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(54) **BALANCED CURRENT-SOURCE INVERTER**

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(*) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 0 days.

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Primary Examiner — Alex Torres-Rivera

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(74) *Attorney, Agent, or Firm* — Bell & Manning, LLC

(51) **Int. Cl.**
H02M 7/521 (2006.01)
H02P 27/06 (2006.01)
H02M 7/523 (2006.01)

(57) **ABSTRACT**

(52) **U.S. Cl.**
CPC **H02M 7/521** (2013.01); **H02M 7/523** (2013.01); **H02P 27/06** (2013.01)

A switching circuit for a current source inverter includes a first inverter leg, a second inverter leg, and a controller. The first inverter leg includes a first reverse-voltage-blocking (RB) switch, a second RB switch, and a third RB switch that are connected in series between a first bus line and a second bus line. The second inverter leg includes a fourth RB switch, a fifth RB switch, and a sixth RB switch are connected in series between the first bus line and the second bus line. The controller is configured to control a switch between an on-state and an off-state for each RB switch. When in the on-state, a reverse voltage is blocked by a respective RB switch, and a current with a positive polarity is conducted through the respective RB switch. When in the off-state, a voltage and the current are blocked by the respective RB switch.

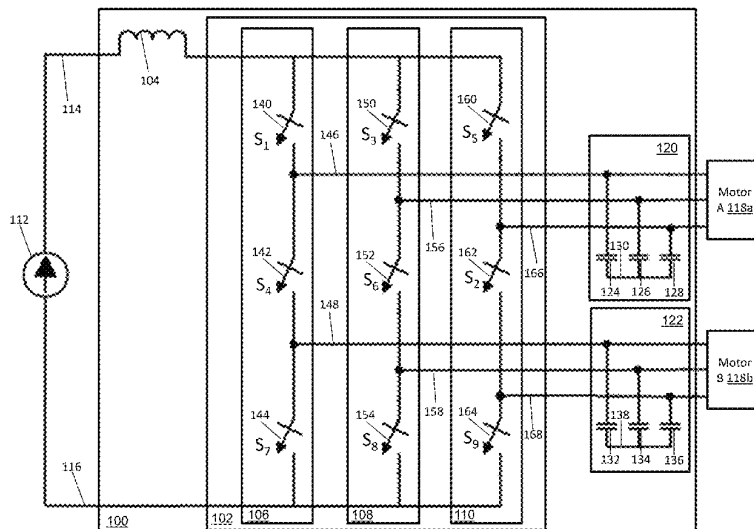
(58) **Field of Classification Search**
CPC H02M 7/521; H02M 7/523; H02M 7/525; H02M 7/527; H02M 7/53; H02M 7/537; H02P 27/04; H02P 27/08; H02P 27/085; H02P 27/10
See application file for complete search history.

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20 Claims, 26 Drawing Sheets
(4 of 26 Drawing Sheet(s) Filed in Color)



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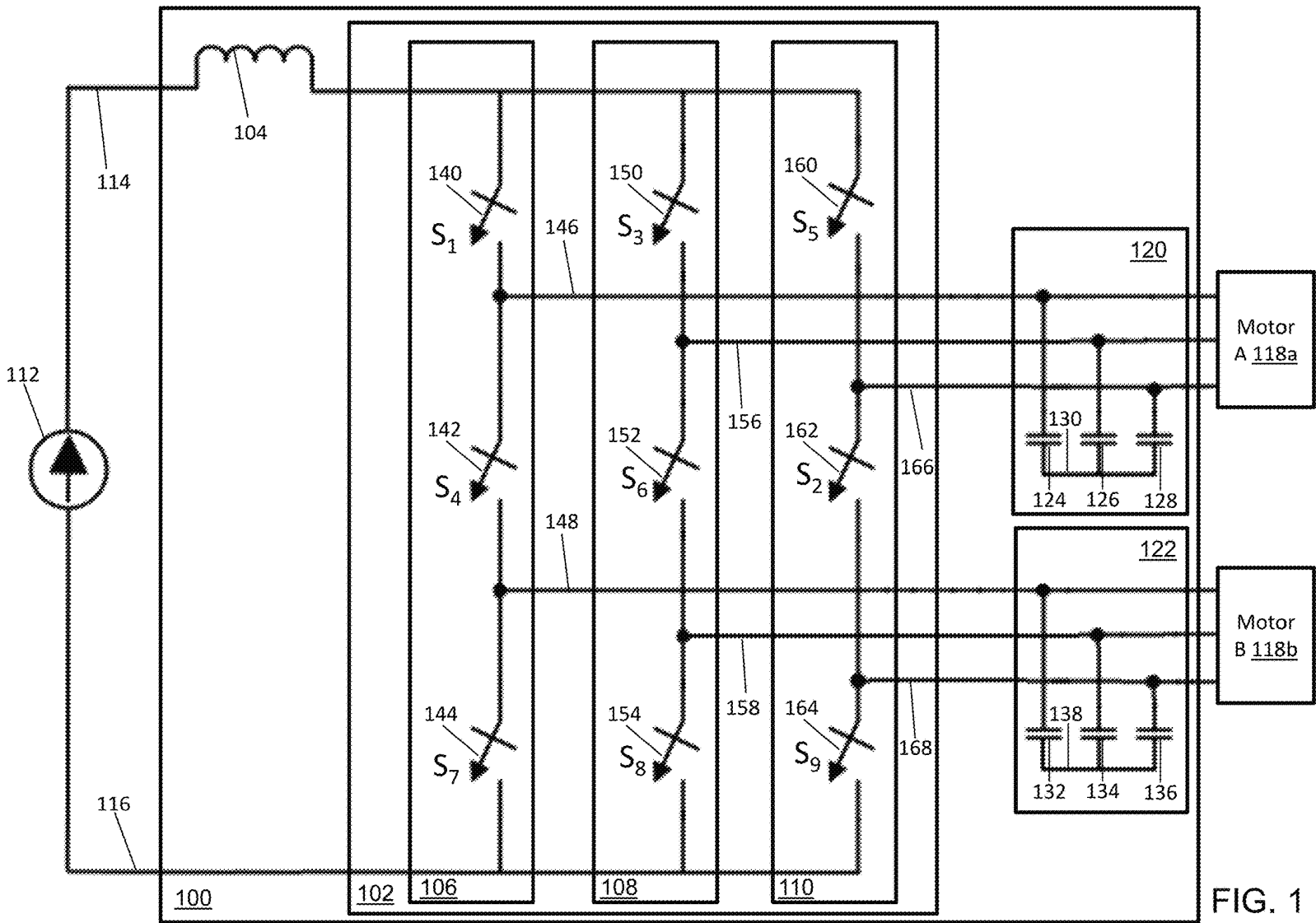


FIG. 1

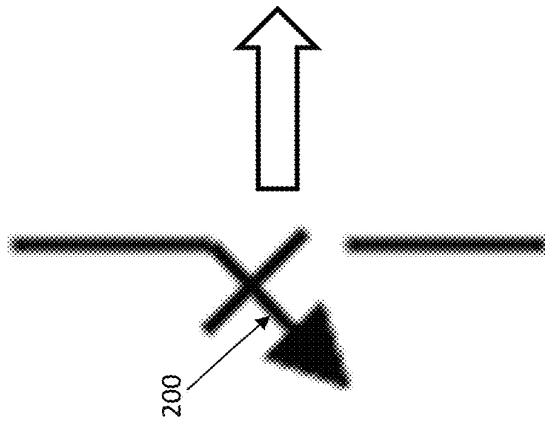
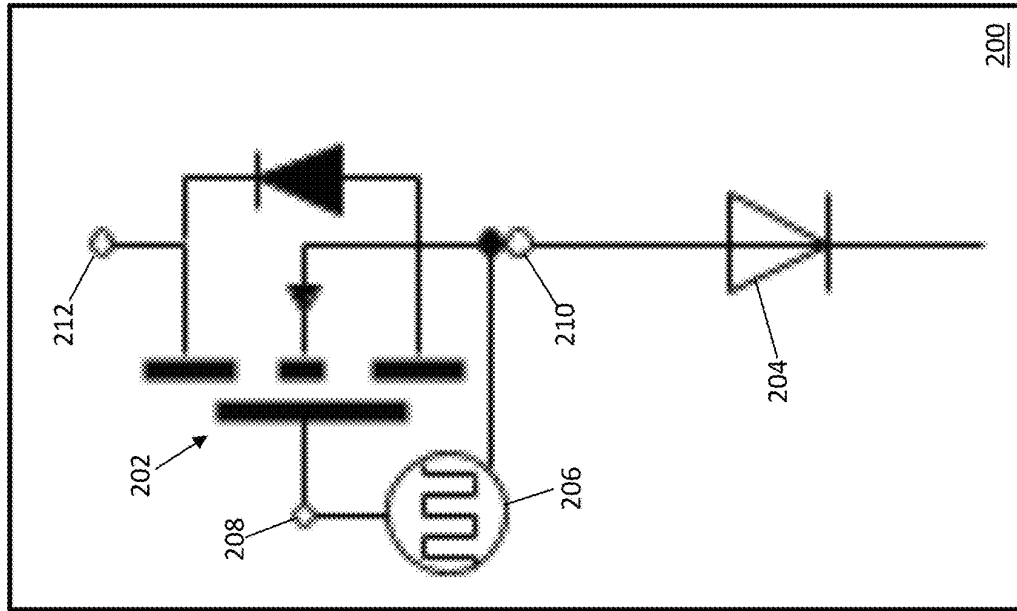


FIG. 2

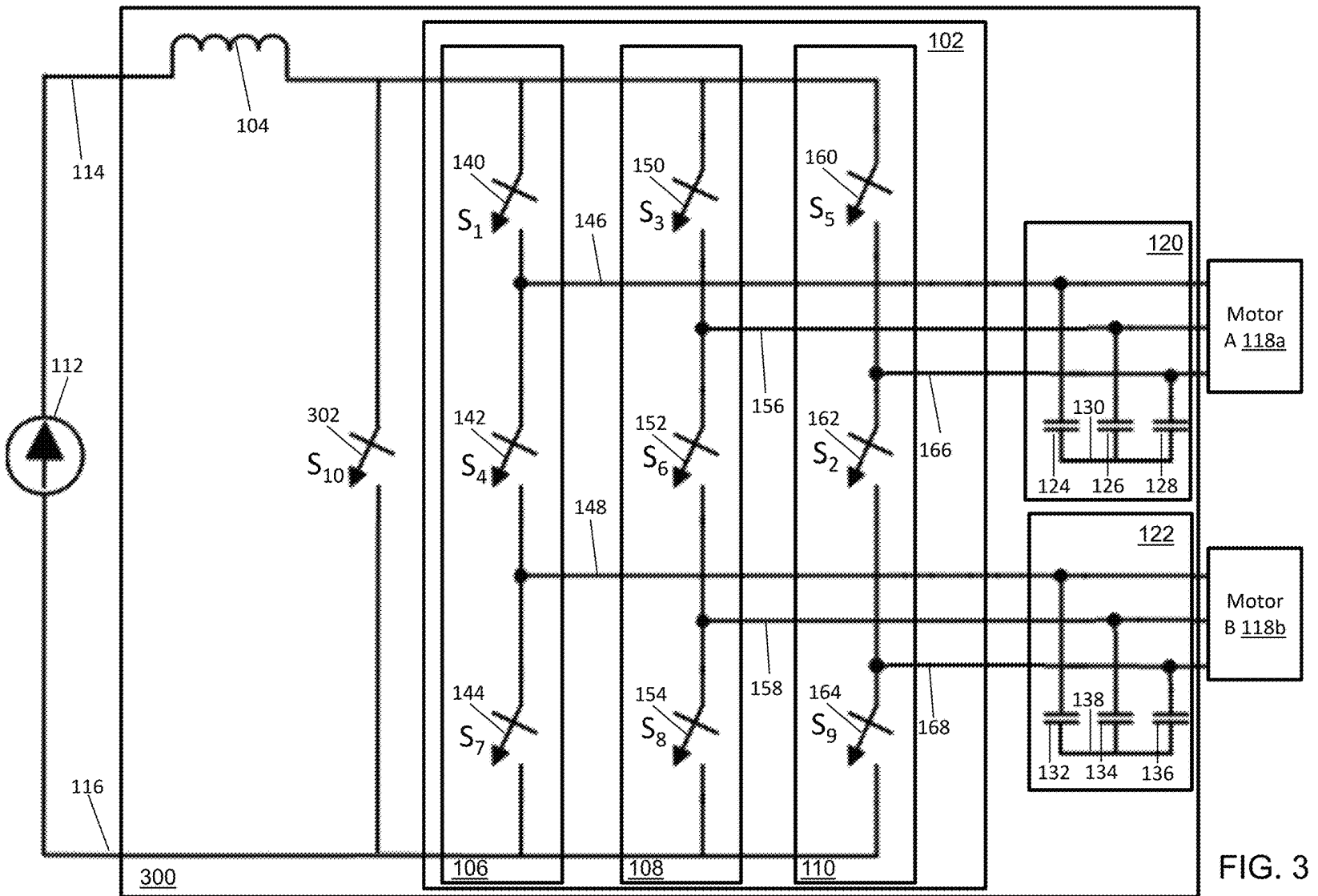


FIG. 3

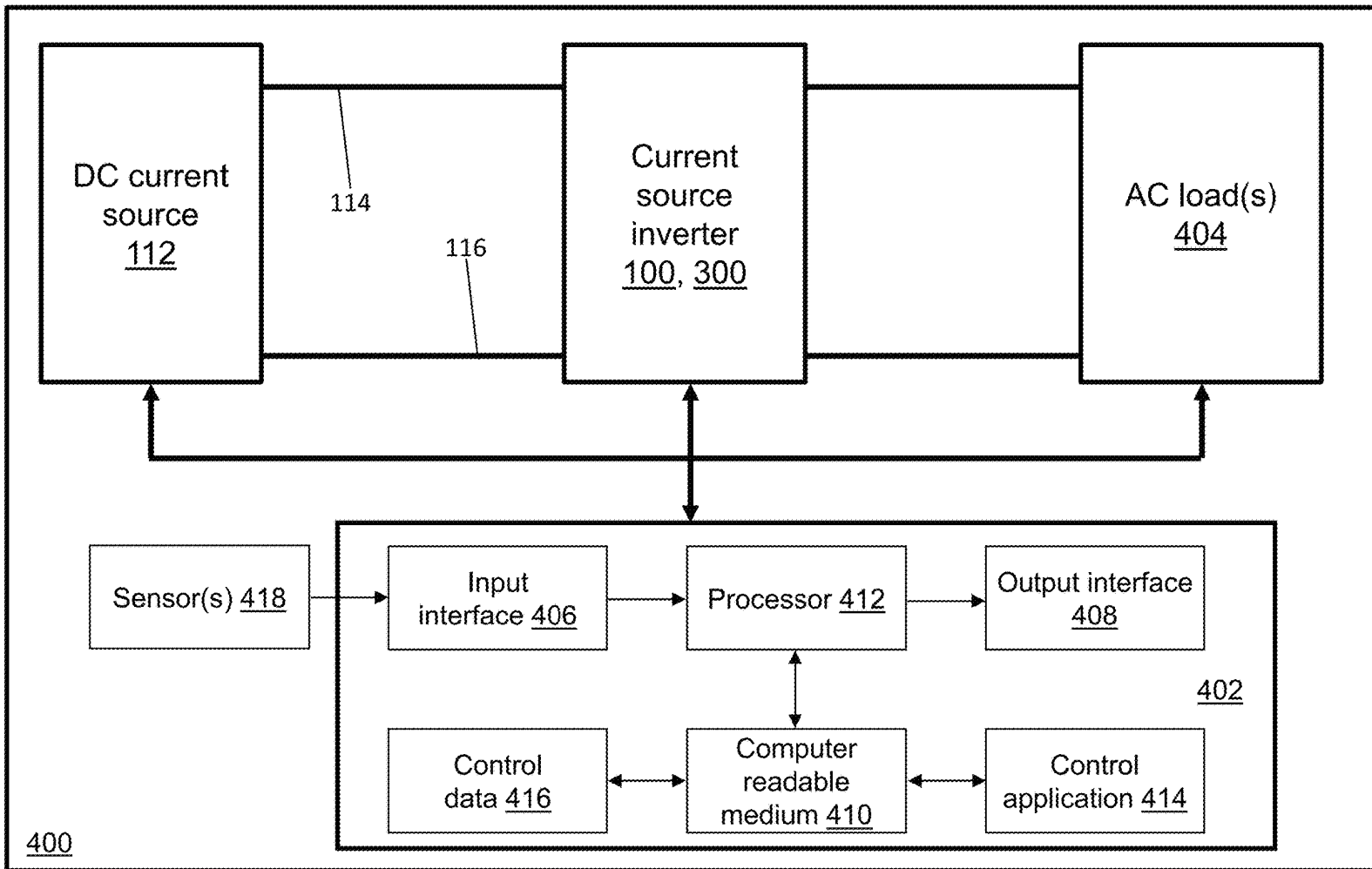


FIG. 4

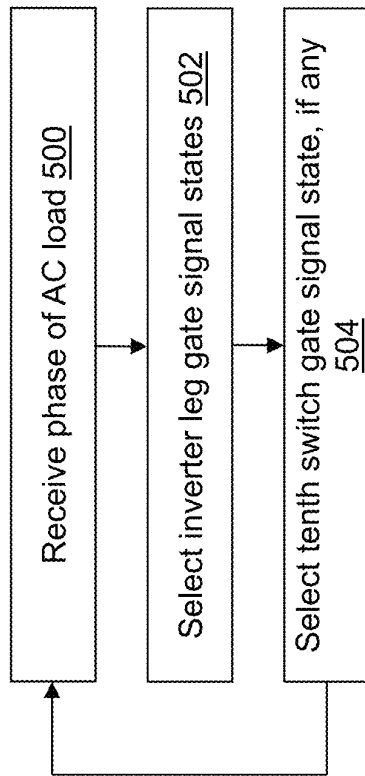
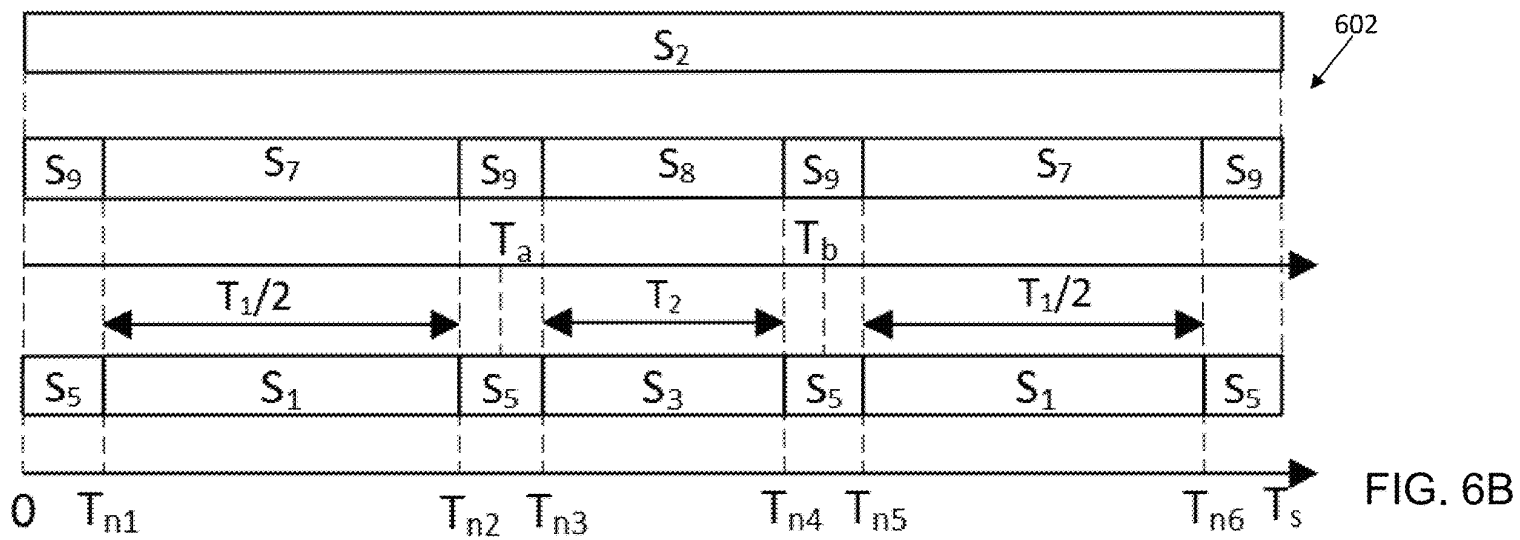
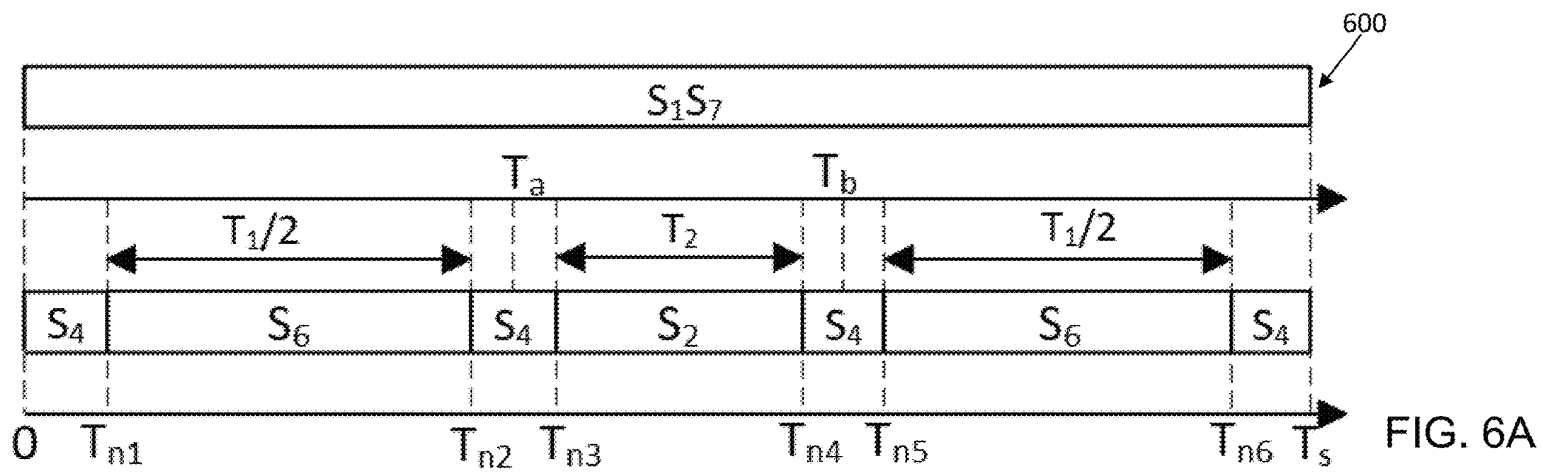
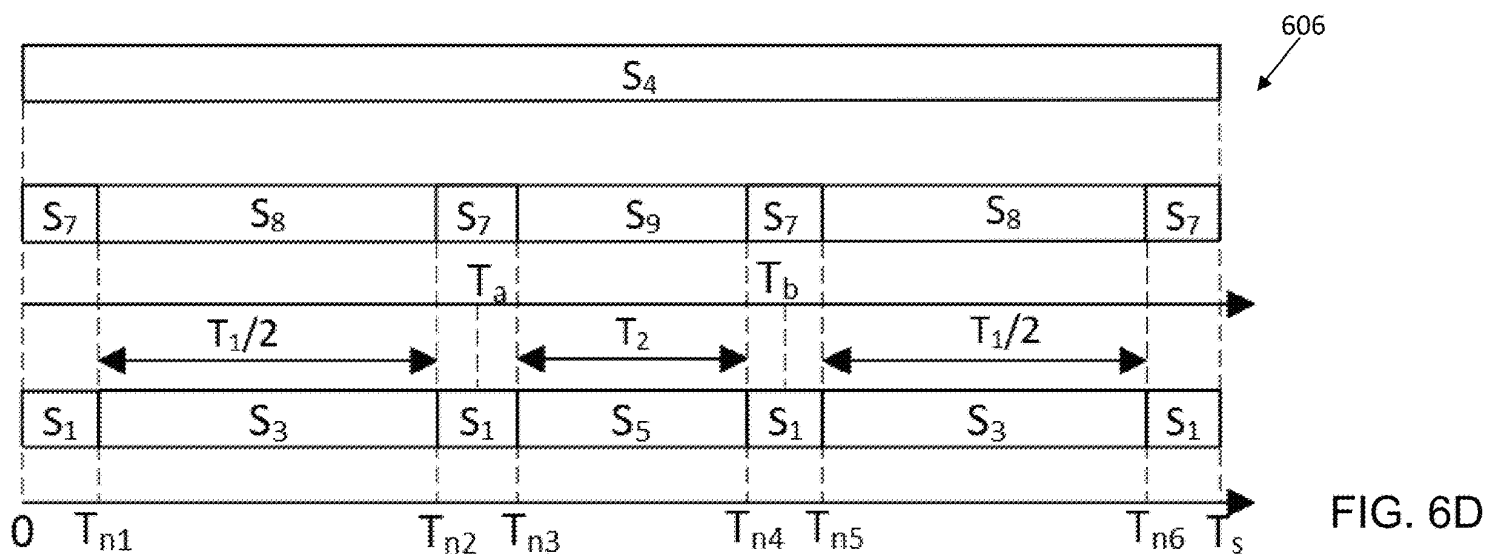
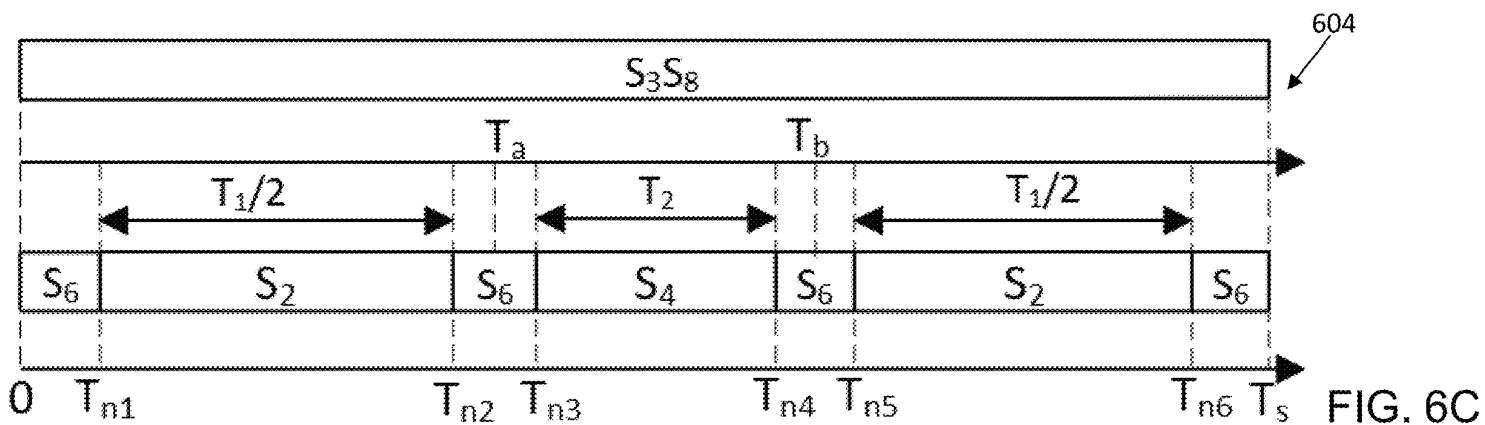


FIG. 5





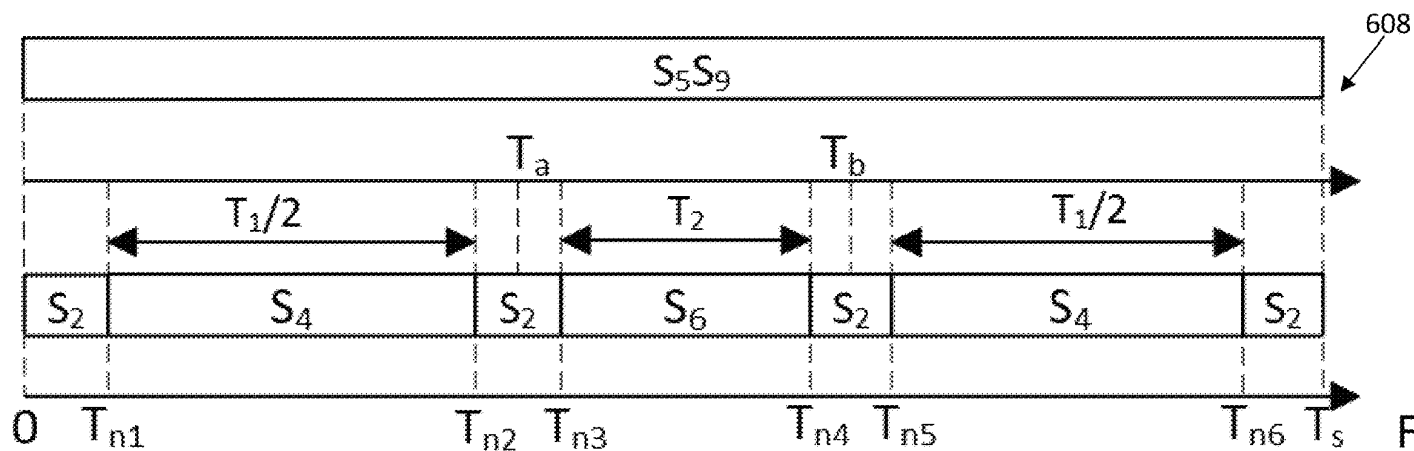


FIG. 6E

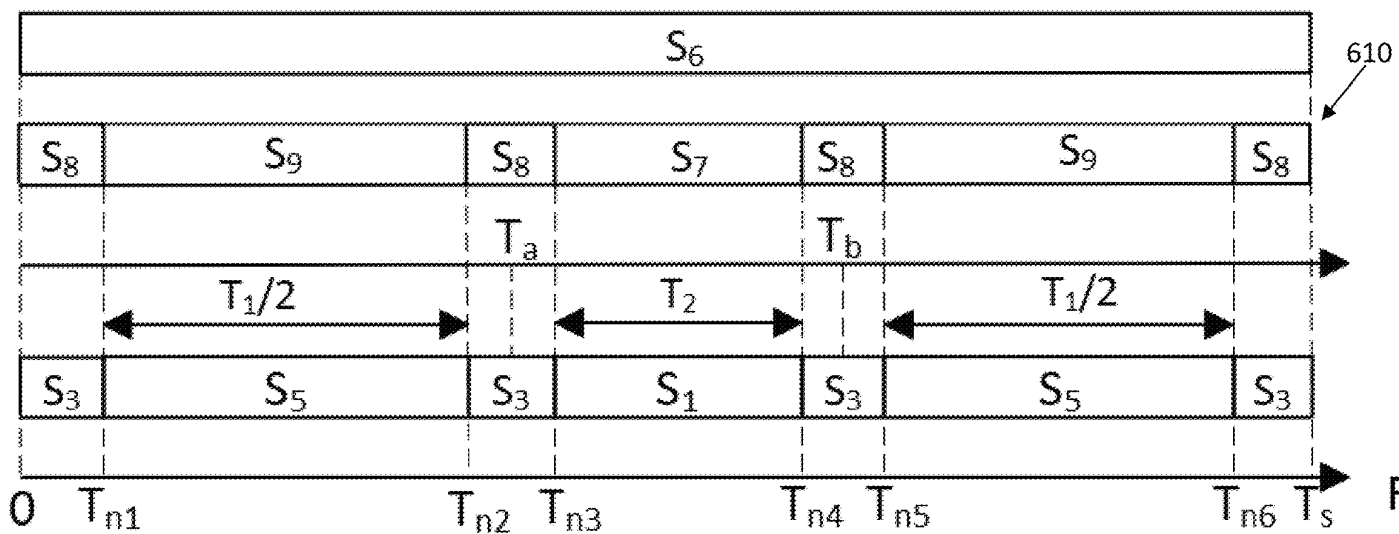


FIG. 6F

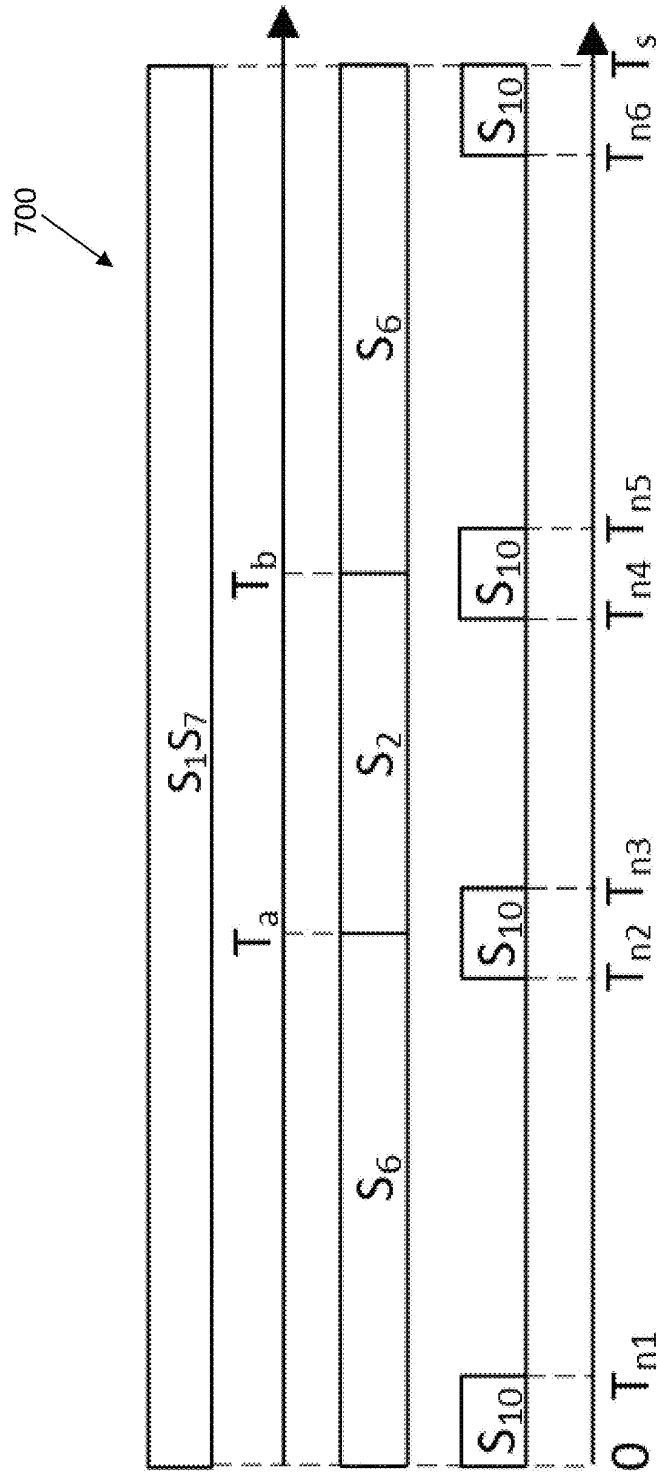


FIG. 7A

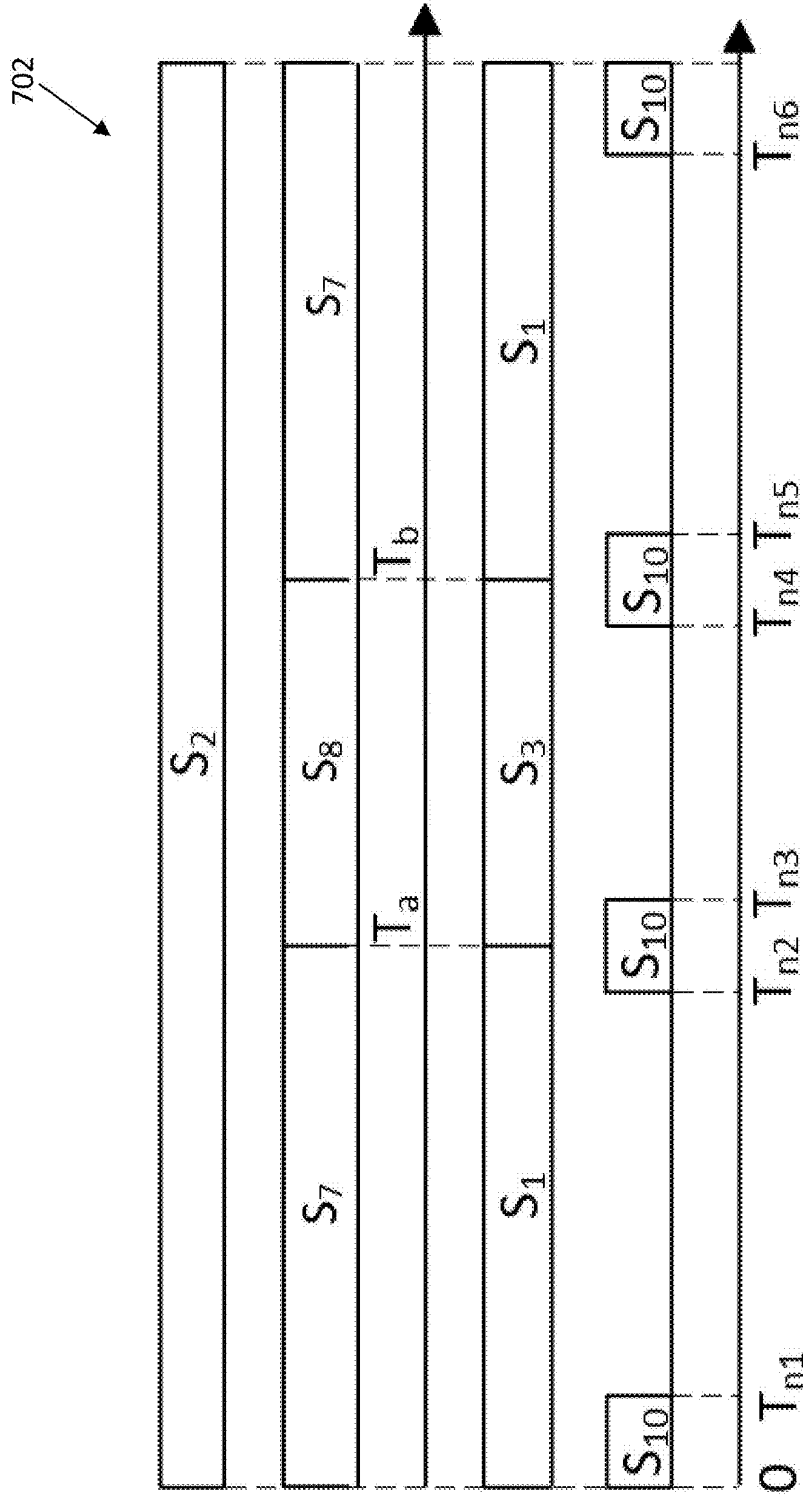


FIG. 7B

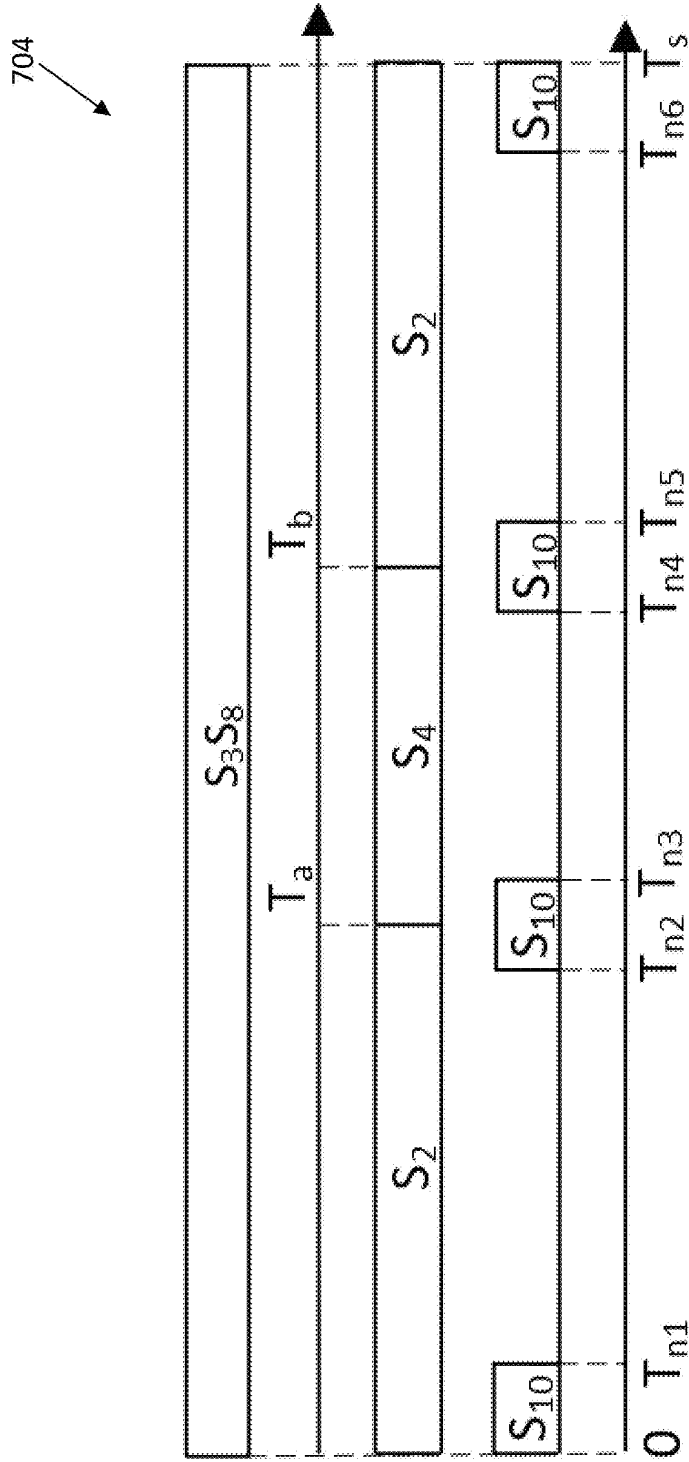


FIG. 7C

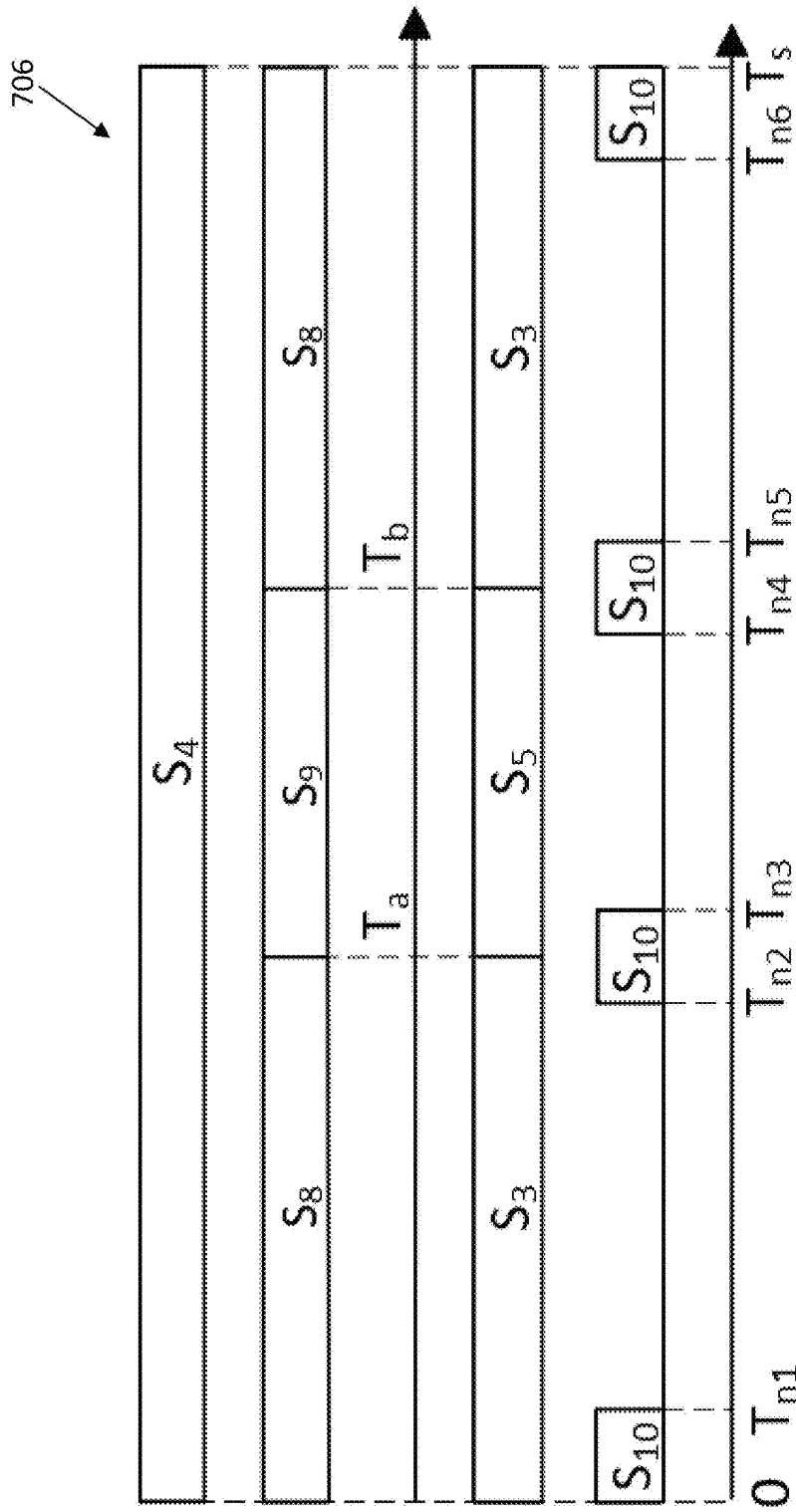


FIG. 7D

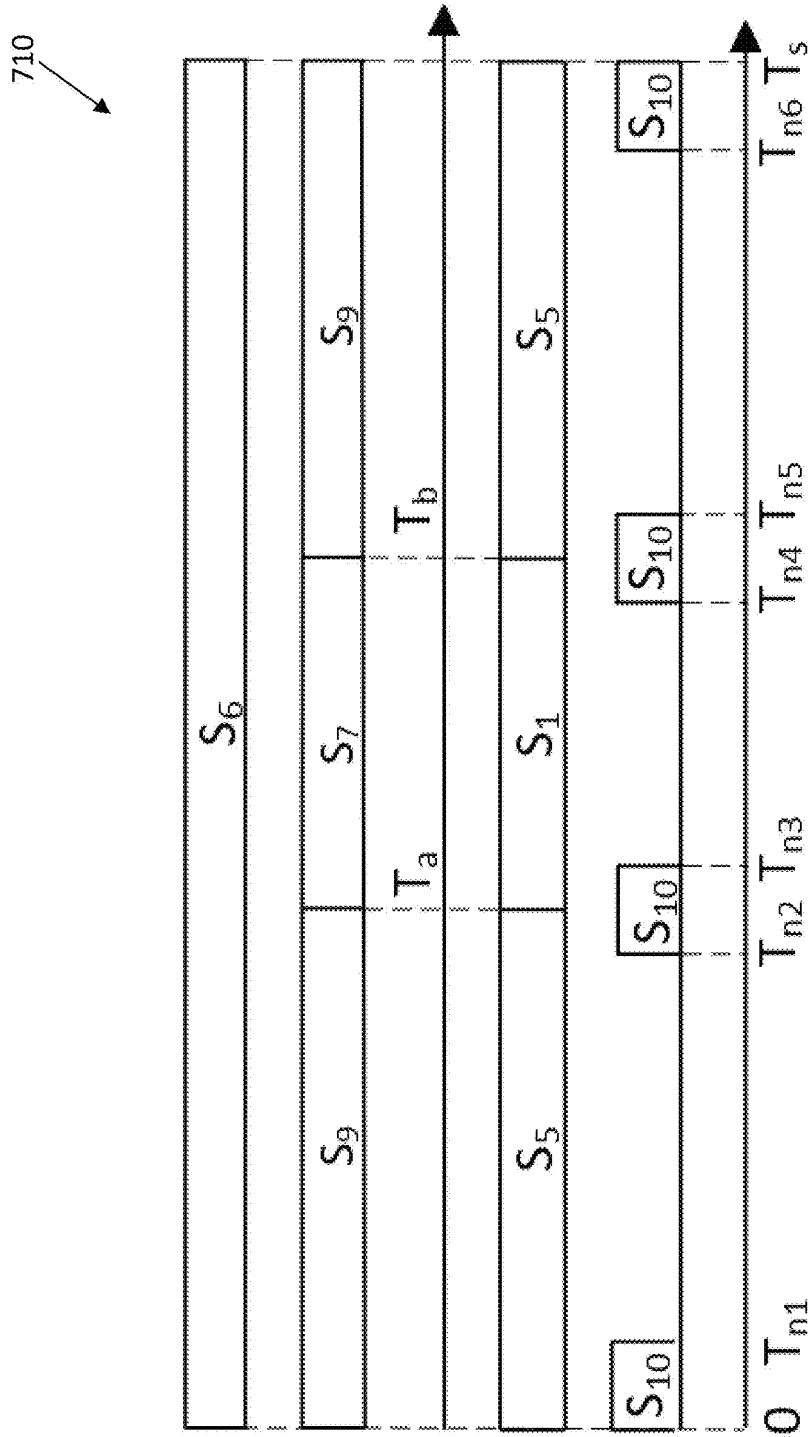


FIG. 7F

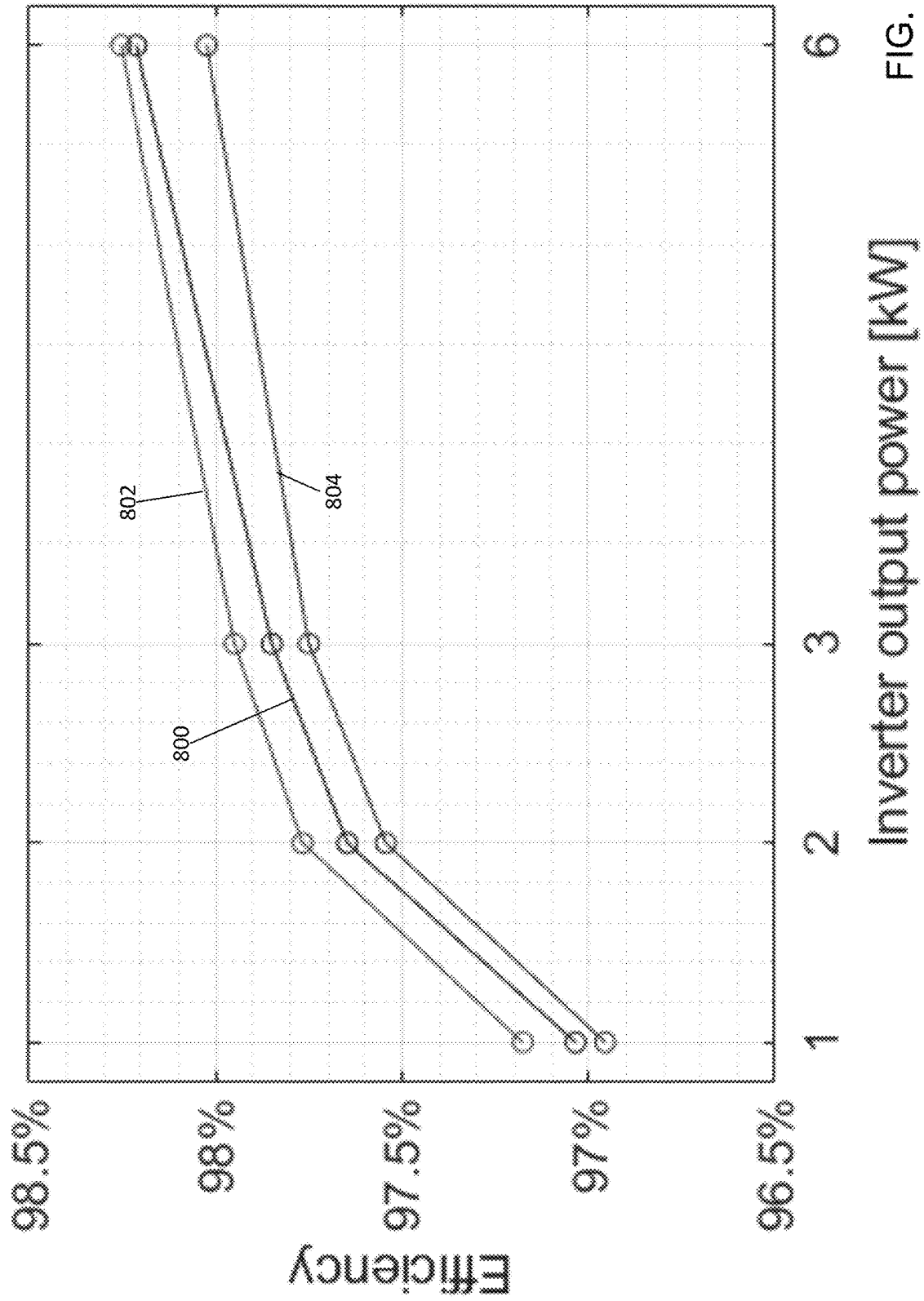


FIG. 8

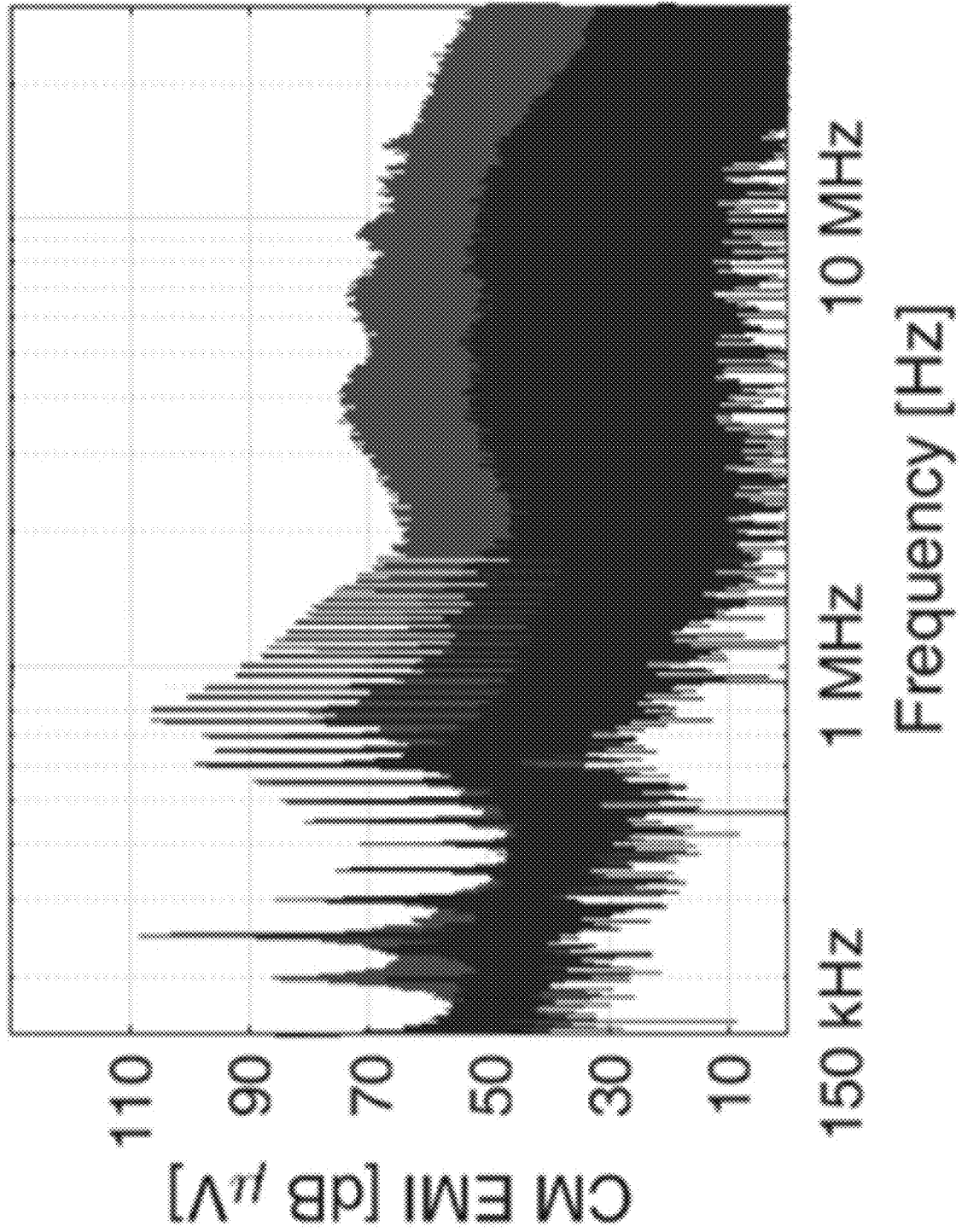


FIG. 9

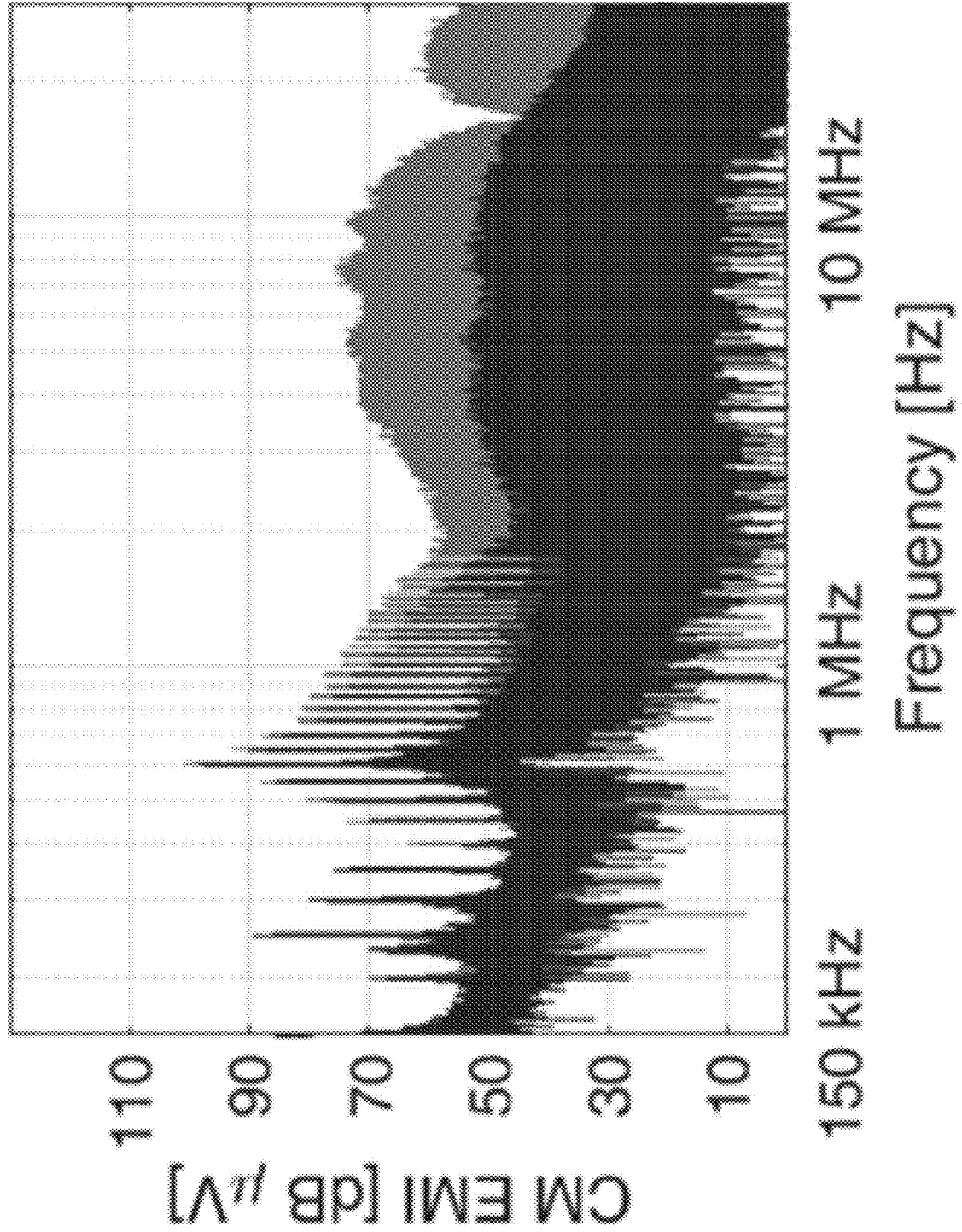


FIG. 10

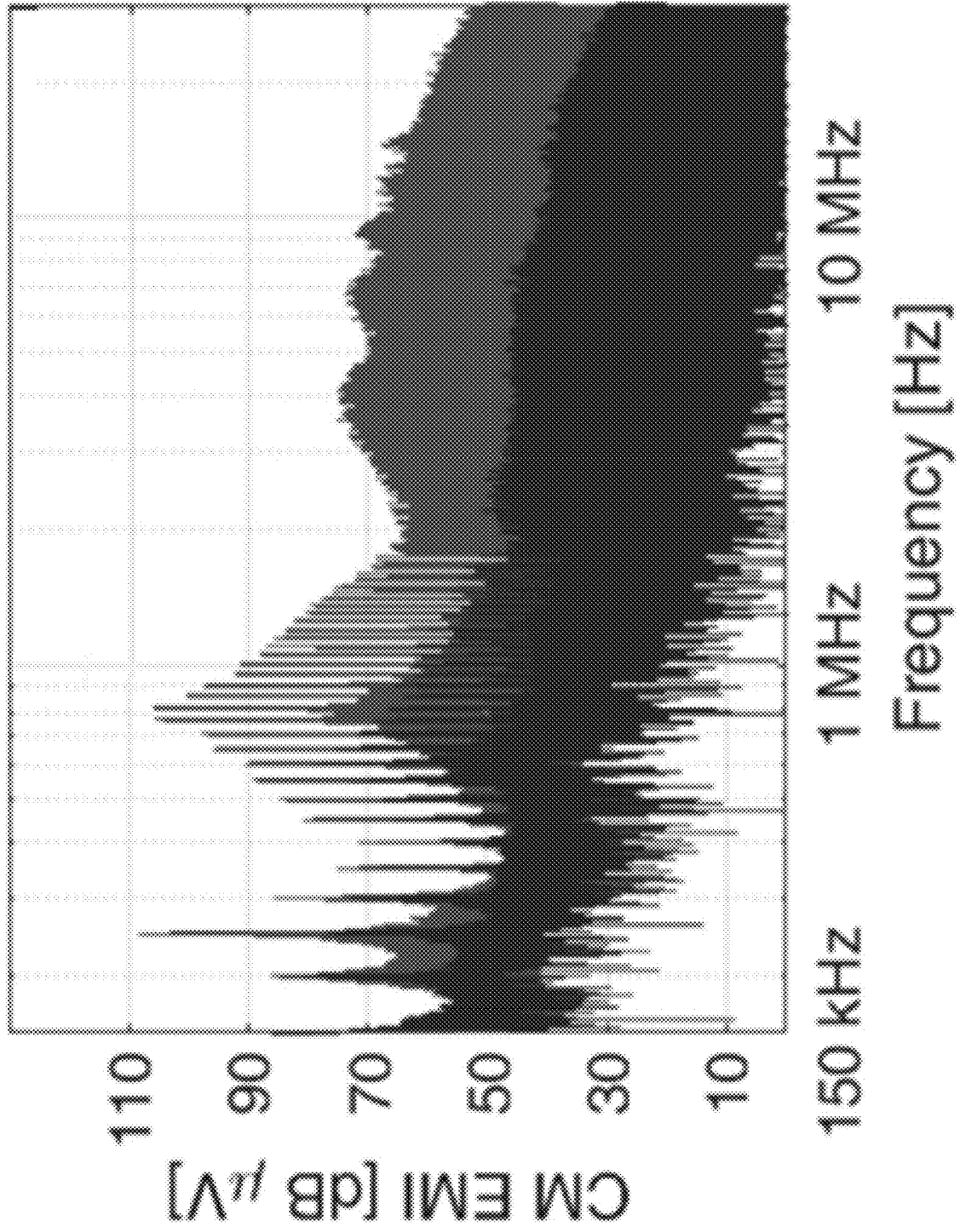


FIG. 11

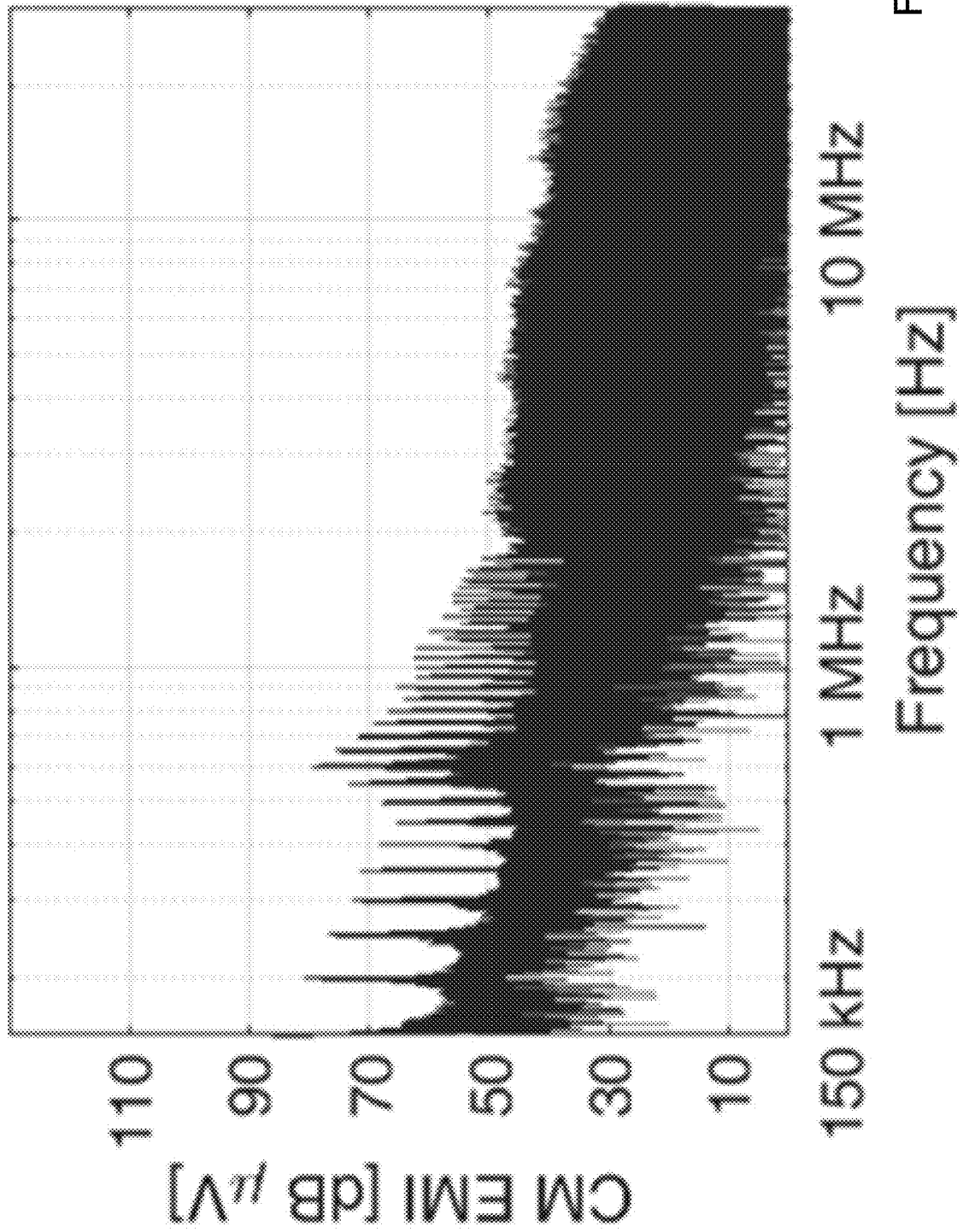


FIG. 12

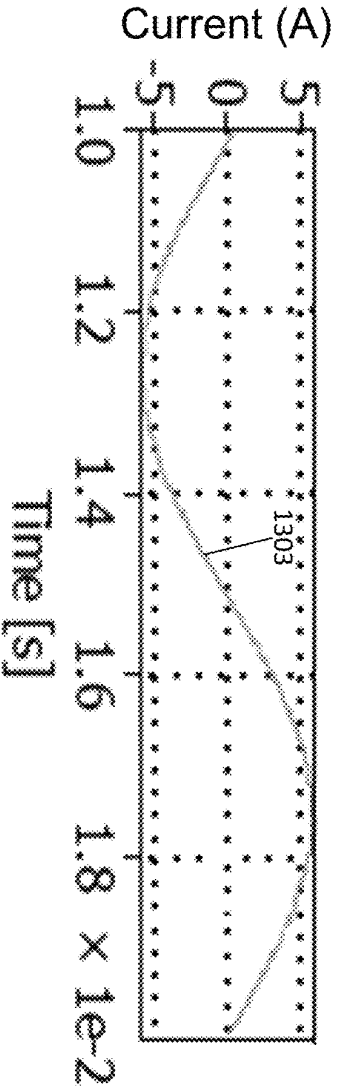
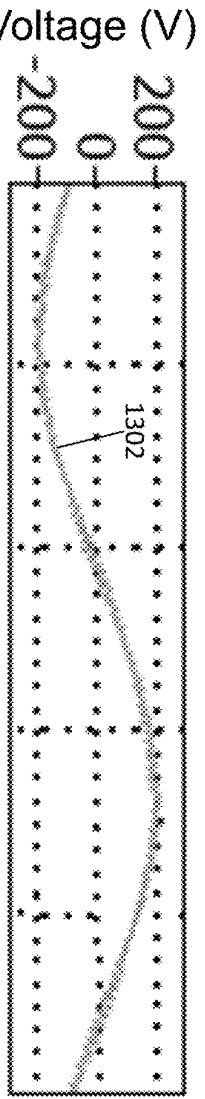
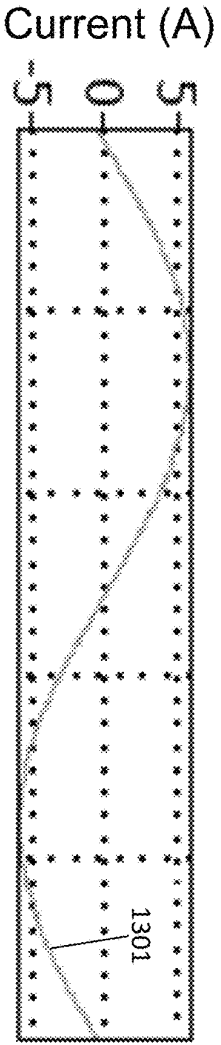
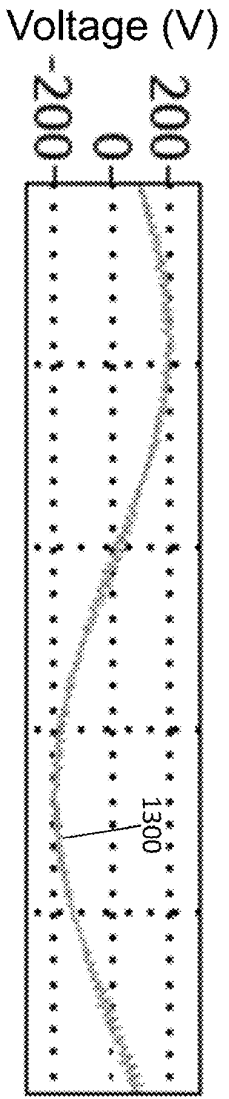


FIG. 13

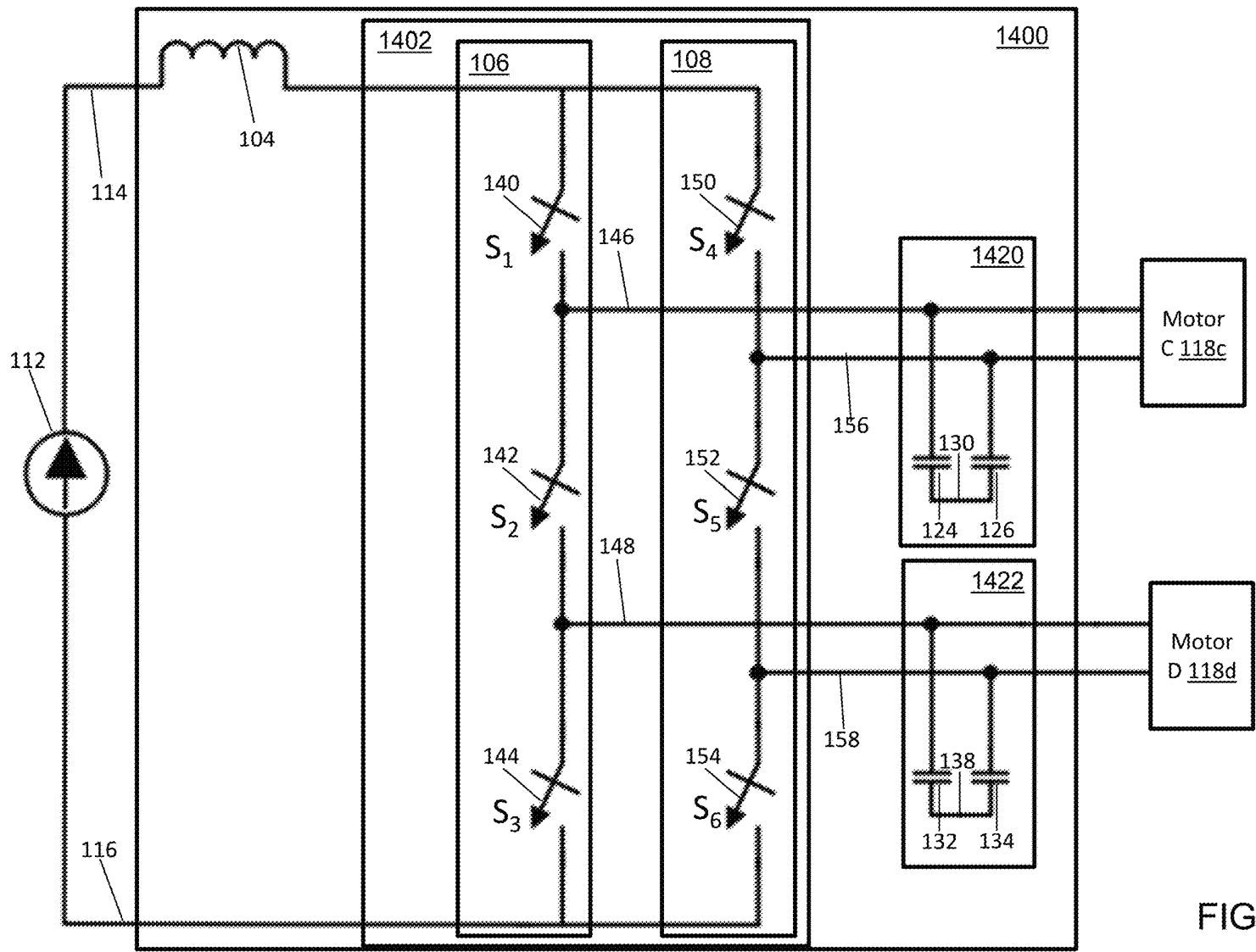


FIG. 14

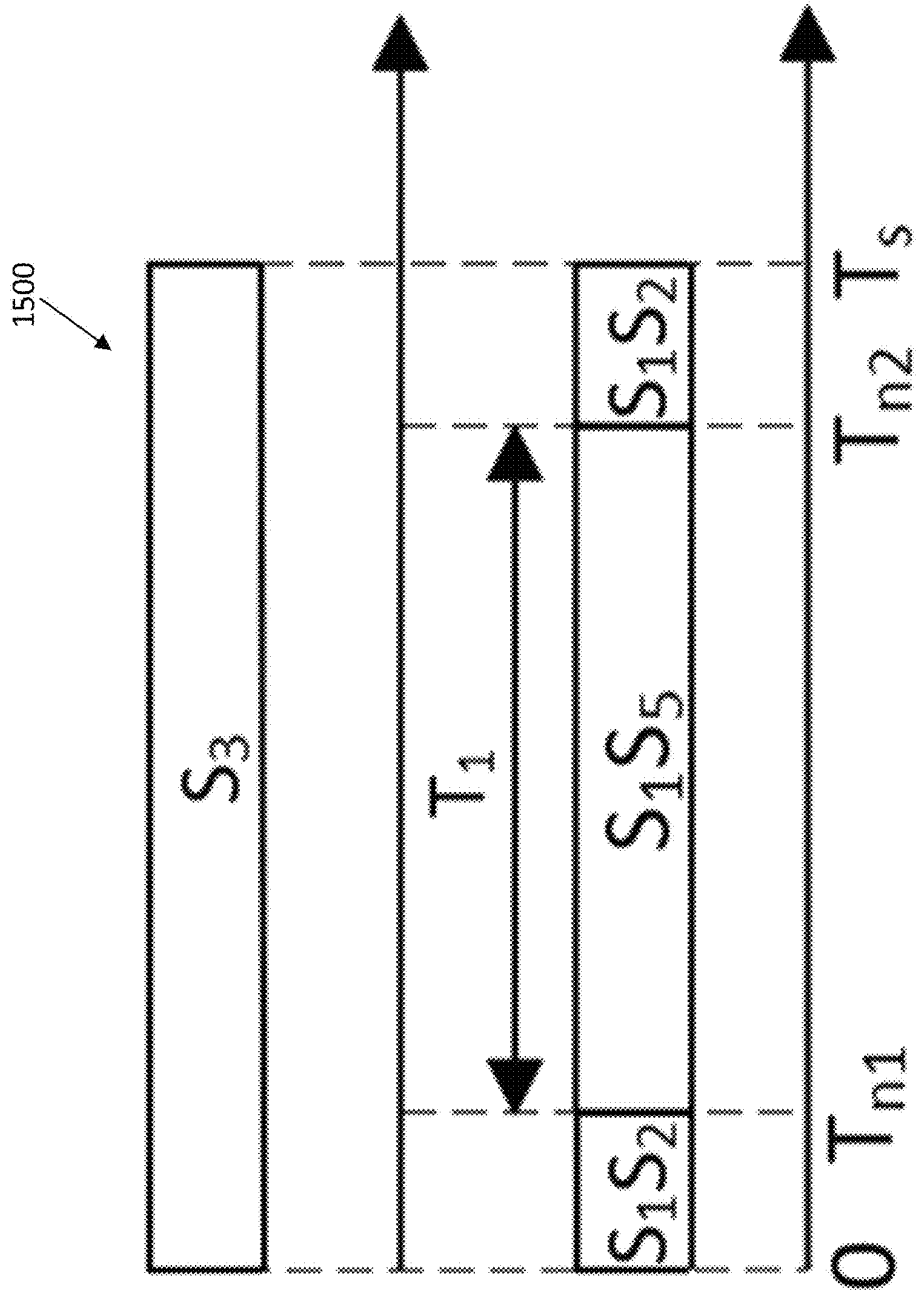


FIG. 15A

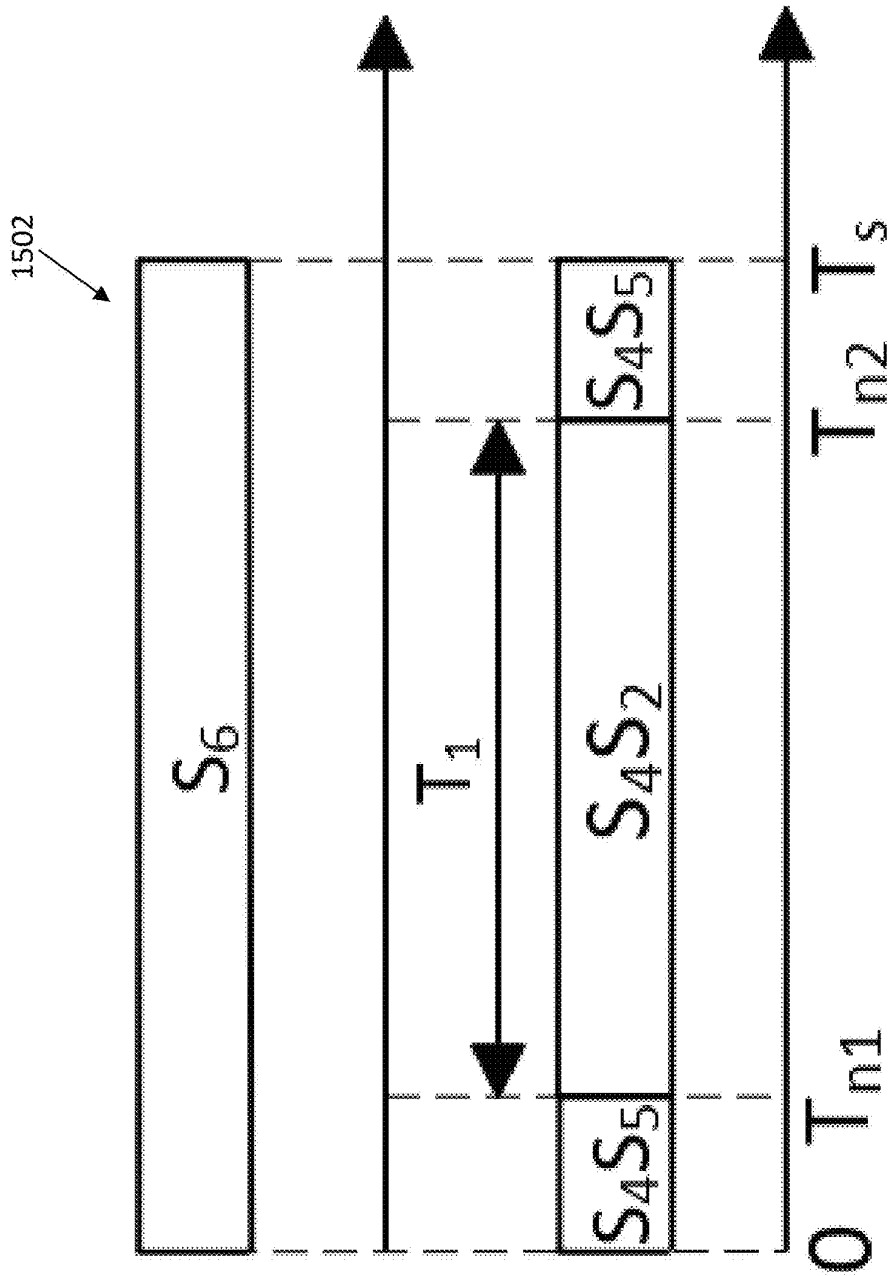


FIG. 15B

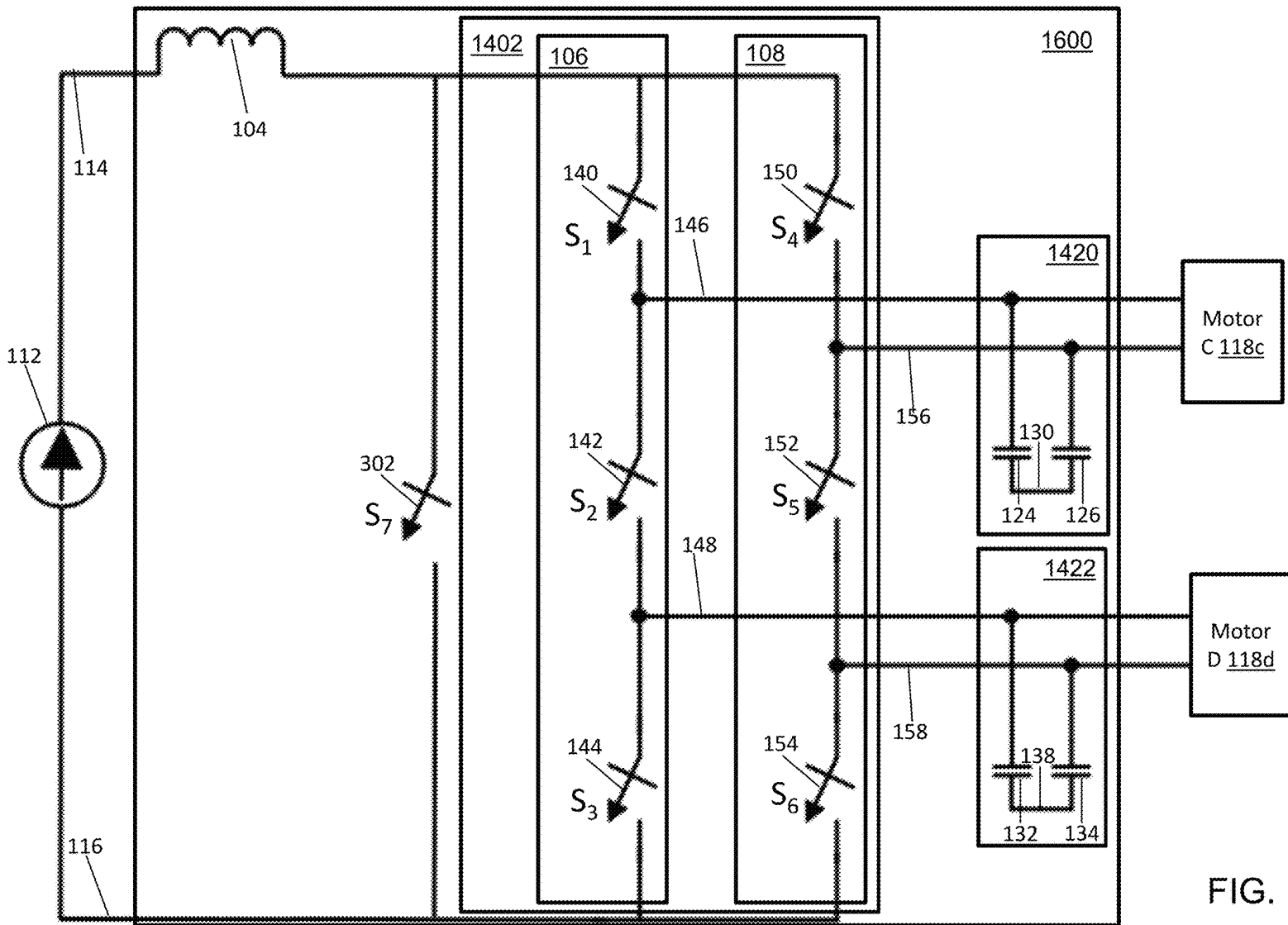


FIG. 16

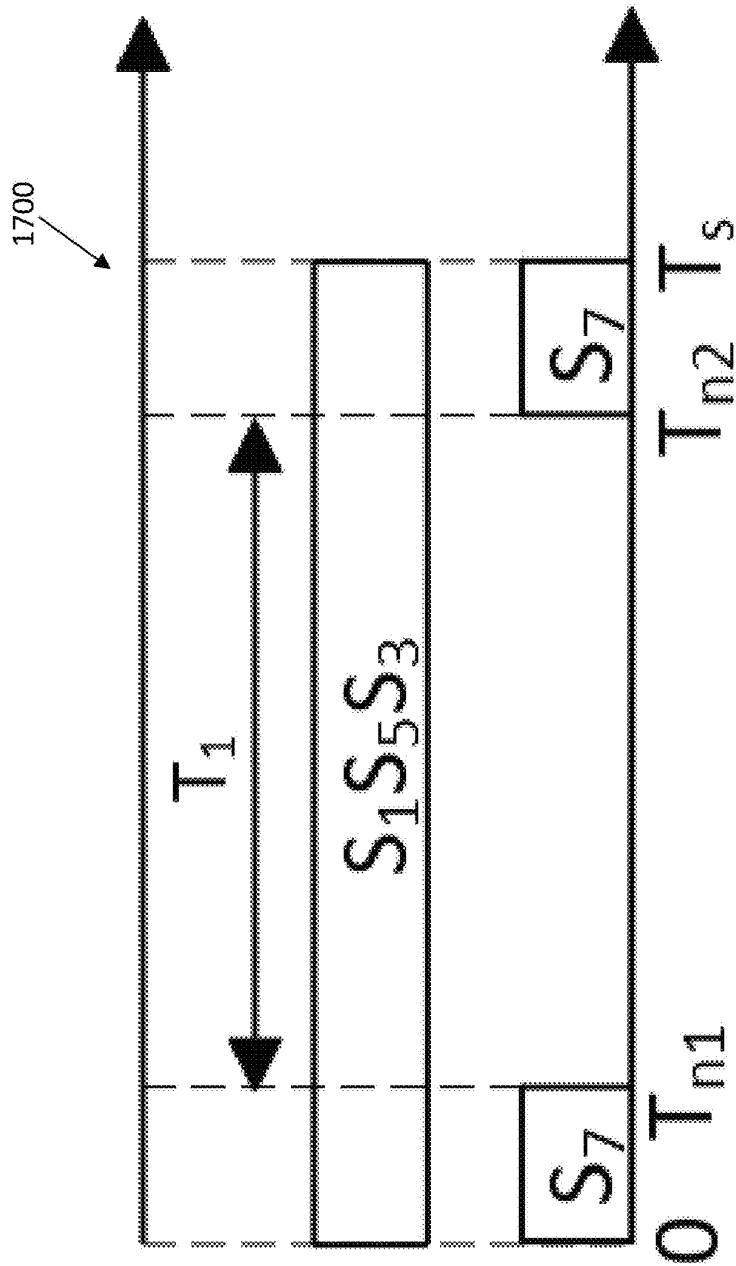


FIG. 17A

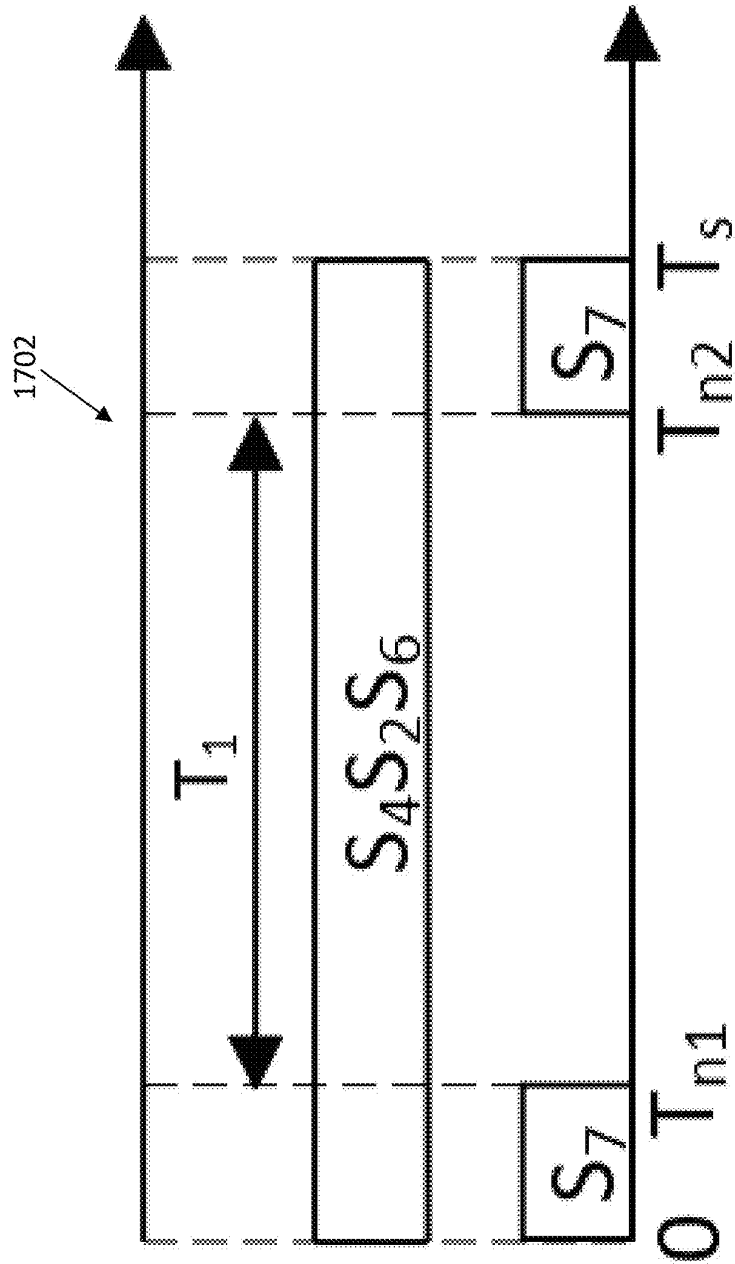


FIG. 17B

BALANCED CURRENT-SOURCE INVERTER

REFERENCE TO GOVERNMENT RIGHTS

This invention was made with government support under DE-AR0000893 awarded by the DOE/ARPA-E. The government has certain rights in the invention.

BACKGROUND

Current-source inverters (CSIs) using reverse-voltage-blocking (RB) switches were dominant in the early days of power electronics and are still used in some megawatt (MW)-level motor drive applications. Due to the latching characteristics of thyristors and low switching frequency capability of thyristor-based devices like gate turn-off thyristors, such CSI systems are usually very bulky. CSIs based on non-latching reverse-voltage-blocking (RB) devices can increase the CSI's switching frequency, but the high conduction loss of available silicon (Si)-based RB switches and their limited availability have prevented CSIs using RB switches from competing with voltage-source inverters (VSIs). The non-latching silicon switches developed since the 1980s including metal-oxide-semiconductor field-effect transistors (MOSFETs) and insulated-gate bipolar transistors (IGBTs) can switch at frequencies in the tens of kilohertz (kHz) and are naturally suitable for voltage-source inverter (VSI) topologies. However, the lack of RB capability in such devices usually requires them to be in series connection with a diode to achieve RB capability, which increases the CSI's conduction loss significantly compared to the VSI which can use the switch without the series diode.

Despite the VSIs' present dominance in commercial products, VSIs in motor drive applications result in a number of undesirable features including low reliability due to use of electrolytic direct current (DC)-link capacitors, detrimental common-mode electromagnetic interference (CM EMI), significant cable overvoltage, increased motor loss, etc. The sinusoidal output voltage and current waveforms and the use of DC-link inductors by CSIs can naturally overcome many of these VSI disadvantages at the same time.

The conventional H6-CSI topology, despite its lower CM EMI as compared to VSI, still requires external filters to suppress the EMI in order to comply with EMI standards.

SUMMARY

In an example embodiment, a switching circuit for a current source inverter is provided that includes, but is not limited to, a first inverter leg, a second inverter leg, and a controller. The first inverter leg includes a first reverse-voltage-blocking (RB) switch, a second RB switch, and a third RB switch that are connected in series between a first bus line and a second bus line. The second inverter leg includes a fourth RB switch, a fifth RB switch, and a sixth RB switch that are connected in series between the first bus line and the second bus line. The controller is configured to control a switch between an on-state and an off-state for each RB switch. When in the on-state, a reverse voltage is blocked by a respective RB switch, and a current with a positive polarity is conducted through the respective RB switch. When in the off-state, a voltage and the current are blocked by the respective RB switch.

In another example embodiment, a current source inverter is provided. The current source inverter includes, but is not limited to, an inductor, a filter, and the switching circuit connected between the inductor and the filter.

Other principal features of the disclosed subject matter will become apparent to those skilled in the art upon review of the following drawings, the detailed description, and the appended claims.

BRIEF DESCRIPTION OF THE DRAWINGS

The patent or application file contains at least one drawing executed in color. Copies of this patent or patent application publication with color drawing(s) will be provided by the Office upon request and payment of the necessary fee.

Illustrative embodiments of the disclosed subject matter will hereafter be described referring to the accompanying drawings, wherein like numerals denote like elements.

FIG. 1 is a circuit diagram of a balanced current source inverter in accordance with an illustrative embodiment.

FIG. 2 is a circuit diagram of a switch that can be included in the current source inverter of FIG. 1 in accordance with an illustrative embodiment.

FIG. 3 is a circuit diagram of a balanced current source inverter in accordance with another illustrative embodiment.

FIG. 4 is a block diagram of a power conversion system in accordance with an illustrative embodiment.

FIG. 5 depicts a flow diagram illustrating examples of operations performed by a controller of the current source inverter in accordance with an illustrative embodiment.

FIGS. 6A-6F are control signal time period snapshots for the current source inverter of FIG. 1 when providing power to an AC load in accordance with an illustrative embodiment.

FIGS. 7A-7F are control signal time period snapshots for the current source inverter of FIG. 3 when providing power to the AC load in accordance with an illustrative embodiment.

FIG. 8 shows a simulated efficiency comparison using the current source inverter of FIG. 1, the current source inverter of FIG. 3, and a conventional H6-CSI in accordance with an illustrative embodiment.

FIG. 9 shows a simulated common mode electro-magnetic interference (CM EMI) comparison between the current source inverter of FIG. 1 and the conventional H6-CSI in accordance with an illustrative embodiment.

FIG. 10 shows a simulated CM EMI comparison between the current source inverter of FIG. 1 with no delay between switching events and with 60 nanoseconds delay between switching events in accordance with an illustrative embodiment.

FIG. 11 shows a simulated CM EMI comparison between the current source inverter of FIG. 3 and the conventional H6-CSI in accordance with an illustrative embodiment.

FIG. 12 shows a simulated CM EMI comparison between the current source inverter of FIG. 3 with no delay between switching events and with 60 nanoseconds delay between switching events in accordance with an illustrative embodiment.

FIG. 13 shows a simulated voltage between two pairs of windings and a current in two different windings generated by the current source inverter of FIG. 3 in accordance with an illustrative embodiment.

FIG. 14 is a circuit diagram of a balanced current source inverter in accordance with another illustrative embodiment.

FIGS. 15A and 15B are control signal time period snapshots for the current source inverter of FIG. 14 when providing power to an AC load in accordance with an illustrative embodiment.

FIG. 16 is a circuit diagram of a balanced current source inverter in accordance with another illustrative embodiment.

FIGS. 17A and 17B are control signal time period snapshots for the current source inverter of FIG. 16 when providing power to the AC load in accordance with an illustrative embodiment.

DETAILED DESCRIPTION

Referring to FIG. 1, a first current source inverter (CSI) 100 is shown in accordance with an illustrative embodiment. First CSI 100 may include an inverter switching circuit 102, an inductor 104, a first capacitive filter 120, and a second capacitive filter 122. Inverter switching circuit 102 is connected between inductor 104 and both first capacitive filter 120 and second capacitive filter 122. First CSI 100 is connected between a direct current (DC) source 112 and an alternating current (AC) load 404 (shown referring to FIG. 4) such as a motor A 118a and a motor B 118b. First CSI 100 converts the DC current from DC source 112 to an AC voltage and current provided to AC load 404.

First CSI 100 is connected between a first bus line 114 and a second bus line 116. In the illustrative embodiment of FIG. 1, inductor 104 is connected on first bus line 114 in series between DC source 112 and switching circuit 102. Inductor 104 may be one or more inductors connected in series of various types with various inductance values. Though not shown, inductor 104 further may include one or more inductors connected in series between DC source 112 and switching circuit 102 on second bus line 116. As understood by a person of skill in the art, an inductor is a passive two-terminal electrical component that stores energy in a magnetic field when electric current flows through it. An inductance value for inductor 104 may be selected to carry a load current based on an application area of first CSI 100 as understood by a person of skill in the art. First bus line 114 and second bus line 116 provide connections to inverter switching circuit 102 from DC source 112 through inductor 104. Inverter switching circuit 102 is connected on a side of inductor 104 opposite the connection of inductor 104 with DC source 112.

Inverter switching circuit 102 may include a first inverter leg 106, a second inverter leg 108, and a third inverter leg 110. First capacitive filter 120 may include a first capacitor 124, a second capacitor 126, and a third capacitor 128, one capacitor for each phase of the AC voltage and current provided to, for example, motor A 118a. A capacitor of first capacitor 124, second capacitor 126, and third capacitor 128 is associated with each inverter leg of first inverter leg 106, second inverter leg 108, and third inverter leg 110, respectively.

Second capacitive filter 122 may include a fourth capacitor 132, a fifth capacitor 134, and a sixth capacitor 128, one capacitor for each phase of the AC voltage and current provided to, for example, motor B 118b. A capacitor of fourth capacitor 132, fifth capacitor 134, and sixth capacitor 128 is associated with each inverter leg of first inverter leg 106, second inverter leg 108, and third inverter leg 110, respectively.

First capacitor 124 is connected between a first, A phase line 146 of first inverter leg 106 and a first filter line 130. Fourth capacitor 132 is connected between a second, A phase line 148 of first inverter leg 106 and a second filter line 138. Second capacitor 126 is connected between a first, B phase line 156 of second inverter leg 108 and first filter line 130. Fifth capacitor 134 is connected between a second, B phase line 158 of second inverter leg 108 and second filter line 138. Third capacitor 128 is connected between a first, C phase line 166 of third inverter leg 110 and first filter line

130. Sixth capacitor 136 is connected between a second, C phase line 168 of third inverter leg 110 and second filter line 138.

Each capacitor of first capacitive filter 120 and of second capacitive filter 122 may be a capacitor of various types and with various ratings. As understood by a person of skill in the art, a capacitor is a passive two-terminal electrical component that stores electrical energy in an electric field and has an associated rated capacitance value. A rating of each capacitor of first capacitive filter 120 and of second capacitive filter 122 may be selected to carry inductive current from AC load 404 without requiring the switches of first inverter leg 106, second inverter leg 108, and third inverter leg 110 to provide a current flow-path. In alternative embodiments, other types of filters may be used based on AC load 404.

First inverter leg 106 may include a first switch 140, a second switch 142, and a third switch 144 connected in series between first bus line 114 and second bus line 116 opposite inductor 104 relative to DC source 112. Second inverter leg 108 may include a fourth switch 150, a fifth switch 152, and a sixth switch 154 connected in series between first bus line 114 and second bus line 116 opposite inductor 104 relative to DC source 112. Third inverter leg 110 may include a seventh switch 160, an eighth switch 162, and a ninth switch 164 connected in series between first bus line 114 and second bus line 116 opposite inductor 104 relative to DC source 112.

First, A phase line 146 is connected between first switch 140 and second switch 142 and to AC load 404, such as motor A 118a, through first capacitive filter 120. Second, A phase line 148 is connected between second switch 142 and third switch 144 and to AC load 404, such as motor B 118b, through second capacitive filter 122. First, B phase line 156 is connected between fourth switch 150 and fifth switch 152 and to AC load 404, such as motor A 118a, through first capacitive filter 120. Second, B phase line 158 is connected between fifth switch 152 and sixth switch 154 and to AC load 404, such as motor B 118b, through second capacitive filter 122. First, C phase line 166 is connected between seventh switch 160 and eighth switch 162 and to AC load 404, such as motor A 118a, through first capacitive filter 120. Second, C phase line 168 is connected between eighth switch 162 and ninth switch 164 and to AC load 404, such as motor B 118b, through second capacitive filter 122.

Each switch of first inverter leg 106, second inverter leg 108, and third inverter leg 110 is a reverse-voltage-blocking (RB) switch. Referring to FIG. 2, an RB switch 200 is shown in accordance with an illustrative embodiment. RB switch 200 is merely an illustrative RB switch that may be used. Alternative RB switches are described in H. Dai, T. M. Jahns, R. A. Torres, M. Liu, B. Sarlioglu, and S. Chang, "Development of High-Frequency WBG Power Modules with Reverse-Voltage-Blocking Capability for an Integrated Motor Drive using a Current-Source Inverter," 2018 IEEE Energy Convers. Congr. Expo, pp. 1808-1815, 2018; P. Wheeler and D. Grant, "Optimised input filter design and low-loss switching techniques for a practical matrix converter," IEE Proc.—Electr. Power Appl., vol. 144, no. 1, p. 53, 1997; and M. Hornkamp, M. Loddenkotter, M. Munzer, O. Simon, and M. Bruckmann, "ECONOMAC THE FIRST ALL-IN-ONE IGBT MODULE FOR MATRIX CONVERTERS," 2001, p. 640.

RB switch 200 may be a semiconductor switch formed of one or more of various types of semiconductors such as a MOSFET, a high electron mobility transistor (HEMT), etc. Referring to FIG. 2, RB switch 200 may include a transistor

202 and a diode 204. Transistor 202 may include a gate terminal 208, a source terminal 210, and a drain terminal 212. For illustration, transistor 202 may be an n-channel, enhancement mode silicon-carbide (SiC)-MOSFET. As understood by a person of skill in the art, the terminals of different types of semiconductor devices may be labeled differently based on the type of switch. For example, for a MOSFET or an HEMT, a first terminal, a second terminal, and a third terminal may be referred to as a drain, a gate, and a source, respectively. A voltage applied to the second terminal determines a switching state of the semiconductor device, as in an on-state or as in an off-state. In the off-state, there is little or no conduction between drain terminal 212 and source terminal 210. In the on-state, there is current flow from drain terminal 212 to source terminal 210.

Gate terminal 208 and source terminal 210 may be connected to a pulse width modulated (PWM) signal generator 206 of controller 402. Source terminal 210 may be connected to the anode of diode 204. Gate terminal 208 and source terminal 210 may be connected to switch together under control of PWM signal generator 206. RB switch 200 may be in an off-state when an off-state control signal is provided by PWM signal generator 206 of controller 402 to gate terminal 208. RB switch 200 may be in an on-state when an on-state control signal is provided by PWM signal generator 206 of controller 402 to gate terminal 208 and source terminal 210.

Diode 204 may be a diode of various types such as a p-n junction type, a Schottky barrier type, etc. with various ratings. As understood by a person of skill in the art, a diode is a two-terminal electrical component that conducts current primarily in one direction from an anode to a cathode. Diode 204 is connected in series to source terminal 210 of transistor 202 with the anode of diode 204 connected to receive current from transistor 202.

First CSI 100 converts an input DC current from DC source 112 on first bus line 114 to a three-phase current output signal with a first phase current signal output on first, A phase line 146 and on second, A phase line 148, with a second phase current signal output on first, B phase line 156 and on second, B phase line 158, and with a third phase current signal output on first, C phase line 166 and on second, C phase line 168. In an illustrative embodiment, the first phase current signal output on first, A phase line 146 is shifted 180 degrees relative to the first phase current signal output on second, A phase line 148; the second phase current signal output on first, B phase line 156 is shifted 180 degrees relative to the second phase current signal output on second, B phase line 158; and the third phase current signal output on first, C phase line 166 is shifted 180 degrees relative to the third phase current signal output on second, C phase line 168.

First capacitive filter 120 may be configured to reduce voltage spikes on a voltage output to the AC load 404, such as motor A 118a, by reducing a rate of rise and fall of the first phase current signal, the second phase current signal, and the third phase current signal on first, A phase line 146, first, B phase line 156, and first, C phase line 166, respectively. First, A phase line 146, first, B phase line 156, and first, C phase line 166 may be connected to provide the three-phase current output signal to AC load 404, such as motor A 118a.

Second capacitive filter 122 may be configured to reduce voltage spikes on a voltage output to the AC load 404, such as motor B 118b, by reducing a rate of rise and fall of the first phase current signal, the second phase current signal, and the third phase current signal on second, A phase line 148, second, B phase line 158, and second, C phase line 168,

respectively. Second, A phase line 148, second, B phase line 158, and second, C phase line 168 may be connected to provide the three-phase current output signal to AC load 404, such as motor B 118b.

Referring to FIG. 3, a second CSI 300 is shown in accordance with an illustrative embodiment. Second CSI 300 may include inverter switching circuit 102, a tenth RB switch 302, inductor 104, first capacitive filter 120, and second capacitive filter 122. Tenth RB switch 302 is connected between inductor 104 and inverter switching circuit 102 in parallel with inverter switching circuit 102 between first bus line 114 and second bus line 116. Tenth RB switch 302 is connected on a side of inductor 104 opposite the connection with DC source 112.

Referring to FIG. 4, a block diagram of a power conversion system 400 is shown in accordance with an illustrative embodiment. Power conversion system 400 may include controller 402, DC source 112, AC load 404, a sensor(s) 418, and one or more of first CSI 100, second CSI 300, a third CSI 1400 (shown referring to FIG. 14), or a fourth CSI 1600 (shown referring to FIG. 16). For example, DC source 112 may be a DC current source such as a battery, a solar panel, a current source rectifier, etc. Controller 402 may be electrically connected to DC source 112 and to AC load 404 to receive voltage, current, and/or power values used to define the parameters that control the energy transfer between DC source 112 and AC load 404 through first CSI 100, second CSI 300, third CSI 1400, or fourth CSI 1600. For brevity, hereafter CSI 100, 300 refers to either first CSI 100, second CSI 300, third CSI 1400, or fourth CSI 1600 as well as other CSI that support a greater or a fewer number of phases than shown in the illustrative embodiments.

Controller 402 is also electrically connected to CSI 100, 300 to receive a value of the DC-link current, for example, as well as to provide the gating signals, for example, to PWM signal generator 206 of each inverter leg switch as well as optionally to tenth switch 302 to control transmission of each on-state switching signal and each off-state switching signal. The voltage, current, and/or power values may be received for each switching frequency interval, also referred to herein as a switching period T_s , or may be received less frequently or more frequently depending on the dynamic needs of power conversion system 400.

Power conversion system 400 may include one or more sensors 418 of the same or different type to measure system characteristics to adjust energy transferred from DC source 112 to AC load 404. Sensor(s) 418 may measure a physical quantity in an environment to which the sensor is associated and generate a corresponding measurement datum that may be associated with a time that the measurement datum is generated. Illustrative sensors include a pressure sensor, a temperature sensor, a position or location sensor, a voltage sensor, a current sensor, a frequency sensor, a speed sensor, etc. that may be mounted to various components used as part of a system to which power conversion system 400 is providing and/or receiving power.

Controller 402 may include an input interface 406, an output interface 408, a computer-readable medium 410, a processor 412, a control application 414, and control data 416. Fewer, different, and additional components may be incorporated into controller 402. For example, controller 402 may include a communication interface (not shown). The communication interface provides an interface for receiving and transmitting data between devices using various protocols, transmission technologies, and media as understood by those skilled in the art. The communication

interface may support communication using various transmission media that may be wired and/or wireless.

Input interface **406** provides an interface for receiving information from a user or from other devices for entry into controller **402** as understood by those skilled in the art. For example, controller **402** may receive a signal from sensor(s) **418** continuously, periodically, when an event occurs, etc. through input interface **406**. Input interface **406** may further interface with various input technologies including, but not limited to, a keyboard, a mouse, a display, a track ball, a keypad, one or more buttons, etc. to allow the user to enter information into controller **402** or to make selections in a user interface displayed on the display. The same interface may support both input interface **406** and output interface **408**. Controller **402** may have one or more input interfaces that use the same or a different input interface technology. Inputs through input interface **406** may include the voltage, current, and/or power values received from DC source **112** and/or AC load **404**.

Output interface **408** provides an interface for outputting information for review by a user of controller **402** and for input to another device. For example, output interface **408** may interface with various output technologies including, but not limited to, a display. Controller **402** may have one or more output interfaces that use the same or a different interface technology. Additional outputs through output interface **408** from controller **402** may be the switching signals sent to one or more PWM signal generator **206** of each inverter leg switch and tenth switch **302**. For example, control application **414** may determine which switches of CSI **100, 300** are in an on-state and which are in an off-state. These signals may be provided to the switches of CSI **100, 300** through output interface **408** using a respective PWM signal generator **206**.

Computer-readable medium **410** is an electrical holding place or storage for information so the information can be accessed by processor **412** as understood by those skilled in the art. Computer-readable medium **410** can include, but is not limited to, any type of random access memory (RAM), any type of read only memory (ROM), any type of flash memory, etc. such as magnetic storage devices (e.g., hard disk, floppy disk, magnetic strips, . . .), optical disks (e.g., compact disc (CD), digital versatile disc (DVD), . . .), smart cards, flash memory devices, etc. Controller **402** may have one or more computer-readable media that use the same or a different memory media technology. For example, computer-readable medium **410** may include different types of computer-readable media that may be organized hierarchically to provide efficient access to the data stored therein as understood by a person of skill in the art. As an example, a cache may be implemented in a smaller, faster memory that stores copies of data from the most frequently/recently accessed main memory locations to reduce an access latency. Controller **402** also may have one or more drives that support the loading of a memory media such as a CD, DVD, an external hard drive, etc. One or more external hard drives further may be connected to controller **402** using the communication interface.

Processor **412** executes instructions as understood by those skilled in the art. The instructions may be carried out by a special purpose computer, logic circuits, or hardware circuits. Processor **412** may be implemented, for example, as a field programmable gate array. Processor **412** may be implemented in hardware and/or firmware. Processor **412** executes an instruction, meaning it performs/controls the operations called for by that instruction. The term "execution" is the process of running an application or the carrying

out of the operation called for by an instruction. The instructions may be written using one or more programming language, scripting language, assembly language, etc. Processor **412** operably couples with input interface **406**, with output interface **408**, and with computer-readable medium **410** to receive, to send, and to process information. Processor **412** may retrieve a set of instructions from a permanent memory device and copy the instructions in an executable form to a temporary memory device that is generally some form of RAM. Controller **402** may include a plurality of processors that use the same or a different processing technology.

Control application **414** performs operations associated with implementing some or all of the control of CSI **100, 300** possibly based on sensor measurements from sensor(s) **418** among other sensors included as part of DC source **112** and AC load **404**. The operations may be implemented using hardware, firmware, software, or any combination of these methods. Referring to the example embodiment of FIG. **4**, control application **414** is implemented in software (comprised of computer-readable and/or computer-executable instructions) stored in computer-readable medium **410** and accessible by processor **412** for execution of the instructions that embody the operations of control application **414**. Control application **414** may be written using one or more programming languages, assembly languages, scripting languages, etc.

Referring to FIG. **5**, example operations associated with control application **414** are described. Additional, fewer, or different operations may be performed depending on the embodiment of control application **414**. The order of presentation of the operations of FIG. **5** is not intended to be limiting. Some of the operations may not be performed in some embodiments. Although some of the operational flows are presented in sequence, the various operations may be performed simultaneously, for example, using multiple threads, in various repetitions and/or in other orders than those that are illustrated, for example, using interrupts.

Though not shown, control data **416** may be read into a RAM type of computer readable medium **410** by control application **414** when controller **402** is executing. For example, control data **416** may include various switching frequency timing parameters precomputed for control application **414** for power conversion system **400** as described further below.

In an operation **500**, a phase of AC load **404** may be received. A phase-locked-loop may be used to obtain a current three-phase voltage relationship at an output terminal from CSI **100, 300** to AC load **404**.

In operation **502**, an on-state or an off-state signal determination is made for each inverter leg switch of CSI **100, 300**.

In operation **504**, an on-state or an off-state signal determination is made for tenth RB switch **302** of CSI **300** if CSI **300** is used. Processing continues in operation **500** to continuously or periodically receive the phase and determine switch states for each inverter leg switch of CSI **100, 300** and for tenth RB switch **302** of CSI **300** if CSI **300** is used.

Referring to FIGS. **6A-6F**, control signal time period snapshots for the example of first CSI **100** are shown in accordance with an illustrative embodiment. The control signal time period snapshots shown referring to FIGS. **6A-6F** are used to determine whether each inverter leg switch is in the on-state or the off-state as described further below. Referring to FIGS. **7A-7F**, control signal time period snapshots for the example of second CSI **300** are shown in accordance with an illustrative embodiment. The control

signal time period snapshots shown referring to FIGS. 7A-7F are used to determine whether each inverter leg switch is in the on-state or the off-state and whether tenth RB switch 302 is in the on-state or the off-state as described further below.

To define the modulation of first CSI 100, for example, consider a three-phase balanced set of sinusoidal voltage waveforms desired at the output of first capacitive filter 120 and second capacitive filter 122 that is input to AC load 404. A first-phase output waveform (current, voltage, or power) that may include a first A-phase waveform created by operation of first inverter leg 106, is output on first, A phase line 146, and a second A-phase waveform created by operation of first inverter leg 106 is output on second, A phase line 148. The first A-phase waveform is 180 degrees out of phase relative to the second A-phase waveform. A second-phase output waveform (current, voltage, or power) that may include a first B-phase waveform created by operation of second inverter leg 108 is output on first, B phase line 156, and a second B-phase waveform created by operation of second inverter leg 108 is output on second, B phase line 158. The first B-phase waveform is 180 degrees out of phase relative to the second B-phase waveform. A third-phase output waveform (current, voltage, or power) that may include a first C-phase waveform created by operation of third inverter leg 110 is output on first, C phase line 166, and a second C-phase waveform created by operation of third inverter leg 110 is output on second, C phase line 168. The first C-phase waveform is 180 degrees out of phase relative to the second C-phase waveform. As understood by a person of skill in the art, the current and voltage waveforms are 360/m degrees out of phase with each other, where m represents a number of phases. Thus, a first A-phase voltage $V_{1,A}$, a first B-phase voltage $V_{1,B}$, and a first C-phase voltage $V_{1,C}$ are 120 degrees out of phase with each other; a first A-phase current $I_{1,A}$, a first B-phase current $I_{1,B}$, and a first C-phase current $I_{1,C}$ are 120 degrees out of phase with each other; a second A-phase voltage $V_{2,A}$, a second B-phase voltage $V_{2,B}$, and a second C-phase voltage $V_{2,C}$ are 120 degrees out of phase with each other; and a second A-phase current $I_{2,A}$, a second B-phase current $I_{2,B}$, and a second C-phase current $I_{2,C}$ are 120 degrees out of phase with each other. $V_{1,A}$, $V_{1,B}$, and $V_{1,C}$ and $V_{2,A}$, $V_{2,B}$, and $V_{2,C}$ are also 180 degrees out of phase with each other, respectively. $I_{1,A}$, $I_{1,B}$, and $I_{1,C}$ and also $I_{2,A}$, $I_{2,B}$, and $I_{2,C}$ are 180 degrees out of phase with each other, respectively.

A time interval of one period of the three-phase output waveforms can be divided into six sectors, depending on which of the phase voltages is the most positive and which of the phase voltages is the most negative. For example, in sector I, $V_{1,A}$ is the most positive and $V_{1,B}$ is the most negative; in sector II, $V_{1,A}$ is the most positive and $V_{1,C}$ is the most negative; in sector III, $V_{1,B}$ is the most positive and $V_{1,C}$ is the most negative; in sector IV, $V_{1,B}$ is the most positive and $V_{1,A}$ is the most negative; in sector V, $V_{1,C}$ is the most positive and $V_{1,A}$ is the most negative; and in sector VI, $V_{1,C}$ is the most positive and $V_{1,B}$ is the most negative. CSI 100, 300 remains in a sector for $\frac{1}{6}$ of a fundamental period. For example, a fundamental period may be $\frac{1}{60}$ for a 60 Hertz fundamental frequency. Once CSI 100, 300 completes one fundamental period, CSI 100, 300 returns to the first sector.

Control application 414 implements a control algorithm that operates first CSI 100 from sector I to sector VI as summarized in FIGS. 6A-6F respectively, and back to sector I in a continuous loop to continually respond to DC source 112 and/or AC load 404. FIG. 6A represents sector I. FIG. 6B represents sector II. FIG. 6C represents sector III. FIG.

6D represents sector IV. FIG. 6E represents sector V. FIG. 6F represents sector VI. Of course, when first CSI 100 implements a fewer or a greater number of phase currents, there are a fewer or a greater number of sectors. For example, first CSI 100 with a single phase has two sectors, and first CSI 100 with four phases has fourteen sectors though implemented in a similar manner.

Referring to FIGS. 6A-6F, S_1 indicates the on-state for first switch 140, S_2 indicates the on-state for eighth switch 162, S_3 indicates the on-state for fourth switch 150, S_4 indicates the on-state for second switch 142, S_5 indicates the on-state for seventh switch 160, S_6 indicates the on-state for fifth switch 152, S_7 indicates the on-state for third switch 144, S_8 indicates the on-state for sixth switch 154, and S_9 indicates the on-state for ninth switch 164.

The pulses indicate when the respective RB switches are turned on. The non-designated switches in each sector are in the off-state unless shown in a pulse. For example, " S_1S_4 " indicates that the respective pair of switches that includes first switch 140 and second switch 142 are in the on-state based on an on-state control signal provided by the respective PWM signal generator 206 connected to first switch 140 and second switch 142. As another example, " S_1S_6 " indicates that the respective pair of switches that includes first switch 140 and fifth switch 152 are in the on-state based on an on-state control signal provided by the respective PWM signal generator 206 connected to first switch 140 and fifth switch 152. As yet another example, " S_7 " indicates that third switch 144 is in the on-state based on an on-state control signal provided by the respective PWM signal generator 206 connected to third switch 144. Though not shown, all of the on-state signals of first CSI 100 pass through a turn-off delay logic to implement an overlap time as understood by a person of skill in the art.

Referring to FIG. 6A, a sector I pulse sequence 600 is shown in accordance with an illustrative embodiment. Third switch 144 is in the on-state from a start of the switching interval indicated as "0" to an end of the switching period designated as T_s to show a single switching period. First switch 140 and second switch 142 are in the on-state from the start of the switching interval to a time designated as T_{n1} ; first switch 140 and fifth switch 152 are in the on-state from the time designated as T_{n1} to a time designated as T_{n2} ; first switch 140 and second switch 142 are in the on-state from the time designated as T_{n2} to a time designated as T_{n3} ; first switch 140 and eighth switch 162 are in the on-state from the time designated as T_{n3} to a time designated as T_{n4} ; first switch 140 and second switch 142 are in the on-state from the time designated as T_{n4} to a time designated as T_{n5} ; and first switch 140 and fifth switch 152 are in the on-state from the time designated as T_{n5} to a time designated as T_{n6} ; first switch 140 and second switch 142 are in the on-state from the time designated as T_{n6} to the end of the switching period.

The time values can be determined based on known time values for a conventional CSI using six switches (H6-CSI), for example, as described in B. Wu, High-Power Converters and AC Drives, Ch. 10, pp. 189-218, Wiley, 2006. T_s is the inverter switching period, and f_s is a switching frequency, where

$$T_s = \frac{1}{f_s} \cdot I_{ref}$$

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is a desired inverter output current waveform peak value, I_d is an inverter DC-link current value, and m_a is a modulation index that ranges from 0 to 1, where

$$m_a = \frac{I_{ref}}{I_d}.$$

T_1 is the H6-CSI space vector S_1S_6 's dwell time in one T_s without considering overlap time, and θ is an angle of the space vector, where

$$T_1 = m_a T_s \sin\left(\frac{\pi}{6} - \theta\right).$$

T_2 is the H6-CSI space vector S_1S_2 's dwell time in one T_s without considering overlap time, where

$$T_2 = m_a T_s \sin\left(\frac{\pi}{6} + \theta\right).$$

T_0 is the H6-CSI space vector zero state's dwell time in one T_s without considering overlap time, where $T_0 = T_s - T_1 - T_2$. Using these values,

$$T_a = \frac{T_1}{2} + \frac{3}{8}T_0, T_b = T_a + T_2 + \frac{1}{4}T_0, T_{n1} = \frac{T_0}{4}, T_{n2} = T_a - \frac{T_0}{8},$$

$$T_{n3} = T_a + \frac{T_0}{8}, T_{n4} = T_b - \frac{T_0}{8}, T_{n5} = T_b + \frac{T_0}{8}, \text{ and } T_{n6} = T_s - \frac{T_0}{4}.$$

Referring to FIG. 6B, a sector II pulse sequence **602** is shown in accordance with an illustrative embodiment. Ninth switch **164** is in the on-state from the start of the switching interval to the time designated as T_{n1} . Third switch **144** is in the on-state from the time designated as T_{n1} to the time designated as T_{n2} . Ninth switch **164** is in the on-state from the time designated as T_{n2} to the time designated as T_{n3} . Sixth switch **154** is in the on-state from the time designated as T_{n3} to the time designated as T_{n4} . Ninth switch **164** is in the on-state from the time designated as T_{n4} to the time designated as T_{n5} . Third switch **144** is in the on-state from the time designated as T_{n5} to the time designated as T_{n6} . Ninth switch **164** is in the on-state from the time designated as T_{n6} to the end of the switching period.

Eighth switch **162** and seventh switch **160** are in the on-state from the start of the switching interval to a time designated as T_{n1} ; first switch **140** and eighth switch **162** are in the on-state from the time designated as T_{n1} to a time designated as T_{n2} ; eighth switch **162** and seventh switch **160** are in the on-state from the time designated as T_{n2} to a time designated as T_{n3} ; eighth switch **162** and fourth switch **150** are in the on-state from the time designated as T_{n3} to a time designated as T_{n4} ; eighth switch **162** and seventh switch **160** are in the on-state from the time designated as T_{n4} to a time designated as T_{n5} ; first switch **140** and eighth switch **162** are in the on-state from the time designated as T_{n5} to a time designated as T_{n6} ; and eighth switch **162** and seventh switch **160** are in the on-state from the time designated as T_{n6} to the end of the switching period.

Referring to FIG. 6C, a sector III pulse sequence **604** is shown in accordance with an illustrative embodiment. Sixth switch **154** is in the on-state from the start of the switching interval to the end of the switching period. First switch **140**

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and second switch **142** are in the on-state from the start of the switching interval to a time designated as T_{n1} ; fourth switch **150** and second switch **142** are in the on-state from the time designated as T_{n1} to a time designated as T_{n2} ; first switch **140** and second switch **142** are in the on-state from the time designated as T_{n2} to a time designated as T_{n3} ; second switch **142** and seventh switch **160** are in the on-state from the time designated as T_{n3} to a time designated as T_{n4} ; first switch **140** and second switch **142** are in the on-state from the time designated as T_{n4} to a time designated as T_{n5} ; and fourth switch **150** and second switch **142** are in the on-state from the time designated as T_{n5} to a time designated as T_{n6} ; first switch **140** and second switch **142** are in the on-state from the time designated as T_{n6} to the end of the switching period.

Referring to FIG. 6D, a sector IV pulse sequence **606** is shown in accordance with an illustrative embodiment. Third switch **144** is in the on-state from the start of the switching interval to the time designated as T_{n1} . Sixth switch **154** is in the on-state from the time designated as T_{n1} to the time designated as T_{n2} . Third switch **144** is in the on-state from the time designated as T_{n2} to the time designated as T_{n3} . Ninth switch **164** is in the on-state from the time designated as T_{n3} to the time designated as T_{n4} . Third switch **144** is in the on-state from the time designated as T_{n4} to the time designated as T_{n5} . Sixth switch **154** is in the on-state from the time designated as T_{n5} to the time designated as T_{n6} . Third switch **144** is in the on-state from the time designated as T_{n6} to the end of the switching period.

First switch **140** and second switch **142** are in the on-state from the start of the switching interval to a time designated as T_{n1} ; fourth switch **150** and second switch **142** are in the on-state from the time designated as T_{n1} to a time designated as T_{n2} ; first switch **140** and second switch **142** are in the on-state from the time designated as T_{n2} to a time designated as T_{n3} ; second switch **142** and seventh switch **160** are in the on-state from the time designated as T_{n3} to a time designated as T_{n4} ; first switch **140** and second switch **142** are in the on-state from the time designated as T_{n4} to a time designated as T_{n5} ; fourth switch **150** and second switch **142** are in the on-state from the time designated as T_{n5} to a time designated as T_{n6} ; and first switch **140** and second switch **142** are in the on-state from the time designated as T_{n6} to the end of the switching period.

Referring to FIG. 6E, a sector V pulse sequence **608** is shown in accordance with an illustrative embodiment. Ninth switch **164** is in the on-state from the start of the switching interval to the end of the switching period. Eighth switch **162** and seventh switch **160** are in the on-state from the start of the switching interval to a time designated as T_{n1} ; second switch **142** and seventh switch **160** are in the on-state from the time designated as T_{n1} to a time designated as T_{n2} ; eighth switch **162** and seventh switch **160** are in the on-state from the time designated as T_{n2} to a time designated as T_{n3} ; seventh switch **160** and fifth switch **152** are in the on-state from the time designated as T_{n3} to a time designated as T_{n4} ; eighth switch **162** and seventh switch **160** are in the on-state from the time designated as T_{n4} to a time designated as T_{n5} ; and second switch **142** and seventh switch **160** are in the on-state from the time designated as T_{n5} to a time designated as T_{n6} ; eighth switch **162** and seventh switch **160** are in the on-state from the time designated as T_{n6} to the end of the switching period.

Referring to FIG. 6F, a sector VI pulse sequence **610** is shown in accordance with an illustrative embodiment. Sixth switch **154** is in the on-state from the start of the switching interval to the time designated as T_{n1} . Ninth switch **164** is in

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the on-state from the time designated as T_{n1} to the time designated as T_{n2} . Sixth switch **154** is in the on-state from the time designated as T_{n2} to the time designated as T_{n3} . Third switch **144** is in the on-state from the time designated as T_{n3} to the time designated as T_{n4} . Sixth switch **154** is in the on-state from the time designated as T_{n4} to the time designated as T_{n5} . Ninth switch **164** is in the on-state from the time designated as T_{n5} to the time designated as T_{n6} . Sixth switch **154** is in the on-state from the time designated as T_{n6} to the end of the switching period.

Fourth switch **150** and fifth switch **152** are in the on-state from the start of the switching interval to a time designated as T_{n1} ; seventh switch **160** and fifth switch **152** are in the on-state from the time designated as T_{n1} to a time designated as T_{n2} ; fourth switch **150** and fifth switch **152** are in the on-state from the time designated as T_{n2} to a time designated as T_{n3} ; first switch **140** and fifth switch **152** are in the on-state from the time designated as T_{n3} to a time designated as T_{n4} ; fourth switch **150** and fifth switch **152** are in the on-state from the time designated as T_{n4} to a time designated as T_{n5} ; seventh switch **160** and fifth switch **152** are in the on-state from the time designated as T_{n5} to a time designated as T_{n6} ; and fourth switch **150** and fifth switch **152** are in the on-state from the time designated as T_{n6} to the end of the switching period.

In the sector I to sector VI pulse sequences summarized in FIGS. 6A-6F, each RB switch of a single inverter leg of first inverter leg **106**, second inverter leg **108**, and third inverter leg **110** is controlled to enter the on-state for the time period

$$\frac{T_0}{4}$$

before and after a transition from the on-state to the off-state of a pair of RB switches selected from different inverter legs of first inverter leg **106**, second inverter leg **108**, and third inverter leg **110** with third RB switch **144**, sixth RB switch **154**, or ninth RB switch **164** selected from a common inverter leg of one RB switch of the pair of RB switches. For example, referring again to FIG. 6A, first switch **140**, second switch **142**, and third switch **144** are in the on-state from the time designated as T_{n2} to the time designated as T_{n3} , where

$$T_{n3} - T_{n2} = \frac{T_0}{4},$$

after fifth switch **152** transition from the on-state to the off-state. First switch **140** and fifth switch **152** are in first inverter leg **106** and second inverter leg **108**, respectively, and third RB switch **144** is in first inverter leg **106**.

For example, referring again to FIG. 6B, seventh switch **160**, eighth switch **162**, and ninth switch **164** are in the on-state from the time designated as T_{n2} to the time designated as T_{n3} , where

$$T_{n3} - T_{n2} = \frac{T_0}{4},$$

after eighth switch **162** transition from the on-state to the off-state. First switch **140** and eighth switch **162** are in first inverter leg **106** and third inverter leg **110**, respectively, and ninth switch **164** is in third inverter leg **110**.

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To summarize, there are four acceptable switching states (A, B, C, and D) for any of first inverter leg **106**, second inverter leg **108**, and third inverter leg **110**:

Switching state A: upper and lower switches are on, and the middle switch is off. For first inverter leg **106**, S_1 and S_7 are on, S_4 is off; for second inverter leg **108**, S_3 and S_8 are on, S_6 is off; and for third inverter leg **110**, S_5 and S_9 are on, S_2 is off.

Switching state B: upper and lower switches are off, and the middle switch is on. For first inverter leg **106**, S_1 and S_7 are off, S_4 is on; for second inverter leg **108**, S_3 and S_8 are off, S_6 is on; and for third inverter leg **110**, S_5 and S_9 are off, S_2 is on.

Switching state C: all three switches are off. For first inverter leg **106**, S_1 , S_4 , and S_7 are off; for second inverter leg **108**, S_3 , S_6 , and S_8 are off; and for third inverter leg **110**, S_5 , S_2 , and S_9 are off.

Switching state D: all three switches are on. For first inverter leg **106**, S_1 , S_4 , and S_7 are on; for second inverter leg **108**, S_3 , S_6 , and S_8 are on; and for third inverter leg **110**, S_5 , S_2 , and S_9 are on.

If none of the three phase legs is in switching state D, one of the three phase legs must be in switching state A, one of the phase legs must be in switching state B, and one of the phase legs must be in switching state C. Acceptable combinations are shown in Table I below.

TABLE I

First inverter leg 106	Second inverter leg 108	Third inverter leg 110
A	B	C
A	C	B
B	A	C
B	C	A
C	A	B
C	B	A

If one of the three phase legs is in switching state D, then the two other phase legs must be in switching state C. For all the switching states, during the transition process, a turn-off delay is implemented to guarantee a continuous current path for the dc-link inductor, inductor **104**.

Similar to FIGS. 6A-6F, referring to FIGS. 7A-7F, show the sector pulse sequence for second CSI **300**. Referring to FIG. 7A, a sector I pulse sequence **700** is shown in accordance with an illustrative embodiment. Third switch **144** is in the on-state from the start of the switching interval indicated as "0" to an end of the switching period designated as T_s to show a single switching period. Tenth switch **302** is in the on-state from the start of the switching interval to the time designated as T_{n1} , from the time designated as T_{n2} to a time designated as T_{n3} , from the time designated as T_{n4} to the time designated as T_n , and from the time designated as T_{n6} to the end of the switching period. First switch **140** and fifth switch **152** are in the on-state from the start of the switching interval to a time designated as T_a ; first switch **140** and eighth switch **162** are in the on-state from the time designated as T_a to a time designated as T_b ; and first switch **140** and fifth switch **152** are in the on-state from the time designated as T_b to the end of the switching period.

Referring to FIG. 7B, a sector II pulse sequence **702** is shown in accordance with an illustrative embodiment. Third switch **144** is in the on-state from the start of the switching interval to a time designated as T_a ; sixth switch **154** is in the on-state from the time designated as T_a to a time designated as T_b ; and third switch **144** is in the on-state from the time

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designated as T_b to the end of the switching period. Tenth switch **302** is in the on-state from the start of the switching interval to the time designated as T_{n1} , from the time designated as T_{n2} to a time designated as T_{n3} , from the time designated as T_{n4} to the time designated as T_{n5} , and from the time designated as T_{n6} to the end of the switching period. First switch **140** and eighth switch **162** are in the on-state from the start of the switching interval to a time designated as T_a ; eighth switch **162** and fourth switch **150** are in the on-state from the time designated as T_a to a time designated as T_b ; and first switch **140** and eighth switch **162** are in the on-state from the time designated as T_b to the end of the switching period.

Referring to FIG. 7C, a sector III pulse sequence **704** is shown in accordance with an illustrative embodiment. Sixth switch **154** is in the on-state from the start of the switching interval indicated as "0" to an end of the switching period designated as T_s to show a single switching period. Tenth switch **302** is in the on-state from the start of the switching interval to the time designated as T_{n1} , from the time designated as T_{n2} to a time designated as T_{n3} , from the time designated as T_{n4} to the time designated as T_{n5} , and from the time designated as T_{n6} to the end of the switching period. Eighth switch **162** and fourth switch **150** are in the on-state from the start of the switching interval to a time designated as T_a ; fourth switch **150** and second switch **142** are in the on-state from the time designated as T_a to a time designated as T_b ; and eighth switch **162** and fourth switch **150** are in the on-state from the time designated as T_b to the end of the switching period.

Referring to FIG. 7D, a sector IV pulse sequence **706** is shown in accordance with an illustrative embodiment. Sixth switch **154** is in the on-state from the start of the switching interval to a time designated as T_a ; ninth switch **164** is in the on-state from the time designated as T_a to a time designated as T_b ; and sixth switch **154** is in the on-state from the time designated as T_b to the end of the switching period. Tenth switch **302** is in the on-state from the start of the switching interval to the time designated as T_{n1} , from the time designated as T_{n2} to a time designated as T_{n3} , from the time designated as T_{n4} to the time designated as T_{n5} , and from the time designated as T_{n6} to the end of the switching period. Fourth switch **150** and second switch **142** are in the on-state from the start of the switching interval to a time designated as T_a ; second switch **142** and seventh switch **160** are in the on-state from the time designated as T_a to a time designated as T_b ; and fourth switch **150** and second switch **142** are in the on-state from the time designated as T_b to the end of the switching period.

Referring to FIG. 7E, a sector V pulse sequence **708** is shown in accordance with an illustrative embodiment. Ninth switch **164** is in the on-state from the start of the switching interval indicated as "0" to an end of the switching period designated as T_s to show a single switching period. Tenth switch **302** is in the on-state from the start of the switching interval to the time designated as T_{n1} , from the time designated as T_{n2} to a time designated as T_{n3} , from the time designated as T_{n4} to the time designated as T_{n5} , and from the time designated as T_{n6} to the end of the switching period. Second switch **162** and seventh switch **160** are in the on-state from the start of the switching interval to a time designated as T_a ; seventh switch **160** and fifth switch **152** are in the on-state from the time designated as T_a to a time designated as T_b ; and second switch **162** and seventh switch **160** are in the on-state from the time designated as T_b to the end of the switching period.

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Referring to FIG. 7F, a sector VI pulse sequence **710** is shown in accordance with an illustrative embodiment. Ninth switch **164** is in the on-state from the start of the switching interval to a time designated as T_a ; third switch **144** is in the on-state from the time designated as T_a to a time designated as T_b ; and ninth switch **164** is in the on-state from the time designated as T_b to the end of the switching period. Tenth switch **302** is in the on-state from the start of the switching interval to the time designated as T_{n1} , from the time designated as T_{n2} to a time designated as T_{n3} , from the time designated as T_{n4} to the time designated as T_{n5} , and from the time designated as T_{n6} to the end of the switching period. Seventh switch **160** and fifth switch **152** are in the on-state from the start of the switching interval to a time designated as T_a ; first switch **140** and fifth switch **152** are in the on-state from the time designated as T_a to a time designated as T_b ; and seventh switch **160** and fifth switch **152** are in the on-state from the time designated as T_b to the end of the switching period.

Having tenth switch **302** controlled to enter the on-state for the time period

$$\frac{T_0}{4}$$

before and after a transition from the on-state to the off-state of a pair of RB switches provides zero current switching for first inverter leg **106**, second inverter leg **108**, and third inverter leg **110**. One of first switch **140**, fourth switch **150**, or seventh switch **160** is controlled to enter the on-state for the time period

$$\frac{T_1}{2} + \frac{3T_0}{8}$$

at the start and the end of the switching period. One of second switch **142**, fifth switch **152**, or eighth switch **162** is also controlled to enter the on-state for the time period

$$\frac{T_1}{2} + \frac{3T_0}{8}$$

at the start and the end of the switching period. One of third switch **144**, sixth switch **154**, or ninth switch **164** is also controlled to enter the on-state for the time period

$$\frac{T_1}{2} + \frac{3T_0}{8}$$

at the start and the end of the switching period. One of first switch **140**, fourth switch **150**, or seventh switch **160** is controlled to enter the on-state for the time period

$$T_b - T_a = T_2 + \frac{T_0}{4}$$

One of second switch **142**, fifth switch **152**, or eighth switch **162** is also controlled to enter the on-state for the time period

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$$T_b - T_a = T_2 + \frac{T_0}{4}.$$

One of third switch **144**, sixth switch **154**, or ninth switch **164** is also controlled to enter the on-state for the time period

$$T_b - T_a = T_2 + \frac{T_0}{4}.$$

To summarize, there are three acceptable switching states (A, B, and C) for first inverter leg **106**, second inverter leg **108**, and third inverter leg **110**. The acceptable combinations are shown in Table I above.

Irrespective of whether tenth switch **302** is in the on-state or the off-state, one of first inverter leg **106**, second inverter leg **108**, and third inverter leg **110** is in switching state A, one of first inverter leg **106**, second inverter leg **108**, and third inverter leg **110** is in switching state B, and one of first inverter leg **106**, second inverter leg **108**, and third inverter leg **110** is in switching state C. Tenth switch **302** can be in its on-state or off-state at any time instant. The switching condition of tenth switch **302** does not depend on the switching states of first inverter leg **106**, second inverter leg **108**, and third inverter leg **110**. However, any change in the switching state of any of first inverter leg **106**, second inverter leg **108**, and third inverter leg **110** occurs only when tenth switch **302** is in its on-state.

Referring to FIG. **8**, a simulated efficiency comparison is shown between first CSI **100**, second CSI **300**, and a conventional H6-CSI in accordance with an illustrative embodiment. A first efficiency curve **800** shows the simulated efficiency for first CSI **100**. A second efficiency curve **802** shows the simulated efficiency for second CSI **300**. A third efficiency curve **804** shows the simulated efficiency for H6-CSI. Second CSI **300** provides a higher efficiency than first CSI **100**, and first CSI **100** provides a higher efficiency than H6-CSI. Second CSI **300** was predicted to deliver 0.25% increase in efficiency at 6 kilowatts (kW) corresponding to a 12.5% reduction of loss compared to the H6-CSI. The required DC-link current amplitude on first bus line **114** of both first CSI **100** and second CSI **300** was also reduced from 15.5 Amps (A) using H6-CSI to 10.8 A for a 30% reduction under 6 kW operation. Such a significant reduction of the DC-link current makes an inductance of inductor **104** much lower than that using H6-CSI.

Referring to FIG. **9**, a simulated common mode electromagnetic interference (CM EMI) comparison is shown between first CSI **100** and H6-CSI in accordance with an illustrative embodiment. The H6-CSI CM EMI is shown in red, and the first CSI **100** CM EMI is shown in blue. Switching events in the upper and lower rows of each inverter leg of first CSI **100** cancel with ideal switching resulting in a CM EMI that is 20 decibel microvolts (dB μ V), or ten times, lower when compared to H6-CSI.

Propagational delay distortion is unavoidable in practical power electronics circuits resulting in switching events in the upper and lower rows of each inverter leg of CSI **100** that occur at different times that those shown in FIGS. **6A-6F**. For example, gate driver chip delay differences may occur for PWM signal generator **206** of different switches. There also may be delay differences from controller **402**. There further may be differences in the turn on and turn off time of each switch. As a result, 10s to 100s of nanosecond differences may result in the switch timing relative to that shown

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in FIGS. **6A-6F**. Usually, for power electronics with higher power levels, the propagational delay distortion is higher. Referring to FIG. **10**, a simulated CM EMI comparison is shown for first CSI **100** with no delay between switching events as shown in FIG. **9** and with 60 nanoseconds delay between switching events. The 60 nanosecond delay was implemented between the switching of third switch **144**, sixth switch **154**, and ninth switch **164** and first switch **140**, fourth switch **150**, and seventh switch **160**. The first CSI **100** CM EMI with no delay is shown in blue, and the first CSI **100** CM EMI with 60 nanoseconds delay is shown in red. The CM EMI benefits have been decreased significantly especially at higher frequency regions. For a lower power level CSI (such as from several watts to several hundred watts), the propagational delay distortion will be much lower than 60 nanoseconds. For these low-power applications, first CSI **100** provides significant CM EMI reduction throughout the frequency regions.

Referring to FIG. **11**, a simulated CM EMI comparison is shown between second CSI **300** and H6-CSI in accordance with an illustrative embodiment. The H6-CSI CM EMI is shown in red, and the second CSI **300** CM EMI is shown in blue. The CM EMI that results using second CSI **300** is as high as 35 dB μ V (~750 kilohertz), which corresponds to 56 times lower when compared to H6-CSI. The reduction was consistently better than 20 dB μ V.

Referring to FIG. **12**, a simulated CM EMI comparison is shown for second CSI **300** with no delay between switching events and with 60 nanoseconds delay between switching events in accordance with an illustrative embodiment. The second CSI **300** CM EMI with no delay is shown in blue, and the second CSI **300** CM EMI with 60 nanoseconds delay is shown in red. The CM EMI benefits are essentially the same meaning second CSI **300** is not sensitive to propagational delays as a result of inclusion of tenth switch **302**. Second CSI **300** further provides a higher efficiency and a higher fault tolerance through inclusion of tenth switch **302** because tenth switch **302** provides another current path for DC-link inductor **104** when the gate signals to inverter switching circuit **102** are all off.

Referring to FIG. **13**, a simulated voltage between two pairs of windings and a current in two different windings generated by either first CSI **100** or second CSI **300** is shown in accordance with an illustrative embodiment. A first voltage curve **1300** shows the voltage $V_{1,A}$. A second voltage curve **1302** shows the voltage $V_{2,A}$. $V_{1,A}$ and $V_{2,A}$ are sinusoidal and 180 degrees out of phase with each other as expected. A first current curve **1301** shows the current $I_{1,A}$ on first, A phase line **146**. A second current curve **1303** shows the current $I_{2,A}$ on second, A phase line **148**. $I_{1,A}$ and $I_{2,A}$ are sinusoidal and 180 degrees out of phase with each other as expected.

Inverter switching circuit **102** of either first CSI **100** or second CSI **300** may be modified to support a greater or a fewer number of phases of the output signal. For example, referring to FIG. **14**, third current source inverter (CSI) **1400** is shown in accordance with an illustrative embodiment. Third CSI **1400** may include a second inverter switching circuit **1402**, inductor **104**, a third capacitive filter **1420**, and a fourth capacitive filter **1422**. Second inverter switching circuit **1402** is connected between inductor **104** and both third capacitive filter **1420** and fourth capacitive filter **1422**. Third CSI **1400** is connected between DC source **112** and AC load **404** such as a motor C **118c** and a motor D **118d**. Second application **414** implements a control algorithm that operates third CSI **1400** from sector I to sector II as summarized in FIGS. **15A-15B** respectively, and back to

sector I in a continuous loop to continually respond to DC source **112** and/or AC load **404**. FIG. **15A** represents sector I. FIG. **15B** represents sector II. Third CSI **1400** converts the DC current from DC source **112** to a single-phase AC voltage and current provided to each of motor C **118c** and motor D **118d**.

Second inverter switching circuit **1402** may include first inverter leg **106** and second inverter leg **108**. Third capacitive filter **1420** may include first capacitor **124** and second capacitor **126**. Fourth capacitive filter **1422** may include fourth capacitor **132** and fifth capacitor **134**.

Referring to FIGS. **15A** and **15B**, S_1 indicates the on-state for first switch **140**, S_2 indicates the on-state for second switch **142**, S_3 indicates the on-state for third switch **144**, S_4 indicates the on-state for fourth switch **150**, S_5 indicates the on-state for fifth switch **152**, and S_6 indicates the on-state for sixth switch **154**. The pulses indicate when the respective RB switches are turned on. The non-designated switches in each sector are in the off-state unless shown in a pulse. Control application **414** implements a control algorithm that operates third CSI **1400** from sector I to sector II as summarized in FIGS. **15A** and **15B** respectively, and back to sector I in a continuous loop to continually respond to DC source **112** and/or AC load **404**. FIG. **15A** represents sector I. FIG. **15B** represents sector II. Though not shown, all of the on-state signals of third CSI **1400** pass through a turn-off delay logic to implement an overlap time as understood by a person of skill in the art.

Referring to FIG. **15A**, a sector I pulse sequence **1500** is shown in accordance with an illustrative embodiment. Third switch **144** is in the on-state from a start of the switching interval indicated as "0" to an end of the switching period designated as T_s to show a single switching period. First switch **140** and second switch **142** are in the on-state from the start of the switching interval to a time designated as T_{n1} ; first switch **140** and fifth switch **152** are in the on-state from the time designated as T_{n1} to a time designated as T_{n2} ; and first switch **140** and second switch **142** are in the on-state from the time designated as T_{n2} to the end of the switching period, where

$$T_1 = m_a T_s \sin(\theta)$$

for

$$0 \leq \theta < \pi, T_0 = T_s - T_1, T_{n1} = \frac{T_0}{2}, T_{n2} = T_s - \frac{T_0}{2}.$$

Referring to FIG. **15B**, a sector II pulse sequence **1502** is shown in accordance with an illustrative embodiment. Sixth switch **154** is in the on-state from the start of the switching interval to the end of the switching period. Fourth switch **150** and fifth switch **152** are in the on-state from the start of the switching interval to a time designated as T_{n1} ; fourth switch **150** and second switch **142** are in the on-state from the time designated as T_{n1} to a time designated as T_{n2} ; and fourth switch **150** and fifth switch **152** are in the on-state from the time designated as T_{n2} to the end of the switching period, where

$$T_1 = m_a T_s \sin(\theta - \pi)$$

for

$$\pi \leq \theta < 2\pi, T_0 = T_s - T_1, T_{n1} = \frac{T_0}{2}, T_{n2} = T_s - \frac{T_0}{2}.$$

As another example, referring to FIG. **16**, fourth CSI **1600** is shown in accordance with an illustrative embodiment. Fourth CSI **1600** may include second inverter switching circuit **1402**, tenth RB switch **302**, inductor **104**, third capacitive filter **1420**, and fourth capacitive filter **1422**. Tenth RB switch **302** is connected between inductor **104** and second inverter switching circuit **1402** in parallel with second inverter switching circuit **1402** between first bus line **114** and second bus line **116**. Tenth RB switch **302** is connected on the side of inductor **104** opposite the connection with DC source **112**. Fourth CSI **1600** converts the DC current from DC source **112** to a single-phase AC voltage and current provided to each of motor C **118c** and motor D **118d**.

Referring to FIGS. **17A** and **17B**, S_1 indicates the on-state for first switch **140**, S_2 indicates the on-state for second switch **142**, S_3 indicates the on-state for third switch **144**, S_4 indicates the on-state for fourth switch **150**, S_5 indicates the on-state for fifth switch **152**, S_6 indicates the on-state for sixth switch **154**, and S_7 indicates the on-state for tenth switch **302**. The pulses indicate when the respective RB switches are turned on. The non-designated switches in each sector are in the off-state unless shown in a pulse. Control application **414** implements a control algorithm that operates fourth CSI **1600** from sector I to sector II as summarized in FIGS. **17A** and **17B** respectively, and back to sector I in a continuous loop to continually respond to DC source **112** and/or AC load **404**. FIG. **17A** represents sector I. FIG. **17B** represents sector II.

Referring to FIG. **17A**, a sector I pulse sequence **1700** is shown in accordance with an illustrative embodiment. First switch **140**, fifth switch **152**, and third switch **144** are in the on-state from a start of the switching interval indicated as "0" to an end of the switching period designated as T_s to show a single switching period. Tenth switch **302** is in the on-state from the start of the switching interval to a time designated as T_{n1} , and tenth switch **302** is in the on-state from the time designated as T_{n2} to the end of the switching period, where

$$T_1 = m_a T_s \sin(\theta)$$

for

$$0 \leq \theta < \pi, T_0 = T_s - T_1, T_{n1} = \frac{T_0}{2}, T_{n2} = T_s - \frac{T_0}{2}.$$

Referring to FIG. **17B**, a sector II pulse sequence **1702** is shown in accordance with an illustrative embodiment. Fourth switch **150**, second switch **142**, and sixth switch **154** are in the on-state from a start of the switching interval indicated as "0" to an end of the switching period designated as T_s to show a single switching period. Tenth switch **302** is in the on-state from the start of the switching interval to a time designated as T_{n1} , and tenth switch **302** is in the on-state from the

$$T_1 = m_a T_s \sin(\theta - \pi)$$

for

$$\pi \leq \theta < 2\pi, T_0 = T_s - T_1, T_{n1} = \frac{T_0}{2}, T_{n2} = T_s - \frac{T_0}{2}.$$

As another example, as understood by a person of skill in the art, when inverter switching circuit **102** provides N phases instead of the three phases provided in the illustrative embodiment, inverter switching circuit **102** includes N inverter legs, and first capacitive filter **120** includes N capacitors to provide a first N phase output to motor A **118a**, and second capacitive filter **122** includes N capacitors to provide a second N phase output to motor B **118b**.

A DC-link current ripple can be reduced resulting in a smaller inductance for inductor **104**. For the same output power, the DC-link current amplitude can be reduced by 50% because the voltage has been doubled again resulting in a smaller inductance for inductor **104** and a lighter inductor **104**, which is particularly beneficial in aerospace applications. A smaller inductance for inductor **104** also results in a higher power density.

Tenth switch **302** transiently shorts the DC-link's positive terminal directly to its negative terminal thereby shifting the responsibility for implementing the inverter zero states to the switching operation of tenth switch **302** making zero-current switching possible even in the presence of propagation switching delays. In addition, for any of first CSI **100**, second CSI **300**, third CSI **1400**, and fourth CSI **1600**, the use of the third row of switches generates a second common-mode voltage (CMV) component that forces the total CMV of any of first CSI **100**, second CSI **300**, third CSI **1400**, and fourth CSI **1600** to be close to zero. This suppression of the total CMV produced by the balanced first CSI **100**, second CSI **300**, third CSI **1400**, and fourth CSI **1600** significantly reduces the conducted CM EMI.

The balanced first CSI **100**, second CSI **300**, third CSI **1400**, and fourth CSI **1600** provide benefits relative to a balanced voltage-source inverter (VSI) topology. First, first CSI **100**, second CSI **300**, third CSI **1400**, and fourth CSI **1600** can use a rugged and high-temperature capable DC-link inductor (inductor **104**), while the balanced VSI uses a more fragile and temperature-limited DC-link capacitor. Second, the output voltages of both balanced CSI topologies are sinusoidal, while the balanced VSI topology delivers output voltage waveforms that consist of voltage pulses with high-dv/dt wavefronts. Third, the balanced first CSI **100**, second CSI **300**, third CSI **1400**, and fourth CSI **1600** use reverse-voltage-blocking (RB) switches, while the balanced VSI uses standard switches that replace the RVB capability with reverse-current conduction capability. Fourth, inclusion of tenth switch **302** introduced across the DC-link in second CSI **300** and in fourth CSI **1600** is not possible in the balanced VSI because it would directly short-circuit the DC-link capacitor, creating a dangerous fault condition.

The word "illustrative" is used herein to mean serving as an example, instance, or illustration. Any aspect or design described herein as "illustrative" is not necessarily to be construed as preferred or advantageous over other aspects or designs. Further, for the purposes of this disclosure and unless otherwise specified, "a" or "an" means "one or

more". Still further, using "and" or "or" in the detailed description is intended to include "and/or" unless specifically indicated otherwise.

The foregoing description of illustrative embodiments of the disclosed subject matter has been presented for purposes of illustration and of description. It is not intended to be exhaustive or to limit the disclosed subject matter to the precise form disclosed, and modifications and variations are possible in light of the above teachings or may be acquired from practice of the disclosed subject matter. The embodiments were chosen and described in order to explain the principles of the disclosed subject matter and as practical applications of the disclosed subject matter to enable one skilled in the art to utilize the disclosed subject matter in various embodiments and with various modifications as suited to the particular use contemplated.

What is claimed is:

1. A switching circuit for a current source inverter comprising:
 - a first inverter leg comprising
 - a first reverse-voltage-blocking (RB) switch;
 - a second RB switch; and
 - a third RB switch, wherein the first RB switch, the second RB switch, and the third RB switch are connected in series between a first bus line and a second bus line;
 - a second inverter leg comprising
 - a fourth RB switch;
 - a fifth RB switch; and
 - a sixth RB switch, wherein the fourth RB switch, the fifth RB switch, and the sixth RB switch are connected in series between the first bus line and the second bus line; and
 - a controller configured to control a switch between an on-state and an off-state for each RB switch; wherein, when in the on-state, a reverse voltage is blocked by a respective RB switch, and a current with a positive polarity is conducted through the respective RB switch, wherein, when in the off-state, a voltage and the current are blocked by the respective RB switch.
2. The switching circuit of claim 1, wherein each RB switch comprises:
 - a semiconductor switch comprising
 - a first terminal;
 - a second terminal; and
 - a third terminal, wherein, when the on-state signal is sent to the first terminal, a first current is conducted from the second terminal to the third terminal; and
 - a diode, wherein an anode of the diode is connected to the third terminal.
3. The switching circuit of claim 1, further comprising:
 - a seventh RB switch connected between the first bus line and the second bus line,
 - wherein the controller is further configured to switch the seventh RB switch between the on-state and the off-state.
4. The switching circuit of claim 3, wherein the seventh RB switch is controlled to enter the on-state for a predefined time period at a beginning of a switching period, wherein the seventh RB switch is controlled to enter the on-state for the predefined time period before an end of the switching period.
5. The switching circuit of claim 4, wherein either the first RB switch, the third RB switch, and the fifth RB switch or the second RB switch, the fourth RB switch, and the sixth RB switch are controlled to enter the on-state from the

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beginning of the switching period to the end of the switching period based on an angle of a space vector.

6. The switching circuit of claim 1, further comprising:

a third inverter leg comprising

a seventh RB switch;

an eighth RB switch; and

a ninth RB switch, wherein the seventh RB switch, the eighth RB switch, and the ninth RB switch are connected in series between the first bus line and the second bus line;

wherein the controller is further configured to switch the seventh RB switch, the eighth RB switch, and the ninth RB switch between the on-state and the off-state.

7. The switching circuit of claim 6, wherein the controller selects a first switching state for the first inverter leg from a set of four switching states, wherein the set includes only four switching states, a second switching state for the second inverter leg from the set of four switching states, and a third switching state for the third inverter leg from the set of four switching states, wherein each selected switching state is unique relative to other selected switching states.

8. The switching circuit of claim 7, wherein a first selectable switching state of the set of four switching states indicates that, unless all of the RB switches are controlled in the off-state, when the second RB switch is controlled in the off-state, the first RB switch and the third RB switch are in the on-state, or when the fifth RB switch is controlled in the off-state, the fourth RB switch and the sixth RB switch are in the on-state, or when the eighth RB switch is controlled in the off-state, the seventh RB switch and the ninth RB switch are in the on-state.

9. The switching circuit of claim 8, wherein a second selectable switching state of the set of four switching states indicates that, when the second RB switch is controlled in the on-state, the first RB switch and the third RB switch are in the off-state, or when the fifth RB switch is controlled in the on-state, the fourth RB switch and the sixth RB switch are in the off-state, or when the eighth RB switch is controlled in the on-state, the seventh RB switch and the ninth RB switch are in the off-state.

10. The switching circuit of claim 9, wherein a third selectable switching state of the set of four switching states indicates that the first RB switch, the second RB switch, the third RB switch, the fourth RB switch, the fifth RB switch, the sixth RB switch, the seventh RB switch, the eighth RB switch and the ninth RB switch are controlled to be simultaneously in the off-state.

11. The switching circuit of claim 10, wherein a fourth selectable switching state of the set of four switching states indicates that the first RB switch, the second RB switch, the third RB switch, the fourth RB switch, the fifth RB switch, the sixth RB switch, the seventh RB switch, the eighth RB switch and the ninth RB switch are controlled to be simultaneously in the on-state,

wherein, when one of the first inverter leg, the second inverter leg, or the third inverter leg is controlled to be in the fourth selectable switching state, a remaining pair of the first inverter leg, the second inverter leg, and the third inverter leg is controlled to be simultaneously in the off-state.

12. The switching circuit of claim 11, wherein, when any RB switch transitions from the on-state to the off-state or from the off-state to the on-state, the first RB switch, the second RB switch, the third RB switch, the fourth RB switch, the fifth RB switch, the sixth RB switch, the seventh

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RB switch, the eighth RB switch and the ninth RB switch are controlled to be simultaneously in the off-state for a predefined time period.

13. The switching circuit of claim 6, further comprising: a tenth RB switch connected between the first bus line and the second bus line,

wherein the controller is further configured to switch the tenth RB switch between the on-state and the off-state.

14. The switching circuit of claim 13, wherein the controller selects a first switching state for the first inverter leg from a set of three switching states, wherein the set includes only three switching states, a second switching state for the second inverter leg from the set of three switching states and a third switching state for the third inverter leg from the set of three switching states, wherein each selected switching state is unique relative to other selected switching states.

15. The switching circuit of claim 14, wherein a first selectable switching state of the set of three switching states indicates that, unless all of the RB switches are controlled in the off-state, when the second RB switch is controlled in the off-state, the first RB switch and the third RB switch are in the on-state, or when the fifth RB switch is controlled in the off-state, the fourth RB switch and the sixth RB switch are in the on-state, or when the eighth RB switch is controlled in the off-state, the seventh RB switch and the ninth RB switch are in the on-state.

16. The switching circuit of claim 15, wherein a second selectable switching state of the set of three switching states indicates that, when the second RB switch is controlled in the on-state, the first RB switch and the third RB switch are in the off-state, or when the fifth RB switch is controlled in the on-state, the fourth RB switch and the sixth RB switch are in the off-state, or when the eighth RB switch is controlled in the on-state, the seventh RB switch and the ninth RB switch are in the off-state.

17. The switching circuit of claim 16, wherein a third selectable switching state of the set of three switching states indicates that the first RB switch, the second RB switch, the third RB switch, the fourth RB switch, the fifth RB switch, the sixth RB switch, the seventh RB switch, the eighth RB switch and the ninth RB switch are controlled to be simultaneously in the off-state.

18. The switching circuit of claim 13, wherein the tenth RB switch is controlled to enter the on-state for a predefined time period, wherein the predefined time period occurs before and after a transition from the on-state to the off-state of any RB switch.

19. The switching circuit of claim 18, wherein the predefined time period is one-fourth of a space vector zero state's dwell time in a predefined inverter switching period.

20. A current source inverter comprising:

an inductor;

a first filter;

a second filter;

a switching circuit connected between the inductor and the first filter and between the inductor and the second filter, the switching circuit comprising

a first inverter leg comprising

a first reverse-voltage-blocking (RB) switch;

a second RB switch; and

a third RB switch, wherein the first RB switch, the second RB switch, and the third RB switch are connected in series between a first bus line and a second bus line; and

a second inverter leg comprising

a fourth RB switch;

a fifth RB switch; and

a sixth RB switch, wherein the fourth RB switch, the
fifth RB switch, and the sixth RB switch are
connected in series between the first bus line and
the second bus line; and
a controller configured to control a switch between an 5
on-state and an off-state for each RB switch;
wherein, when in the on-state, a reverse voltage is blocked
by a respective RB switch, and a current with a positive
polarity is conducted through the respective RB switch,
wherein, when in the off-state, a voltage and the current 10
are blocked by the respective RB switch,
wherein the first filter is configured to be connected
between the switching circuit and a first load, wherein
the second filter is configured to be connected between
the switching circuit and a second load. 15

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