where there is no stimulation (pulse interval **68**) counterintuitively increases total clearance.

In one embodiment of the present invention, the carrier wave **62** may have a frequency between 5 kilohertz and 300 kilohertz for non-invasive stimulation. The carrier wave **62** may have a current amplitude of less than 100 microamps for invasive stimulation and less than 40 milliamps for non-invasive stimulation and a voltage controlled to achieve this current per current control known in the art. The modulating signal **70** may have a period between 15 microseconds and 5 milliseconds.

Although electrical stimulation has been shown and described with respect to stimulating the facial nerves and trigeminal nerves, it is understood that the temporal patterning of the present invention may also be applied to other

target nerves identified as providing increased CSF flow, and as further described below with respect to Examples 2 and 3.

Example 2

Vagus Nerve, Carotid Sinus Nerve, and Baroreceptor

Changes in cerebral vasculature blood flow driven by ¹⁰ stimulation of baroreflex inputs such as the vagus nerve, aortic depressor nerve, carotid sinus nerve, and carotid sinus bulb/aortic arch are not driven by direct connection to the cerebral vasculature. Instead, they dilate the peripheral arteries through activation of the baroreflex pathway, and the ¹⁵ cerebral vessels then react to maintain constant perfusion in the brain. As this response is indirect it has a slower time constant for temporal patterning. Stimulation must be maintained longer to cause this indirect effect on cerebral vasculature, and the habituation period is driven by the entire ²⁰ system finding a new set point for homeostasis. The longer rest period is needed to allow the neural inputs indirectly governing the peripheral vasculature response to recover.

Referring to FIG. **9**, the carrier wave **62** may be a single frequency waveform (e.g. a sine wave) where the frequency ²⁵ of the carrier wave **62** may be less than 75 hertz, and between 20 hertz and 75 hertz and preferably between 25 hertz and 50 hertz, with the preferred range centered around 30 hertz. At higher frequencies (75 Hz or above), neural habituation occurs before peak flow change is obtained ³⁰ and/or unwanted chemoreceptor activation can occur, causing a weaker effective pulse.

In some embodiments, the modulating signal **70** of the modulator **64** may be a single frequency, monophasic signal such as a sine wave creating "bursts" of electrical stimula-³⁵ tion. The frequency of the modulating signal **70** is preferably between ¹/₄₅ hertz and ¹/₁₈₀ hertz. The modulating signal **70** may provide electrical stimulation **72** with electrical pulses **74** having a time duration **66** between 15 seconds and 60 seconds, and preferably 30 seconds, and pulse intervals **68** 40 between **30** seconds. Although the inventors do not wish to be bound by a particular theory, the introduction of a relaxation period where there is no stimulation (pulse interval **68**) counterintuitively increases total clearance. **45**

In one embodiment of the present invention, the carrier wave **62** may have a frequency between 5 kilohertz and 300 kilohertz for non-invasive stimulation. The carrier wave **62** may have a current amplitude of less than 100 microamps for invasive stimulation and less than 40 milliamps for ⁵⁰ non-invasive stimulation and a voltage controlled to achieve this current per current control known in the art. The modulating signal **70** may have a period between 15 microseconds and 5 milliseconds.

Example 3

Sciatic Nerve and Peripheral Nerve

The mechanism by which peripheral nerves influence 60 blood flow in the cerebral vasculature blood flow that are not mediated by the baroreflex is by increasing activity in specific regions of the brain. This increase in brain activity increases metabolic demand in these areas, and the vasculature of the brain compensates to increase supply, known as 65 neurovascular coupling. Consequently, the temporal patterning needed to optimize pulsatility of the cerebral vasculature

is slower than described for facial/trigeminal nerves that directly dilate cerevasculature or for baroreflex mediated response. This creates the smallest increase in pulsatility of the neural input options described. However, as neural inputs such as the sciatic are superficial, they are often easier to engage with non-invasive or minimally invasive surgical strategies. There is a delay for the blood flow to respond to the increased metabolic demand, and the rest period is necessary to allow metabolic demand/supply to return to normal before activating another pulse sequence.

Referring to FIG. 10, the carrier wave 62 may be a single frequency waveform (e.g. a sine wave) with the frequency of the carrier wave 62 may be less than 75 hertz, and between 20 hertz and 60 hertz and preferably between 25 hertz and 55 hertz, with the preferred range centered around 50 hertz.

In some embodiments, the modulating signal 70 of the modulator 64 may be a single frequency, monophasic signal such as a sine wave creating "bursts" of electrical stimulation. The frequency of the modulating signal 70 is preferably between $\frac{1}{400}$ hertz and $\frac{1}{40}$ hertz. The modulating signal 70 may provide electrical stimulation 72 with electrical pulses 74 having a time duration 66 between 1 minute and 4 minutes, and preferably 3 minutes, and pulse intervals 68 between 4 minutes. Although the inventors do not wish to be bound by a particular theory, the introduction of a relaxation period where there is no stimulation (pulse interval 68) counterintuitively increases total clearance.

The invention contemplates that at some point it may be possible to provide real-time sensing of clearance. In that case the processor **102** executing one or more stored programs **105** stored in non-transitory memory **103** may automatically determine a frequency in which pulsatility is maximized by providing variations in the above described parameters and monitoring clearance appropriately. Similarly, the processor **102** may automatically determine a minimum time duration of the electrical pulses required to provide maximum effect.

In this respect, the real-time sensing of clearance, for example, monitoring preictal seizure activity or heart rate, may be used to determine when additional electrical stimulation to the stimulation device is needed and further administered to the patient, or to alert the patient or medical professional to deliver electrical stimulation to the patient.

The CSF/ISF flow may be monitored using known imaging modalities such as CT scan, MRI scan, and panoramic x-ray during electrical stimulation. It is understood that other physiological factors may also be monitored to determine the effectiveness of stimulation parameters, such as changes to heart rate, respiratory rate, or presence of certain biomarkers in the patient's blood or saliva as further described below. These physiological factors may be measured using, for example, neuroimaging techniques (e.g., panoramic x-ray, computerized topography (CT) scan, diffuse optical imaging (DOI), event-related optical signal (EROS), magnetic resonance imaging (MM), functional 55 magnetic resonance imaging (fMRI), magnetoencephalography (MEG), positron emission tomography (PET), singlephoton emission computed tomography (SPECT), and cranial ultrasound), cognitive function testing (e.g., learning tests and memory tests), motor function testing, sensory function testing, biopsy, CSF testing, blood testing and/or genetic testing.

Intraoral Device to Activate the Facial/Trigeminal Nerves

Referring to FIGS. 4 and 5, the electrical stimulation 72 of facial and lingual nerves may be facilitated by electrodes

50 placed on an intraoral device 52 placed within the mouth. The intraoral device 52 may be used to conveniently and consistently position the electrodes 50 at specific locations in the mouth to provide electrical stimulation 72 to target nerves. For example, the electrodes 50 may be placed in close proximity to the mental foramen and/or the inferior alveolar nerve 30 and mental branch nerves 40, accessible through the labial gingiva 90 and alveolar mucosa 92 of the mouth as described below. The hydrated epithelial tissue of the labial gingiva 90 and alveolar mucosa 92 assist to provide a conductive path to the target nerves.

In one embodiment of the present invention, the intraoral device 52 is a mouthpiece 100 receivable into a patient's mouth and configured to carry the electrical circuitry of the 15 electrical stimulator 58 as described above with respect to FIG. 2, and generally including the processor 102 and battery power supply 104 (for example, including rechargeable lead acid or lithium ion batteries) for delivery of electrical stimulation 72 to the electrodes 50 within the 20 100 may support the electrical circuitry components of the mouth.

The mouthpiece 100 may be a mouthguard-type device made of a medical grade, non-conductive material such as acrylic, poly (vinyl acetate-ethylene) copolymer clear thermoplastic, polyurethane, laminated thermoplastic, or other 25 medical grade plastic. The mouthpiece 100 provides a cover that extends upward or downward over at least part of the teeth 106, labial gingiva 90, and optionally, alveolar mucosa 92 in a manner which would support electrodes 50 close to the labial gingiva 90, and optionally, alveolar mucosa 92 30 overlaying the target nerves. The mouthpiece 100 may be custom molded to fit a specific patient's mouth, teeth 106 and jawbone 44. For example, the mouthpiece 100 may be 3D printed based on a CT scan of the jawbone 44. Alternatively, the mouthpiece 100 may be manufactured at various 35 predetermined sizes in a manner which would allow the mouthpiece 100 to fit different sized mouths, teeth 106 and jawbones 44 of patients.

The mouthpiece 100 may be molded to receive both the upper and lower dental arches of a patient's mouth when the 40 mouthpiece 100 may be determined by a location of the jawbone 44 is closed and the teeth 106 bite down on the mouthpiece 100, similar to a conventional sports mouthguard. However, it may be desired that the mouthpiece 100 also be formed of separate upper and lower components which may be worn on one or both of the upper or lower 45 dental arches of the patient's mouth, similar to a conventional dental retainer, so that the jawbone 44 can be opened and closed when the mouthpiece 100 is worn.

In an exemplary embodiment showing a lower component mouthpiece 100, as illustrated in FIGS. 4 and 5, the mouth- 50 piece 100 may be an arcuate tube 107 having a circular or oval cross section cut along a generally longitudinal plane to define a downwardly extending arch with a downwardly extending outer sidewall 108 and inner sidewall 110 extending generally parallel and flanking outer and inner sides of 55 the lower teeth 106 respectively. A bottom of the arcuate tube 107 is open to reveal a channel 112 sized and shaped to receive the lower teeth 106 of the patient's mouth. The arcuate tube 107 extends over a top of the lower teeth 106 with the outer sidewall 108 extending downwardly along an 60 outer side of the lower teeth 106 to partially cover at least part of the labial gingiva 90 and optionally the alveolar mucosa 92 on an outside of the lower dental arch, while the inner sidewall 110 extends downwardly along a rear side of the lower teeth 16 and may at least partially cover the labial 65 gingiva 90 and alveolar mucosa 92 on an inside of the lower dental arch. It is understood that the inner sidewall 110 does

not need to extend as far downwardly as the outer sidewall 108 and is meant primarily to support the arcuate tube 107 over the lower teeth 106.

The mouthpiece 100 may have an arcuate length extending rearwardly along a curve generally correlating with the lower dental arch of the patient. The mouthpiece 100 may curve at a front end and extend rearwardly along left and rights sides of the lower jawbone 44 to cover the mandibular anterior teeth 106a and the premolars 106b. The mouthpiece 100 may further extend rearwardly along left and rights sides of the lower jawbone 44 to optionally further cover the second and third molar teeth 106c.

It is understood that an alternative embodiment of the mouthpiece 100 that receives both the upper and lower dental arches of a patient's mouth when the jawbone 44 is closed and the teeth 106 bite down on the mouthpiece 100 may similarly provide outer and inner sidewalls 108, 110 flanking the lower teeth 106.

The outer and inner sidewalls 108, 110 of the mouthpiece electrical stimulator 58 such as the processor 102 and the battery power supply 104. The processor 102 and battery power supply 104 may be embedded within the sidewalls 108, 110 of the mouthpiece 100 so that they do not interfere with the fit of the mouthpiece 100 over the lower dental arch. The processor 102 and battery power supply 104 may communicate with the electrodes 50 supported by the outer sidewall 108 to deliver the modulated electrical stimulation signal 72 to the electrodes 50 as described above.

The battery power supply 104 may provide power to the electrical stimulator 58 in a manner which allows for current delivery to the electrodes 50. It is understood that an external power supply may also be used to deliver power to the electrical stimulator 58 in addition to or instead of the battery power supply 104. It is also understood that the electrical stimulator 58 may be positioned outside of the mouth and communicate remotely with a controller and electrodes 50 of the mouthpiece 100.

A position of the electrodes 50 on the walls of the mental branch nerves 40 and nerve endings 46 in the mouth. In this respect, medical imaging may be used to locate the position of the mental branch nerves 40 in the mouth and to aid in placement of the electrodes 50 on the mouthpiece 100. Specifically, when the mouthpiece 100 is positioned in the patient's mouth, the electrodes 50 are desirably positioned on an interior side of the front sidewall 108 proximate the mandibular anterior teeth 106a and the premolars 106b to abut or be placed in close proximity to the labial gingiva 90 and alveolar mucosa 92 on the outside of the lower dental arch in a manner which provides stimulation to the mental branch nerves 40.

The electrodes 50 may include a stimulating cathode electrode 50a placed close to the desired stimulation site, for example, near the nerve endings 46 of the mental branch nerves 40. An anode electrode 50b may then be placed proximal to the cathode electrode 50a with respect to the nerve endings 46. In this respect, the electrical current flows from the anode electrode 50b to the cathode electrode 50a so that the nerve endings 46 receives the stimulus and propagates an action potential upstream through the mental branch nerves 40. The cathode electrode 50a and anode electrodes 50b are spaced apart along an axis generally parallel to the course of the mental branch nerves 40.

Medical imaging may be used to facilitate precise placement of the cathode electrode 50a close to the nerve ending and the precise placement of the anode electrode 50b upstream from the cathode electrode 50a and proximal to the nerve ending 46. The cathode electrode 50a may be placed less than 2 cm or less than 1 cm from the mental branch nerve ending 46 and the anode electrode 50b may be placed less than 3 cm or less than 2 cm upstream from the cathode 5 electrode 50a along the mental branch nerves 40.

It is understood that the pair of communicating electrodes, i.e., the cathode electrode 50a and anode electrode 50b, may stimulate at least one of the left and right side mental branch nerves 40 of the mouth and the mouthpiece 100 may include 10 more than one pair of anode and cathode electrodes 50a, 50bto stimulate both the left and right mental branch nerves 40 of the left and right sides of the mouth. It is also understood that more than two pairs of anode and cathode electrodes 50a, 50b may be carried by the mouthpiece 100 to stimulate 15 various areas along the mental branch nerves 40. In some embodiments, changing the phase of the modulating signal 70 to different mental branch nerves 40 may be used to enhance the stimulation of the mental branch nerves 40 by timing the delivery of the electrical stimulation to the 20 multiple pairs of electrodes. In one embodiment, electrical simulation may be rotated across several electrodes placed across the target nerve, to maximize activation of that nerve without activating nearby nerves responsible for unwanted side effects.

It is understood that an upper component mouthpiece may be described in a similar manner as the lower component mouthpiece described above and shown in FIGS. **4** and **5** whereby the upper component mouthpiece is rotated 180degrees about a horizontal axis to receive the upper dental 30 arch instead of the lower dental arch and stimulate the superior alveolar nerves of the upper jawbone **44** in a similar manner, as would be understood by one having ordinary skill in the art.

Referring now to FIG. 6, in an alternative embodiment of 35 the present invention, the intraoral device 52 may be a dental filling 120 inserted within a cavity or hole of the tooth 106, or a dental implant 122 implanted within a hole of the gums and jawbone 44, to provide electrical stimulation to the inferior alveolar nerve 30 located below the roots of the 40 molar teeth 106.

In one embodiment, the intraoral device **52** may be dental filling **120** inserted within a cavity or hole **123** drilled through a crown of a molar tooth **106** (similar to a root canal procedure) to expose the pulp **124** of the tooth **106** normally 45 carrying nerves and blood vessels from the healthy tooth to nerves and blood vessels outside and below the tooth **106**. The dental filling **120** may include the electrical circuitry of the electrical stimulator **58** described above with respect to FIG. **2** and stimulating electrodes **50**. The electrodes **50** may 50 include a cathode electrode **50***a* and anode electrode **50***b* separated within the dental filling **120** to provide electrical current flow therebetween and provide current flow into the pulp **124** of the tooth **106** (second and third molar teeth 55 **106***c*) such as the inferior alveolar nerve **30**.

In an alternative embodiment, the intraoral device **52** may be a dental implant **122** implanted within a hole **130** within the gums and jawbone **44** caused by a removed or extracted tooth and providing an opening into which the dental ⁶⁰ implant **122** may be implanted. The dental implant **122** may include the electrical circuitry of the electrical stimulator **58** described above with respect to FIG. **2** and stimulating electrodes **50**. The electrodes **50** may include a cathode electrode **50***a* and anode electrode **50***b* separated within the ⁶⁵ dental implant **122** to provide electrical current flow therebetween and to provide current flow to nerves running

below the hole 130 (below second and third molar teeth 106c) such as the inferior alveolar nerve 30. As understood in the art, the dental implant 122 may also include an implant crown 132 resembling a real tooth worn over the top of the dental implant 122.

Referring to FIGS. 4 through 6, the intraoral devices 52 described above may include and support biomarker sensors 134 with fluorescent indicators indicating the presence of various analytes from tissue or saliva indicating increased levels of neuronal cytokines indicative of an increase in CSF flow to the brain. For example, amyloid beta peptide, tau protein, lactoferrin, alpha-synuclein, DJ-1 protein, chromogranin A, huntingtin protein, DNA methylation disruptions, and micro-RNA profiles may be detected to show an increase in CSF.

The stimulating electrodes 50 or separate electrodes may be used to record electrophysiological signals to detect changes in low frequency power brain waves that propagate outside the calvarium. The electrodes 50 may also be used to pick up heart rate and heart rate variability as well.

Referring to FIG. 7, in another embodiment of the present invention, electrical stimulation of facial and lingual nerves may be facilitated by electrodes **50** placed on or within the cheek region. The electrodes **50** may be a surface electrodes ²⁵ or subcutaneous electrodes providing electrical stimulation to the buccal branch nerves **26** located below the skin in the cheek region.

In one embodiment, the electrodes 50 are surface electrode pads placed externally on the user's cheeks overlying the buccal branch nerves 26 to stimulate the buccal branch nerves 26 and/or facial nerves. The electrodes 50 may include a cathode electrode 50a and anode electrode 50b placed externally on the same cheek. Current flow between the anode and cathode electrodes 50a, 50b may provide electrical stimulation of the target nerve. A second set of anode and cathode electrodes 50a, 50b may be placed on the opposite cheek to stimulate the buccal branch nerves 26 and/or facial nerves of the opposite cheek.

In an alternative embodiment, the electrodes 50 may be subcutaneous electrodes inserted beneath the epidermis within the user's cheeks to stimulate the buccal branch nerves 26. The subcutaneous electrodes may be injectable electrodes 50 such as liquid metal electrodes injectable using a syringe 140 and withdrawable from the skin. The injectable electrodes 50 may include a cathode electrode 50a and anode electrode 50b placed under the skin. Current flow between the anode and cathode electrodes 50a, 50b may provide electrodes 50 may be injected into one or both of the cheeks to stimulate the buccal branch nerves 26.

It is understood that the electrical stimulation describe above could also be accomplished with infrared activation, optogenetic activation, and transcranial/transdermal magnetic stimulation, and focused ultrasound.

The above described methods may be used to treat patients with for example depression, anxiety and epilepsy by increasing the influx of CSF into the brain parenchyma. It has been found that an increase in CSF into the brain parenchyma further dilutes endogenous concentrations of neurochemical transmitters/bioactive molecules and reduces ephaptic (non-synaptic) coupling implicated in abnormal circuit behaviors associated with multiple disorders of the nervous system, for example, anxiety disorders, epilepsy, Alzheimer's disease, and Parkinson's disease.

It is understood that the present invention is not limited to the treatment of traumatic brain injury/chronic traumatic encephalopathy, epilepsy, Alzheimer's disease, and Parkinson's disease and the like and may also be used to treat other conditions and disorders such as hydrocephalus caused by a buildup of CSF in the brain parenchyma by increasing the clearance of CSF through the brain. Also, clearance of orally administered drugs that cross the blood brain barrier, or 5 drugs/biomolecules that are infused via an injection/catheter, can be modulated by changing the CSF flow rate.

In addition to increasing pulsatility, electrical stimulation of the nerves as described above has been found to induce neuroplasticity or cortical plasticity and introduce and 10 modify brain wave oscillation frequency useful for treating neuro-psychiatric disorders. For example, brain wave oscillations may be increased to natural brain wave frequencies, e.g., 8 to 13 hertz, which may be lower in older adults experiencing memory difficulties, and activation of circuitry 15 through the trigeminal sensory nuclei to create broad neurochemical changes in the brain mediated by cross connectivity to the nucleus of the solitary tract (NTS) to enhance plasticity in many conditions such as stroke and tinnitus. The NTS has inputs to locus coeruleus, raphae nucleus, and 20 nucleus basalis which are responsible for most norepinephrine, serotonin, dopaminergic, and cholinergic projections to the rest of the brain. Certain terminology is used herein for purposes of reference only, and thus is not intended to be limiting. For example, terms such as "upper", "lower", 25 "above", and "below" refer to directions in the drawings to which reference is made. Terms such as "front", "back", "rear", "bottom" and "side", describe the orientation of portions of the component within a consistent but arbitrary frame of reference which is made clear by reference to the 30 text and the associated drawings describing the component under discussion. Such terminology may include the words specifically mentioned above, derivatives thereof, and words of similar import. Similarly, the terms "first", "second" and other such numerical terms referring to structures do not 35 imply a sequence or order unless clearly indicated by the context.

When introducing elements or features of the present disclosure and the exemplary embodiments, the articles "a", "an", "the" and "said" are intended to mean that there are 40 one or more of such elements or features. The terms "comprising", "including" and "having" are intended to be inclusive and mean that there may be additional elements or features other than those specifically noted. It is further to be understood that the method steps, processes, and operations 45 described herein are not to be construed as necessarily requiring their performance in the particular order discussed or illustrated, unless specifically identified as an order of performance. It is also to be understood that additional or alternative steps may be employed. 50

References to "an electronic computer" and "a processor" or "the microprocessor" and "the processor," can be understood to include one or more of these devices that can communicate in a stand-alone and/or a distributed environment(s), and can thus be configured to communicate via 55 is supported by a mouthpiece configured to engage a jaw of wired or wireless communications with other processors, where such one or more processor can be configured to operate on one or more processor-controlled devices that can be similar or different devices. Furthermore, references to memory, unless otherwise specified, can include one or more 60 processor-readable and accessible memory elements and/or components that can be internal to the processor-controlled device, external to the processor-controlled device, and can be accessed via a wired or wireless network.

References to "a processor" should be understood to 65 include electronic computers, microprocessors, microcontrollers, FPGA devices, ASIC devices and similar program-

mable or program defined electronic circuits and collections of such devices that can communicate in a stand-alone and/or a distributed environment(s), and can thus be configured to communicate via wired or wireless communications with other processors. Furthermore, references to memory, unless otherwise specified, can include one or more processor-readable and accessible memory elements and/or components that can be internal to the processor or external to the processor and accessed via a wired or wireless network.

It is specifically intended that the present invention not be limited to the embodiments and illustrations contained herein and the claims should be understood to include modified forms of those embodiments including portions of the embodiments and combinations of elements of different embodiments as come within the scope of the following claims. All of the publications described herein, including patents and non-patent publications, are hereby incorporated herein by reference in their entireties.

What we claim is:

1. An electrical stimulation device for improving waste clearance through a perivascular system of a blood brain barrier comprising:

- at least one electrode configured to stimulate a facial nerve;
- an electrical generator generating a carrier wave having a carrier frequency, the electrical generator stimulating the perivascular system into increased cerebral spinal fluid (CSF) and interstitial fluid (ISF) flow;
- an electrical modulation generator configured to generate a modulation wave having a predetermined periodicity providing a first period of stimulation of the perivascular system and a second period of relaxation of the perivascular system, the predetermined periodicity selected to increase pulsatility over continuous stimulation of the perivascular system by the carrier frequency; and
- a modulator receiving the carrier wave and the modulation wave and modulating the carrier wave for application to the at least one electrode.

2. The device of claim 1 wherein the at least one electrode includes a cathode configured to be positioned distally with respect to an end of the facial nerve and an anode configured to be positioned proximally with respect to the end of the facial nerve.

3. The device of claim 2 wherein the cathode and the anode are configured to be spaced apart along an axis substantially parallel to the facial nerve.

4. The device of claim 1 wherein the at least one electrode is adapted to stimulate at least one of a trigeminal nerve, buccal branch nerve, mental branch nerve and facial branch nerve.

5. The device of claim 1 wherein the at least one electrode a user's mouth.

6. The device of claim 5 wherein the mouthpiece is comprised of a curved tube having an inner and outer wall flanking a channel configured to receive at least one of an upper and lower dental arch of a user and covering an outer labia gingiva of the jaw.

7. The device of claim 6 wherein the at least one electrode is supported by an inner surface of the outer wall configured to contact the labia gingiva.

8. The device of claim 7 wherein the at least one electrode comprises a cathode electrode positioned toward a front of the curved mouthpiece configured to receive anterior teeth

and an anode electrode positioned toward a rear of the mouthpiece configured to receive premolar teeth.

9. The device of claim **8** wherein the cathode electrode is configured to overlay nerve endings of mental branch nerve with less than 1 cm distance between the cathode electrode $_5$ and the nerve endings.

10. The device of claim 8 wherein the mouthpiece supports at least two anode-cathode electrode pairs.

11. The device of claim 1 wherein the at least one electrode is supported by a dental filling configured to be inserted within a cavity of a tooth.

12. The device of claim 1 wherein the at least one electrode is supported by a dental implant configured to be inserted within a jawbone.

13. The device of claim **1** further comprising sensors detecting salivary biomarkers indicating a change to CSF flow selected from at least one of the following: amyloid beta peptide, tau protein, lactoferrin, alpha-synuclein, DJ-1 protein, chromogranin A, huntingtin protein, DNA methylation disruptions, and micro-RNA.

14. A method of improving waste clearance through a ²⁰ perivascular system of a blood brain barrier comprising:

- positioning at least one electrode in close proximity to a nerve;
- generating a carrier wave having a carrier frequency stimulating the perivascular system into increased cerebral spinal fluid (CSF) and interstitial fluid (ISF) flow;
- generating a modulation wave having a predetermined periodicity providing a first period of stimulation of the

perivascular system and a second period of relaxation of the perivascular system, the predetermined periodicity selected to increase waste clearance over continuous stimulation of the perivascular system by the carrier frequency; and

modulating the carrier wave and applying the carrier wave to the at least one electrode.

15. The method of claim **14** wherein the carrier frequency of the carrier wave is less than 75 hertz.

16. The method of claim **15** wherein the carrier frequency of the carrier wave is between 25 hertz and 55 hertz.

17. The method of claim **16** wherein the modulation wave has a time duration of between 1 second and 10 seconds and a pulse interval of between 1 second and 10 seconds.

18. The method of claim **17** wherein the at least one electrode is positioned over an inferior alveolar nerve.

19. The method of claim **17** wherein the at least one electrode is positioned over a mental branch nerve.

- **20**. The method of claim **16** wherein the modulation wave has a time duration of between 1 minute and 4 minutes and a pulse interval of between 4 minutes and 6 minutes.
- **21**. The method of claim **15** wherein the carrier frequency of the carrier wave is between 25 hertz and 50 hertz.

22. The method of claim **21** wherein the modulation wave has a time duration of between 15 second and 60 seconds and a pulse interval of between 30 seconds and 120 seconds.

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